

GEOTECHNICAL INVESTIGATION REPORT

Client – Revelop Building & Developments

Project Title – 22 Forest Way, Frenchs Forest NSW

Project Type – Addition of Basement and Alteration of the Shopping complex

Project No. – GR23239

Date Issued – 15/12/2023



Description of Services – Geotechnical Investigation Report

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Table of Contents

1.	Introduction.....	4
1.1	Background	4
1.2	Provided Information.....	4
1.3	Proposed Development	4
1.4	Objectives.....	4
1.5	Scope of Works	4
1.6	Constraints	5
2.	Desktop Assessment	5
2.1	General Site Description	5
2.2	Topography and Geological Description	6
3.	Geotechnical Investigation Results	6
3.1	Sub-Surface Conditions	6
3.2	Groundwater Observation.....	7
3.3	Lab Test Results.....	7
3.3.1	Soil Salinity & Aggressivity Test Results	7
3.3.2	Point Load Test Results.....	8
4.	Discussion and Recommendations	8
4.1	Site Classification	8
4.2	Excavation Assessment.....	8
4.3	Shoring/Footings Design Parameters	9
4.4	Batter Slopes (Temporary/Permanent)	10
4.5	Groundwater Management	10
4.6	Earthquake Site Assessment.....	10
4.7	Exposure Classification.....	10
4.8	Sub-grade Preparation	11
4.9	Conditions of the Recommendations	11
5.	Further Geotechnical Recommendations.....	11
6.	Limitations	12
	References	12

List of Tables

Table 1: Subsurface Conditions	6
Table 2: Results of Electrical Conductivity Test (Salinity)	7
Table 3: Soil pH, Chloride, Sulphate and Electrical Resistivity Test Results (AS 2159-2009).....	8
Table 4: Recommended Maximum PPV	8
Table 5: Geotechnical Design Parameters	9
Table 6: Recommended Batter Slopes (temporary)	10

List of Appendices

- Appendix A:** Site Plan
- Appendix B:** Bore Hole Logs and DCP Test Results
- Appendix C:** Laboratory Test Results
- Appendix D:** Site Classification General Information

1. Introduction

1.1 Background

CEC Geotechnical Pty Ltd was engaged by the client Revelop Building & Developments to carry out a geotechnical investigation for the proposed shopping centre at **22 Forest Way Frenchs Forest NSW**.

This report provides geotechnical recommendations regarding the existing ground conditions in order to have a clear guidance for design and construction of ground structures.

The results presented in this report are mainly based on the investigation, the laboratory tests and the author's experience. This report is prepared based on the information received from the client. If the site conditions change before, during or after construction, the geotechnical engineer shall be notified.

1.2 Provided Information

- A set of Architectural Drawings including site plans, floor plans, elevations and sections, prepared by Nettleton Tribe Architects, Project No. 11993 issued on 06/11/2023.
- A geotechnical investigation report prepared by Coffey Tetra Tech Company, Reference No. SYDE217641, issued on 26/10/2018.

1.3 Proposed Development

With reference to the information provided by the client, it is understood that the proposed development will comprise of the construction of alterations and additions to the existing shopping centre (including addition two basement level carpark).

The lowest proposed basement has a Finished Floor level (FFL) of 143.2 and hence the maximum excavation depths will be approximately 6.5m. Deeper excavation is expected locally for the proposed building footings and service pits and trenches.

1.4 Objectives

The objective of this report included:

- Assessment of subsurface profiles and groundwater considerations.
- Excavation methodologies and monitoring.
- Design parameters and allowable bearing capacities.
- Earthquake subsoil classification in accordance with Australian Standards "AS 1170.4-2007".
- Soil salinity and aggressivity assessment.
- General geotechnical recommendations regarding site preparation.

1.5 Scope of Works

The geotechnical site investigation was carried out on 1/12/2023 by an experienced geotechnical engineer in accordance with "AS 1726- 2017 The scope of works included:

- Desktop Study including a review of existing architectural drawings, survey plan, geology and topography of the site and neighbouring properties.
- Drilling of 3 boreholes (BH01 to BH03) by a 4x4 drill rig with 100 mm diameter solid flight auger and then NMLC coring to depth of 10.5m (location found in Appendix A and logs found in Appendix B)
- Standard Penetration Test (SPT) testing in accordance with Australian Standards "AS 1289"
- Site classification (see Section 4.1) in accordance with Australian Standards "AS 2870-2011"
- Soil samples were extracted from the borehole, to test the soil/rock salinity and aggressivity (see Appendix C)

1.6 Constraints

If a more detailed geotechnical investigation regarding soil reactivity is available, it should be provided to CEC Geotechnical Pty Ltd. In addition, any details related to the site's history should be supplied. This report was produced based on a limited geotechnical investigation in line with the requirements of "AS 1726 and AS 2870".

This classification is based on the findings in this investigation, including visual-tactile identification of the soil profile combined with the author's local knowledge and experience. If the site conditions change from those of the original investigation, the findings of this report may be void.

2. Desktop Assessment

2.1 General Site Description

The site is located within the Local Government Area (LGA) of Northern Beaches and is registered as Lot 20 DP1209801. The site is covering an area of approximately 2 ha and is bounded by Forest Way to the east and Grace Ave to the west as shown in Figure 1. During the site visit it was observed that there was the existing shopping centre.

Figure 1: Site Location



2.2 Topography and Geological Description

Based on the architectural drawings, it can be noted that the site is gently sloping from boundaries to the centre.

The 1:100,000 scale Geological Series Sheet 9130 (Edition 1) 1991 of the Sydney region (Figure 2) indicates that the subject site is underlain by Hawkesbury group SANDSTONE (Rh) consisting of medium to coarse grained quartz sandstone containing minor shale and laminite lenses.

Figure 2: 1:100,000 scale Geological Series Map of the Sydney Region



3. Geotechnical Investigation Results

3.1 Sub-Surface Conditions

The results of the investigation indicate that the subsurface profile comprises of poorly graded clayey sand underlain by sandstone bedrock. Based on the borehole information, a summary of subsurface conditions is presented below. The location of each borehole can be found in Appendix A and more detailed logs can be found in Appendix B.

Table 1: Subsurface Conditions

Unit	Description	BH01 (m)*	BH02 (m)*	BH03 (m)*
Unit – 1: Paving	Concrete	0-0.2	0-0.2	0-0.2
Unit – 2: Residual	Clayey SAND (SC): medium dense to dense, moist	0.2-0.7	0.2-0.7	0.2-0.7
Unit – 3: SANDSTONE -V	Grey, brown, highly weathered, very low to low strength.	0.7-2.2	0.7-2.1	0.7-2.5
Unit – 4: SANDSTONE -IV	Grey, brown, moderately weathered, low to medium strength.	2.2-4.0	2.1-4.5	2.5-4.5
Unit – 5: SANDSTONE - III	Grey, brown, moderately weathered, low to medium strength.	4.0-10.0	4.5-10.5	4.5-10

*Depths below ground level (BGL) at the location of each borehole. This may vary depending on other areas of the site.
BH01, BH02 were terminated/met refusal at depths of 10m and BH03 at 10.5m

3.2 Groundwater Observation

CEC Geotechnical utilised the existing three groundwater monitoring wells previously installed by Coffey Tetra Tech in boreholes (MW01, MW02 & MW03). The groundwater levels were measured few times between from November to 15th of December. No ground water noted in the wells.

Table 2: Observed Groundwater Levels

Groundwater Well	Ground RL	Groundwater Level (m bgl)/RL
GW1	149.9	No Ground Water Encountered
GW2	149.9	No Ground Water Encountered
GW3	149.9	No Ground Water Encountered

3.3 Lab Test Results

6 samples were collected from each borehole (BH01 to BH03) at depths of 0.3 m to 1.0 m. The samples were submitted to NATA accredited laboratories for further testing. These tests included:

- Chemical testing (Salinity, pH, Chloride (Cl), sulphates (SO₄), and electrical conductivity) to assess soil salinity and aggressivity.
- Point Load Strength Index (PLSI) testing on rock core samples.

3.3.1 Soil Salinity & Aggressivity Test Results

The soil encountered is clayey Sand and was tested as stipulated in the Department of Natural Resources (DNR) publication "Site Investigations for Urban Salinity" (2002).

Results of the laboratory testing are attached to this report in Appendix C and summarised in Tables 2 and 3.

Table 3: Results of Electrical Conductivity Test (Salinity)

Borehole	Depth (m bgl)	Electrical Conductivity (dS/m)	Multiplication Factor ^a	Electrical Conductivity of Saturated Extract (dS/m)	Soil Type
				EC _e	
BH01	0.5	0.058	10	0.58	Loam
BH01	1	0.054	10	0.54	Loam
BH02	0.3	0.031	10	0.31	Loam
BH02	1	0.031	10	0.31	Loam
BH03	0.5	0.037	10	0.37	Loam
BH03	1	0.035	10	0.35	Loam

"Site Investigations for Urban Salinity" (2002)

Non-saline <2 dS/m
Saline at >4 dS/m
Slightly saline 2-4 dS/m
Moderately saline 4-8 dS/m
Very saline 8-16 dS/m
Highly saline >16 dS/m

Table 4: Soil pH, Chloride, Sulphate and Electrical Resistivity Test Results (AS 2159-2009)

Borehole	Depth (m bgl)	MC* (%)	pH	Chloride (mg/kg)	Sulphate as SO ₄ (mg/kg)	Electrical Resistivity (ohm.cm)
BH01	0.5	8	9.5	< 10	21	170
BH01	1	9.5	9.1	< 10	42	180
BH02	0.3	8.8	6.5	< 10	41	320
BH02	1	10	5	< 10	36	320
BH03	0.5	10	6.8	< 10	50	270
BH03	1	8.9	5	< 10	50	290

*MC = Moisture Content

Note: Electrical Resistivity converted from Electrical Conductivity

3.3.2 Point Load Test Results

The results of the point load testing have been summarised in Table 4 below.

Table 5: Summary of Rock Laboratory Test Results

Borehole No	Depth (m)	Point Load (IS ₅₀) (MPa)	Borehole No	Depth (m)	Point Load (IS ₅₀) (MPa)
BH01	2.00	0.35	BH02	6.90	0.18
BH01	3.00	1.23	BH02	7.40	0.30
BH01	4.00	0.74	BH02	8.50	0.09
BH01	4.80	0.78	BH02	9.60	0.46
BH01	6.00	0.93	BH03	1.80	0.09
BH01	6.80	0.83	BH03	2.50	0.32
BH01	9.00	0.61	BH03	3.90	0.64
BH02	1.80	0.06	BH03	5.10	0.18
BH02	3.00	0.11	BH03	6.90	0.36
BH02	4.00	0.42	BH03	8.20	0.42
BH02	4.80	0.35	BH03	9.60	0.28
BH02	6.00	0.06			

The test certificates are presented in Appendix C

4. Discussion and Recommendations

4.1 Site Classification

Due to the presence of trees and topsoil, the overall site is classified as **Class P** in accordance with "AS 2870 2011". Once topsoil/fill is removed, this site will then be classified as **CLASS S** at the basement slab level in accordance with "AS 2870 2011". Class S is indicative of 0 to 20mm movement due to moisture changes.

At Basement Slab level the site can be classified as **class A** which is indicative of little or no movement due to moisture changes in accordance with "AS 2870 2011".

4.2 Excavation Assessment

Accordance with the proposed basement levels, the excavations for the proposed basement should mostly encounter residual clayey sand. Removal of materials should be carried out using conventional earthmoving equipment, such as a hydraulic excavator or backhoe. If rock hammers are to be used, such works will need to be completed carefully as there may be direct transmission of ground vibration to existing structures. We recommend that a geotechnical engineer to be present at the site as they may be required to carry out quantitative vibration monitoring to confirm vibration units do not exceed the maximum Peak Particle Velocity (PPV) values provided in Table 4 below.

Table 6: Recommended Maximum PPV

Type of Building or Structure	Maximum PPV (mm/sec)
Historical buildings or structures in sensitive conditions	2
Residential and low-rise buildings	5
Brick or unreinforced structures in good condition	10
Commercial and industrial buildings or structures of reinforced concrete or steel construction	25

It is recommended that monitoring is carried out during demolition and excavation using a vibration monitoring instrument (Vibra) and alarm levels (being the appropriate PPV).

If the vibrations exceed the above values or appear excessive, the excavations should cease, and the project Geotechnical Engineer should be contacted immediately.

4.3 Shoring/Footings Design Parameters

The following parameters established from Rankine's theory would be valid in the design of a retention system. These bearing pressures apply where footings are founded minimum 300mm into the specified material.

Table 7: Geotechnical Design Parameters

Material Description	Unit Weight (kN/m ³)	Allowable Bearing Capacity (kPa)	Ultimate Bearing Capacity (kPa)	C (kPa)	Friction Angle (°)	K _a [#]	K _p [#]	K _o [#]	Modulus of Elasticity (MPa)	Poisson's Ratio v'
Unit 2: Clayey SAND (SC): loose to medium dense	17	100	300	0	26	0.41	2.46	0.58	6	0.3
Unit 3: Rock (SST): SANDSTONE Class -V	20	700	2100	2	30	0.36	2.77	0.53	30	0.3
Unit 4: SANDSTONE Class -IV	22	1500	4500	20	32	0.33	3.00	0.50	200	0.3
Unit 5: SANDSTONE Class -IV	24	3500	11500	50	34	0.3	3.25	0.40	500	0.3

*Approximate depth below ground level based on borehole logs completed during geotechnical investigation.

[#]K_a, K_p and K_o are the active, passive and at-rest earth pressure coefficients.

The following may need to be adopted in response to the design of any retaining wall structures:

- The retaining walls which are propped or restrained by concrete slabs, should be designed using a triangular lateral earth pressure distribution and the K_o , as mentioned in Table 6, for the soil profiles and other backfill materials.
- Free-standing cantilever walls should be designed using a triangular lateral earth pressure distribution and the K_a , as mentioned in Table 5, for the soil profiles and other backfill materials.
- Lateral toe restraint can be achieved through passive resistance adjacent to the wall using a triangular lateral earth pressure and the K_p , as mentioned in Table 5, for the soil profiles and other backfill materials.
- All surcharge loads should be allowed for in the retaining wall design, including building footings and construction related activities, using the appropriate earth pressure coefficient as mentioned in Table 5. (Sloping needs to be considered a surcharge)

4.4 Batter Slopes (Temporary)

The following temporary batter slopes may be considered in areas where sufficient space exists between the basement excavation and the boundary and where an adjacent footing is outside a zone of influence obtained by drawing a line at a 45° angle up from the toe of the proposed excavation.

Table 8: Recommended Batter Slopes (temporary)

Material	Maximum Batter Slope (H:V)
Topsoil / Fill	2:1
Clayey SAND	1.5:1
Rock: SANDSTONE	1:1

4.5 Groundwater Management

Based on observations during the fieldwork, water level monitoring data, available hydrogeological data, and information for the site available at the time of the investigation, ground water level varies across the site. It is considered that the excavation will be predominantly damp or minor seepage condition will be encountered which can be managed by a conventional sump and pump system. In the long term, adequate drainage system should be provided around the perimeter of the basement and below the basement slab on ground. The drainage system needs to be designed and inspected by a hydraulic/stormwater engineer.

4.6 Earthquake Site Assessment

In accordance with Australian Standard “AS 1170.4-2007” (Reference 2) the site may be classified as a “strong rock” (Class Ae).

4.7 Exposure Classification

The lab results show that the electrical conductivity of saturated extracts (EC_e) is approximately 0.31 ds/m to 0.58 ds/m, and hence the samples of residual deposit soil are “**Non-Saline**”.

- In accordance with “AS 2159” *Piling – Design and Installation*, the lab results indicated that the soil is: “**Non-aggressive**” for Steel piles and “**Non-aggressive**” for Reinforced Concrete Piles
- Chloride, Sulphate and Electrical resistivity is “**Non-aggressive**” for Steel Piles and Reinforced Concrete Piles.

4.8 Sub-grade Preparation

- Fill should be compacted close to its optimum moisture content (+/- 2%) during compaction.
- The compaction method and equipment shall suit the filled material. The compaction of soil shall be tested by a NATA accredited laboratory and Geotechnical Inspection and Testing Authority (GITA) to ensure it meets the requirements of “AS 3798-2007 Guidelines on earthworks for commercial and residential developments”.
- Any organic materials (including topsoil) within the proposed building envelope are to be removed.
- The site should be proof rolled after an initial site scrape to unveil any soft spots. Any soft areas are to be removed and backfilled with compacted fill material as described in “AS 2870-2011”, cl 6.4.2.

4.9 Conditions of the Recommendations

- The descriptions of the soils encountered in the boreholes follow those outlined in “AS 726-2017”, Geotechnical Site Investigations. Colour descriptions can vary with soil moisture content and individual interpretation.
- The advice given in this report assumes that the test results are representative of the overall subsurface conditions. However, it should be noted that actual conditions in some parts of the building site may differ from those found in the boreholes. If excavations reveal soil conditions significantly different from those shown in our attached Borehole Log(s), CEC Geotechnical shall be consulted and the excavations shall be stopped immediately.
- Depths mentioned in this report are measured from the surface during testing and may vary accordingly if any filling or excavation works are carried out. The description of the foundation material has been provided for ease of recognition over the whole building site.
- Any sketches in this report should be considered as only approximate pictorial evidence of our work. Therefore, unless otherwise stated, any dimensions or slope information should not be used for any building cost calculations and/or positioning of the building. Dimensions on logs are correct.

5. Further Geotechnical Recommendations

CEC Geotechnical should be engaged at the following stages:

- If soil conditions encountered differ significantly from those described within this report.
- If the proposed development is altered significantly from what has been assessed and described within this report.
- To confirm no permanent groundwater encountered during the construction.
- To confirm safe batter angles and excavation methods during construction.
- To confirm founding materials and allowable bearing capacity.
- If the site conditions at the time of construction differ from those described in this report, then CEC Geotechnical shall be contacted. The owner/builder will be responsible for any fees associated with this additional work.

6. Limitations

This report and its associated recommendations have been prepared exclusively for our client who is named on the front page of this report and is the only intended entity to benefit from this report. CEC Geotechnical notes that reliance on the information provided in this report by any third party will be at their own risk. It should be noted that the analysis and conclusions made in this report may rely on works by other consultants and entities and hence, should these documents and investigations be incorrect, CEC Geotechnical must be made aware and the results of this report may be void.

For and on behalf of CEC Geotechnical Pty Ltd

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Principal Engineering Geologist
B.Sc. M.Sc. RPgeo (Geotechnical Engineering)

References

- AS 2870 -2011, Residential Slab and Footings – Construction
- AS 1726-2017, Geotechnical Site Investigations
- AS 2159-2009, Piling - Design and Installation
- AS 3798-2007 “Guidelines on earthworks for commercial and residential developments”
- Geological Series Sheet 9030 (EDITION 1) 1991, Map of the Sydney Region, Scale 1:100,000
- Site investigations for urban salinity, Date 1 January 2002, Department of Land and Water Conservation .

Appendix A:

Site Plan with Borehole Locations






CEC GEOTECHNICAL

Drawn	KT	CLIENT: REVELOP BUILDING & DEVELOPMENTS SITE ADDRESS: 22 Forest Way, Frenchs Forest	Figure	1
Checked	SG		Title	Site Plan
Date	1/12/2023		Job No	GR23239
Scale @ A3	NTS			

Appendix B:
Borehole Logs, DCP Test Results & Test Pits

UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : KT	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10 m BGL	Date : 01/12/2023	Loc Comment :

Drilling Method	Depth (m)	Water	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Testing	Consistency/Density	Well Diagram
								SPT		
Solid Flight Auger	0.2		Non-Soil		CCT	Concrete				
			Residual		SC	Residual Clayey SAND (SC) : medium dense to dense, low plasticity clay, brown grey, fine grained, moist.	M		MD-D	
	0.7		Rock		SST	Extremely weathered, rock Clayey SAND (SST) : very loose, low plasticity clay, grey red, fine grained, moist.		3, 5, 20, (N = 25)	VL	
	1					1m : Commenced NMLC Coring;				
	2									
	3									
	4									

UTM : 56H

Easting (m) : 0

Northing (m) : 0

Ground Elevation : Not Surveyed

Total Depth : 10 m BGL

Drill Rig : Truck mounted Rig

Driller Supplier : ADF Drilling

Logged By : KT

Reviewed By :

Date : 01/12/2023



Job Number : GR23239

Client : Revelop


Project : Proposed Commercial Development

Location : 22 Forest Way, Frenches Forest

Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	RQD% and TCR%	Defect Spacing (mm)	Defect Description type, inclination, planarity, roughness, coating thickness	Well Diagram
								VLS	LS	MS	HS	VHS	E/S					
						Start Coring at 1m												
NMLC Coring		1	Rock		SST	Rock SANDSTONE: distinctly weathered, very low to low strength, red grey, fine grained, moist.	DW										XWS,	
		1.7	Rock		SST	Rock SANDSTONE: distinctly weathered, low strength, red grey, fine grained, moist.	DW										IS, PL, SO, CT, ,	
		2															J, PL, SO, CL, OP,	
																	J, IR, RO, CT, OP,	
		3																
																	J, PL, SO, CL, C,	
		4															J, CV, RO, CL, ,	
																	J, PL, SO, CL, C,	

UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : KT	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10 m BGL	Date : 01/12/2023	Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	RQD% and TCR%	Defect Spacing (mm)	Defect Description <small>type, inclination, planarity, roughness, coating thickness</small>	Well Diagram
								VLS	LS	MS	HS	VHS	E/S					
NMLC Coring		5	Rock		SST	Rock SANDSTONE: highly weathered, high strength, grey, fine grained, moist.	HW									30	J, STP, RO, CL, OP,	
																100	J, PL, RO, CL, ,	
																300	J, PL, SO, CL, C,	
																1000	J, PL, SO, CL, C,	
																3000	J, PL, SO, CL, C,	
		6															J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
		7															IS, PL, SO, CL, ,	
																	J, PL, SO, CL, ,	
																	J, PL, SO, CL, ,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, ,	
		8															J, PL, SO, CL, ,	
																	J, PL, SO, CL, ,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
		9															J, PL, SO, CL, C,	



Loc Comment :




UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : AL	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10 m BGL	Date : 30/11/2023	Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	ROD% and TCR%	Defect Spacing (mm)					Defect Description	Well Diagram
								VLS	LS	MS	HS	VHS	EHS									

Job Number : GR23239
Client : Revelop
Project : Proposed Commercial Development
Location : 22 Forest Way, Frenches Forest
Loc Comment :

Page 2 of 2



UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : AL	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10.5 m BGL	Date : 30/11/2023	Loc Comment :

Drilling Method	Depth (m)	Water	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Testing	Consistency/Density	Well Diagram
								SPT		
Solid Flight Auger	0.2		Non-Soil		CCT	Concrete	M			
			Residual		SC	Residual Clayey SAND (SC) : medium dense to dense, low plasticity clay, grey brown, fine grained, moist.			MD-D	
	0.7		Rock		SST	Extremely weathered, rock Clayey SAND (SST) : very loose, low plasticity clay, grey, fine grained, moist.		12, (N = 24)	VL	
	1					1m : Commenced NMLC Coring;				
	2									
	3									
	4									


UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : AL	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10.5 m BGL	Date : 30/11/2023	Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	RQD% and TCR%	Defect Spacing (mm)	Defect Description type, inclination, planarity, roughness, coating thickness	Well Diagram
								VLS	LS	MS	HS	VHS	EHS					
						Start Coring at 1m												
NMLC Coring		1	Rock		SST	Rock SANDSTONE: distinctly weathered, low strength, grey, fine grained, moist.	DW								RQD = 87%		J, PL, RO, STN, OP, J, PL, RO, STN, OP,	
		1.6	Rock		SST	Rock SANDSTONE: highly weathered, low strength, grey, fine grained, moist.	HW										J, PL, RO, CT, , J, PL, RO, STN, OP, J, PL, RO, CL, OP, J, PL, RO, STN, OP, J, PL, RO, CL, C, J, PL, RO, CL, OP,	
		2																
		3															J, PL, SO, CL, OP, J, PL, RO, CL, OP,	
		4															J, PL, RO, CL, C, J, PL, CL, OP, J, PL, RO, CL, C,	
																	J, PL, RO, CL, OP, J, PL, RO, CL, C,	
																	J, PL, RO, STN, C, J, PL, RO, CL, OP,	

UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : AL	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10.5 m BGL	Date : 30/11/2023	Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	RQD% and TCR%	Defect Spacing (mm)	Defect Description <small>type, inclination, planarity, roughness, coating thickness</small>	Well Diagram
								VLS	LS	MS	HS	VHS	E/S					
NMLC Coring		5.2	Rock		SST	Rock SANDSTONE: highly weathered, low strength, grey, fine grained, moist.	HW											
			Rock		SST	Rock SANDSTONE: moderately weathered, medium to high strength, grey, fine grained, moist.	MW											
		6															J, PL, RO, STN, ,	
																	J, PL, RO, CL, C,	
																	J, PL, RO, CL, C,	
																	J, PL, RO, STN, ,	
																	J, PL, RO, STN, OP,	
																	J, PL, RO, CL, OP,	
																	J, PL, RO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, OP,	
																	J, PL, RO, CL, ,	
																	J, PL, SO, CL, C,	
																	J, PL, SO, CL, OP,	
																	J, PL, RO, CL, OP,	
																	J, PL, RO, CL, OP,	
																	J, PL, RO, CL, OP,	
																	J, PL, RO, CL, OP,	

UTM : 56H	Drill Rig : Truck mounted Rig	Job Number : GR23239
Easting (m) : 0	Driller Supplier : ADF Drilling	Client : Revelop
Northing (m) : 0	Logged By : AL	Project : Proposed Commercial Development
Ground Elevation : Not Surveyed	Reviewed By :	Location : 22 Forest Way, Frenches Forest
Total Depth : 10.5 m BGL	Date : 30/11/2023	Loc Comment :

Drilling Method	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Weathering	Estimated Strength						Is(50)	RQD% and TCR%	Defect Spacing (mm)	Defect Description <small>type, inclination, planarity, roughness, coating thickness</small>	Well Diagram
								VLS	LS	MS	HS	VHS	EHS					
			Rock		SST	Rock SANDSTONE: moderately weathered, medium to high strength, grey, fine grained, moist.	MW									30 100 300 1000 3000		
		11				BH03 Terminated at 10.5m												
		12																
		13																
		14																

Client:	Revelop Building & Developments
Project Number:	GR23239
Bore No.:	BH01
Project Location:	22 Forest Way, Frenchs Forest

Date:	30/11/2023
Drawn By:	KT
Checked By:	SG
Issue Date:	15/12/2023

GR23206 BH01 Coring Commenced 1.0m



End of Borhole 10.0m

Client:	Revelop Building & Developments
Project Number:	GR23239
Bore No.:	BH02
Project Location:	22 Forest Way, Frenchs Forest

Date:	30/11/2023
Drawn By:	KT
Checked By:	SG
Issue Date:	15/12/2023

GR23206 BH02 Coring Commenced 1.0m



Client:	Revelop Building & Developments
Project Number:	GR23239
Bore No.:	BH03
Project Location:	22 Forest Way, Frenchs Forest

Date:	30/11/2023
Drawn By:	KT
Checked By:	SG
Issue Date:	15/12/2023

GR23206 BH03 Coring Commenced 1.0m



EXPLANATION OF NOTES, ABBREVIATIONS & TERMS USED ON BOREHOLE AND TEST PIT LOGS - SOIL DESCRIPTION (AS1726 - 2017)

SOIL CLASSIFICATION SYSTEM

Coarse Grained Soil

GW	Well graded gravels, gravel-sand mixtures, little or no fines
GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines, uniform gravels
GM	Silty gravels, Gravel-sand-silt mixtures
GC	Clayey gravels, gravel-sand-clay mixtures
SW	Well-graded sands, gravelly sands, little or no fines
SP	Poorly-graded sands, gravelly sand, little or no fines
SM	Silty sands, sand-silt mixtures
SC	Clayey sands, sand-clay mixtures

Fine Grained Soils

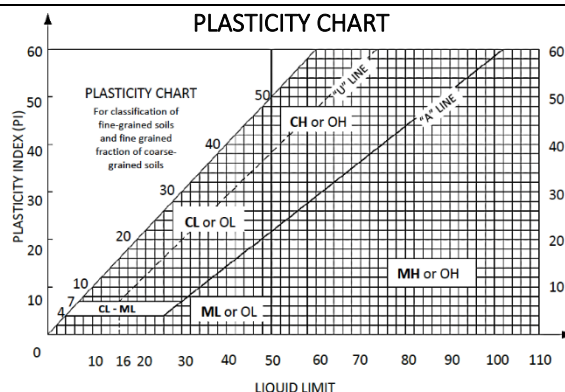
ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or silts with low plasticity
CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays
OL	Organic silts and organic silty clays or low plasticity
MH	Inorganic silts, micaceous or diatomaceous fine sand for silty soils
CH	Inorganic clays of high plasticity
OH	Organic clays of medium to high plasticity, organic silts
PT	Peat, humus, swamp soils with high organic contents

First Letter: G = Gravel, S = Sand, M = Silt, C = Clay; Second Letter: W = Well graded, P = Poorly-graded, M = Mixture, O = Organic, L = Low plasticity, H = High plasticity
Soils may be a combination of multiple soil classifications where borderline

PARTICLE SIZE

Soil	Major Division	Sub-Division	Particle Size (mm)
Coarse	Boulders		>200
	Cobbles		63 – 200
	Gravel	Coarse	20 – 63
		Medium	6 – 20
		Fine	2.36 – 6
	Sand	Coarse	0.6 – 2.36
		Medium	0.2 – 0.6
		Fine	0.075 – 0.2
Fine	Silt		0.002 – 0.075
	Clay		<0.002

0.075 mm is the approximate minimum particle size discernible by eye



MOISTURE CONDITION

Coarse	D	Dry	Sands and gravels are free flowing.
	M	Moist	Soils are darker than in the dry condition and may feel cool. Sands and gravels tend to cohere.
	W	Wet	Soils exude free water. Sands and gravels tend to cohere
Fine	PL	Plastic Limit	Moisture content of fine grained soils are described; as below plastic limit (<PL), near to plastic limit (=PL), above plastic limit(>PL), near to the liquid limit (=LL), or above the liquid limit (>LL)
	LL	Liquid Limit	

CONSISTENCY AND DENSITY

Fine Grained Soils

VS	Very Soft	Exudes between fingers when squeezed
S	Soft	Can be moulded by light finger pressure
F	Firm	Can be moulded by strong finger pressure
St	Stiff	Cannot be moulded by fingers. Can be indented by thumb
VSt	Very Stiff	Can be indented by thumb nail
H	Hard	Can be indented by thumb nail with difficulty

Pocket Penetrometer Reading (kPa)

<25
20 – 50
50 – 100
100 – 200
200 – 400
>400

Coarse Grained Soils

VL	Very Loose	Density Index %	'N' Value
L	Loose	≤15	0 – 4
MD	Medium Dense	15 – 35	4 – 10
D	Dense	35 – 65	10 – 30
VD	Very Dense	65-85	30 – 50
		>85	>50

SECONDARY OR MINOR SOIL COMPONENTS

Designation of Components	In Coarse Grained Soils				In Fine Grained Soils	
	% Fines	Terminology	% Accessory Coarse Fraction	Terminology	% Sand/gravel	Terminology
Minor	≤5	'trace' clay/silt	≤15	'trace' sand/gravel	≤15	'trace' sand/gravel
	5 – 12	'with' clay/silt	15 – 30	'with' sand/gravel	15 – 30	'with' sand/gravel
Secondary	>15	Prefix silty or clayey	>30	Prefix sandy or gravelly	>30	Prefix sandy or gravelly

EXPLANATION OF NOTES, ABBREVIATIONS & TERMS USED ON BOREHOLE AND TEST PIT LOGS - SOIL DESCRIPTION (AS1726 - 2017)

STRENGTH OF INTACT ROCK

Symbol	Term	Point Load Index, (I_{50}) MPa	Field Guide to Strength
VL	Very Low	$0.03 \leq I_{50} < 0.1$	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; pieces up to 30 mm thick can be broken by finger pressure
L	Low	$0.1 \leq I_{50} < 0.3$	Easily scored with knife; indentations 1 mm to 3 mm after firm blow with pick point; core 150mm long and 50 mm diameter can be broken by hand; sharp edges of core friable
M	Medium	$0.3 \leq I_{50} < 1.0$	Readily scored with knife; core 150 mm long and 50 mm diameter can be broken by hand with difficulty
H	High	$1.0 \leq I_{50} < 3$	Core 150 mm long and 50 mm diameter cannot be broken by hand but can be broken by single firm blow of pick; rock rings under hammer
VH	Very High	$3 \leq I_{50} < 10$	Hand held specimen breaks with pick after more than one blow; rock rings under hammer
EH	Extremely High	$10 \leq I_{50}$	Specimen requires many pick blows to break intact rock, rock rings under hammer

Material with rock strength less than “Very Low” is to be described using soil properties

DEGREE OF ROCK WEATHERING

DEGREE OF ROCK WEATHERING				
Term		Symbol	Definition	
Residual Soil		RS	Soil derived from the weathering of rock; the mass structure and material fabric are no longer evident the soil has not been significantly transported.	
Extremely Weathered		XW	Material is weathered to such an extent that it has soil properties, i.e. it either disintegrates or can be remoulded in water. Fabric of original rock still visible.	
Highly Weathered	Distinctly Weathered	HW	DW	Rock strength is changed by weathering. The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognizable. Some minerals are decomposed to clay minerals. Porosity may be increased by leach, or may be decreased due to deposition or weathering products in pores.
Moderately Weathered		MW		The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognizable, but shows little or no change of strength from fresh rock.
Slightly Weathered		SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.	
Fresh		FR	Rock shows no sign of decomposition or staining.	

Distinctly Weathered is to be used when it is not possible to differentiate between highly and moderately weathered.

Extremely Weathered material is to be described using soil properties

ROCK MASS PROPERTIES

Term	Separation of Stratification Planes	Term	Description
Thinly laminated	< 6 mm	Fragmented	Primarily fragments < 20 mm length and mostly of width < core diameter
Laminated	6 mm to 20 mm	Highly fractured	Core lengths generally less than 20 mm to 40 mm with occasional fragments
Very thinly bedded	20 mm to 60 mm		
Thinly bedded	60 mm to 200 mm	Fractured	Core lengths mainly 30 mm to 100 mm with occasional shorter and longer pieces
Medium bedded	0.2 m to 0.6 m	Slightly fractured	Core lengths generally 0.3 m to 1.0 m with occasional longer and shorter sections
Thickly bedded	0.6 m to 2.0 m		
Massive	> 2 m	Unbroken	Core has no fractures

DEFECT TYPES AND DESCRIPTIONS

Defect Type		Defect Shape		Surface Roughness		Defect Coatings	
BR	Bedding parting	PL	Planar	VR	Very rough	CL	Clean
JT	Joint	ST	Stepped	RO	Rough	ST	Stained
SR	Sheared surface	CR	Curved	SM	Smooth	VN	Veneer
SZ	Sheared zone	IR	Irregular	PO	Polished	CT	Coating
SS	Sheared seam	UN	Undulating	SL	Slickenside		
CS	Crushed seam						
IS	Infill seam						
XS	Extremely Weathered Seam						

Vertical Boreholes – The dip of the defect is given from the horizontal
Inclined Boreholes – The angle of the defect is given from the core axis

Appendix C:

Laboratory Test Results

CEC Geotechnical
Unit 4 83 Grose Street
North Paramatta
NSW 2151



NATA Accredited
Accreditation Number 1261
Site Number 18217

Accredited for compliance with ISO/IEC 17025 – Testing
NATA is a signatory to the ILAC Mutual Recognition
Arrangement for the mutual recognition of the
equivalence of testing, medical testing, calibration,
inspection, proficiency testing scheme providers and
reference materials producers reports and certificates.

Attention: **Daniella Touma - CC all Reports/Invoices/SRAs**

Report **1049970-S**
Project name **22 FOREST WAY FRENCHS FOREST**
Project ID **GR23239**
Received Date **Dec 01, 2023**

Client Sample ID			BH01-0.5	BH01-1.0	BH02-0.3	BH02-1.0
Sample Matrix			Soil	Soil	Soil	Soil
Eurofins Sample No.			S23-De0003250	S23-De0003251	S23-De0003252	S23-De0003253
Date Sampled			Nov 30, 2023	Nov 30, 2023	Nov 30, 2023	Nov 30, 2023
Test/Reference	LOR	Unit				
Chloride	10	mg/kg	< 10	< 10	< 10	< 10
Conductivity (1:5 aqueous extract at 25 °C as rec.)	10	uS/cm	58	54	31	31
pH (1:5 Aqueous extract at 25 °C as rec.)	0.1	pH Units	9.5	9.1	6.5	5.0
Resistivity*	0.5	ohm.m	170	180	320	320
Sulphate (as SO4)	10	mg/kg	21	42	41	36
Sample Properties						
% Moisture	1	%	8.0	9.5	8.8	10

Client Sample ID			BH03-0.5	BH03-1.0
Sample Matrix			Soil	Soil
Eurofins Sample No.			S23-De0003254	S23-De0003255
Date Sampled			Nov 30, 2023	Nov 30, 2023
Test/Reference	LOR	Unit		
Chloride	10	mg/kg	< 10	< 10
Conductivity (1:5 aqueous extract at 25 °C as rec.)	10	uS/cm	37	35
pH (1:5 Aqueous extract at 25 °C as rec.)	0.1	pH Units	6.8	5.0
Resistivity*	0.5	ohm.m	270	290
Sulphate (as SO4)	10	mg/kg	50	50
Sample Properties				
% Moisture	1	%	10	8.9

Sample History

Where samples are submitted/analysed over several days, the last date of extraction is reported.

If the date and time of sampling are not provided, the Laboratory will not be responsible for compromised results should testing be performed outside the recommended holding time.

Description	Testing Site	Extracted	Holding Time
Chloride	Sydney	Dec 04, 2023	28 Days
- Method: LTM-INO-4270 Anions by Ion Chromatography			
Conductivity (1:5 aqueous extract at 25 °C as rec.)	Sydney	Dec 04, 2023	7 Days
- Method: LTM-INO-4030 Conductivity			
pH (1:5 Aqueous extract at 25 °C as rec.)	Sydney	Dec 04, 2023	7 Days
- Method: LTM-GEN-7090 pH by ISE			
Sulphate (as SO ₄)	Sydney	Dec 04, 2023	28 Days
- Method: In-house method LTM-INO-4270 Sulphate by Ion Chromatograph			
% Moisture	Sydney	Dec 02, 2023	14 Days
- Method: LTM-GEN-7080 Moisture			



web: www.eurofins.com.au
email: EnviroSales@eurofins.com

Melbourne 6 Monterey Road Dandenong South VIC 3175 +61 3 8564 5000 NATA# 1261 Site# 1254	Geelong 19/8 Lewalan Street Grovedale VIC 3216 +61 3 8564 5000 NATA# 1261 Site# 25403	Sydney 179 Magowar Road Girraween NSW 2145 +61 2 9900 8400 NATA# 1261 Site# 18217	Canberra Unit 1,2 Dacre Street Mitchell ACT 2911 +61 2 6113 8091 NATA# 1261 Site# 25466	Brisbane 1/21 Smallwood Place Murarie QLD 4172 T: +61 7 3902 4600 NATA# 1261 Site# 20794	Newcastle 1/2 Frost Drive Mayfield West NSW 2304 +61 2 4968 8448 NATA# 1261 Site# 25079 & 25289	Perth 46-48 Banksia Road Welshpool WA 6106 +61 8 6253 4444 NATA# 2377 Site# 2370	Auckland 35 O'Rorke Road Penrose, Auckland 1061 +64 9 526 4551 IANZ# 1327	Auckland (Asb) Unit C1/4 Pacific Rise, Mount Wellington, Auckland 1061 +64 9 525 0568 IANZ# 1308	Christchurch 43 Detroit Drive Rolleston, Christchurch 7675 +64 3 343 5201 IANZ# 1290	Tauranga 1277 Cameron Road, Gate Pa, Tauranga 3112 +64 9 525 0568 IANZ# 1402
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Company Name:	CEC Geotechnical	Order No.:		Received:	Dec 1, 2023 3:14 PM
Address:	Unit 4 83 Grose Street North Paramatta NSW 2151	Report #:	1049970	Due:	Dec 7, 2023
		Phone:	02 9630 0121	Priority:	5 Day
		Fax:		Contact Name:	Daniella Touma - CC all
Project Name:	22 FOREST WAY FRENCHS FOREST				
Project ID:	GR23239				

Eurofins Analytical Services Manager : Hannah Mawbey

Sample Detail						Aggressivity Soil Set	Moisture Set
Sydney Laboratory - NATA # 1261 Site # 18217						X	X
External Laboratory							
No	Sample ID	Sample Date	Sampling Time	Matrix	LAB ID		
1	BH01-0.5	Nov 30, 2023		Soil	S23-De0003250	X	X
2	BH01-1.0	Nov 30, 2023		Soil	S23-De0003251	X	X
3	BH02-0.3	Nov 30, 2023		Soil	S23-De0003252	X	X
4	BH02-1.0	Nov 30, 2023		Soil	S23-De0003253	X	X
5	BH03-0.5	Nov 30, 2023		Soil	S23-De0003254	X	X
6	BH03-1.0	Nov 30, 2023		Soil	S23-De0003255	X	X
Test Counts						6	6

Internal Quality Control Review and Glossary

General

- Laboratory QC results for Method Blanks, Duplicates, Matrix Spikes, and Laboratory Control Samples follow guidelines delineated in the National Environment Protection (Assessment of Site Contamination) Measure 1999, as amended May 2013. They are included in this QC report where applicable. Additional QC data may be available on request.
- All soil/sediment/solid results are reported on a dry weight basis unless otherwise stated.
- All biota/food results are reported on a wet weight basis on the edible portion unless otherwise stated.
- For CEC results where the sample's origin is unknown or environmentally contaminated, the results should be used advisedly.
- Actual LORs are matrix dependent. Quoted LORs may be raised where sample extracts are diluted due to interferences.
- Results are uncorrected for matrix spikes or surrogate recoveries except for PFAS compounds.
- SVOC analysis on waters is performed on homogenised, unfiltered samples unless noted otherwise.
- Samples were analysed on an 'as received' basis.
- Information identified in this report with **blue** colour indicates data provided by customers that may have an impact on the results.
- This report replaces any interim results previously issued.

Holding Times

Please refer to the 'Sample Preservation and Container Guide' for holding times (QS3001).

For samples received on the last day of holding time, notification of testing requirements should have been received at least 6 hours before sample receipt deadlines as stated on the SRA.

If the Laboratory did not receive the information in the required timeframe, and despite any other integrity issues, suitably qualified results may still be reported.

Holding times apply from the date of sampling; therefore, compliance with these may be outside the laboratory's control.

For VOCs containing vinyl chloride, styrene and 2-chloroethyl vinyl ether, the holding time is 7 days; however, for all other VOCs, such as BTEX or C6-10 TRH, the holding time is 14 days.

Units

mg/kg: milligrams per kilogram	mg/L: milligrams per litre	ppm: parts per million
µg/L: micrograms per litre	ppb: parts per billion	%: Percentage
org/100 mL: Organisms per 100 millilitres	NTU: Nephelometric Turbidity Units	MPN/100 mL: Most Probable Number of organisms per 100 millilitres
CFU: Colony forming unit	Colour: Pt-Co Units	

Terms

APHA	American Public Health Association
CEC	Cation Exchange Capacity
COC	Chain of Custody
CP	Client Parent - QC was performed on samples pertaining to this report
CRM	Certified Reference Material (ISO17034) - reported as percent recovery.
Dry	Where moisture has been determined on a solid sample, the result is expressed on a dry weight basis.
Duplicate	A second piece of analysis from the same sample and reported in the same units as the result to show comparison.
LOR	Limit of Reporting.
LCS	Laboratory Control Sample - reported as percent recovery.
Method Blank	In the case of solid samples, these are performed on laboratory-certified clean sands and in the case of water samples, these are performed on de-ionised water.
NCP	Non-Client Parent - QC performed on samples not pertaining to this report, QC represents the sequence or batch that client samples were analysed within.
RPD	Relative Percent Difference between two Duplicate pieces of analysis.
SPIKE	Addition of the analyte to the sample and reported as percentage recovery.
SRA	Sample Receipt Advice
Surr - Surrogate	The addition of a similar compound to the analyte target is reported as percentage recovery. See below for acceptance criteria.
TBTO	Tributyltin oxide (<i>bis</i> -tributyltin oxide) - individual tributyltin compounds cannot be identified separately in the environment; however, free tributyltin was measured, and its values were converted stoichiometrically into tributyltin oxide for comparison with regulatory limits.
TCLP	Toxicity Characteristic Leaching Procedure
TEQ	Toxic Equivalency Quotient or Total Equivalence
QSM	US Department of Defense Quality Systems Manual Version 5.4
US EPA	United States Environmental Protection Agency
WA DWER	Sum of PFBA, PFPeA, PFHxA, PFHpA, PFOA, PFBS, PFHxS, PFOS, 6:2 FTSA, 8:2 FTSA

QC - Acceptance Criteria

The acceptance criteria should only be used as a guide and may be different when site-specific Sampling Analysis and Quality Plan (SAQP) have been implemented.

RPD Duplicates: Global RPD Duplicates Acceptance Criteria is ≤30%; however, the following acceptance guidelines are equally applicable:

Results <10 times the LOR:	No Limit
Results between 10-20 times the LOR:	RPD must lie between 0-50%
Results >20 times the LOR:	RPD must lie between 0-30%

NOTE: pH duplicates are reported as a range, not as RPD

Surrogate Recoveries: Recoveries must lie between 20-130% for Speciated Phenols & 50-150% for PFAS. SVOCs recoveries 20 – 150%, VOC recoveries 70 – 130%

PFAS field samples containing surrogate recoveries above the QC limit designated in QSM 5.4, where no positive PFAS results have been reported or reviewed, and no data was affected.

QC Data General Comments

- Where a result is reported as less than (<), higher than the nominated LOR, this is due to either matrix interference, extract dilution required due to interferences or contaminant levels within the sample, high moisture content or insufficient sample provided.
- Duplicate data shown within this report that states the word "BATCH" is a Batch Duplicate from outside of your sample batch but within the laboratory sample batch at a 1:10 ratio. The Parent and Duplicate data shown are not data from your samples.
- pH and Free Chlorine analysed in the laboratory - Analysis on this test must begin within 30 minutes of sampling. Therefore, laboratory analysis is unlikely to be completed within holding time. Analysis will begin as soon as possible after sample receipt.
- Recovery Data (Spikes & Surrogates) - where chromatographic interference does not allow the determination of recovery, the term "INT" appears against that analyte.
- For Matrix Spikes and LCS results, a dash "-" in the report means that the specific analyte was not added to the QC sample.
- Duplicate RPDs are calculated from raw analytical data; thus, it is possible to have two sets of data.

Quality Control Results

Test				Units	Result 1		Acceptance Limits	Pass Limits	Qualifying Code
Method Blank									
Chloride				mg/kg	< 10		10	Pass	
Conductivity (1:5 aqueous extract at 25 °C as rec.)				uS/cm	< 10		10	Pass	
Sulphate (as SO4)				mg/kg	< 10		10	Pass	
LCS - % Recovery									
Chloride				%	106		70-130	Pass	
Sulphate (as SO4)				%	100		70-130	Pass	
Test	Lab Sample ID	QA Source	Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Spike - % Recovery									
				Result 1					
Chloride	S23-De0005791	NCP	%	108			70-130	Pass	
Sulphate (as SO4)	S23-De0005791	NCP	%	100			70-130	Pass	
Test	Lab Sample ID	QA Source	Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Duplicate									
				Result 1	Result 2	RPD			
Conductivity (1:5 aqueous extract at 25 °C as rec.)	S23-De0003250	CP	uS/cm	58	55	4.9	30%	Pass	
pH (1:5 Aqueous extract at 25 °C as rec.)	S23-De0003250	CP	pH Units	9.5	9.4	<1	30%	Pass	
Resistivity*	S23-De0003250	CP	ohm.m	170	180	4.9	30%	Pass	
Duplicate									
				Result 1	Result 2	RPD			
% Moisture	S23-De0003256	NCP	%	20	18	8.5	30%	Pass	
Duplicate									
				Result 1	Result 2	RPD			
Chloride	S23-De0003254	CP	mg/kg	< 10	< 10	<1	30%	Pass	
Sulphate (as SO4)	S23-De0003254	CP	mg/kg	50	50	<1	30%	Pass	

Comments

Sample Integrity

Custody Seals Intact (if used)	N/A
Attempt to Chill was evident	No
Sample correctly preserved	Yes
Appropriate sample containers have been used	Yes
Sample containers for volatile analysis received with minimal headspace	Yes
Samples received within HoldingTime	Yes
Some samples have been subcontracted	No

Authorised by:

Hannah Mawbey
Ryan Phillips

Analytical Services Manager
Senior Analyst-Inorganic



Glenn Jackson
Managing Director

Final Report – this report replaces any previously issued Report

- Indicates Not Requested

* Indicates NATA accreditation does not cover the performance of this service

Measurement uncertainty of test data is available on request or please [click here](#).

Eurofins shall not be liable for loss, cost, damages or expenses incurred by the client, or any other person or company, resulting from the use of any information or interpretation given in this report. In no case shall Eurofins be liable for consequential damages including, but not limited to, lost profits, damages for failure to meet deadlines and lost production arising from this report. This document shall not be reproduced except in full and relates only to the items tested. Unless indicated otherwise, the tests were performed on the samples as received.

Appendix D:
Site Classification General Information
(CSIRO Document – BTF18)

Foundation Maintenance and Footing Performance: A Homeowner's Guide



CSIRO

BTF 18
replaces
Information
Sheet 10/91

Buildings can and often do move. This movement can be up, down, lateral or rotational. The fundamental cause of movement in buildings can usually be related to one or more problems in the foundation soil. It is important for the homeowner to identify the soil type in order to ascertain the measures that should be put in place in order to ensure that problems in the foundation soil can be prevented, thus protecting against building movement.

This Building Technology File is designed to identify causes of soil-related building movement, and to suggest methods of prevention of resultant cracking in buildings.

Soil Types

The types of soils usually present under the topsoil in land zoned for residential buildings can be split into two approximate groups – granular and clay. Quite often, foundation soil is a mixture of both types. The general problems associated with soils having granular content are usually caused by erosion. Clay soils are subject to saturation and swell/shrink problems.

Classifications for a given area can generally be obtained by application to the local authority, but these are sometimes unreliable and if there is doubt, a geotechnical report should be commissioned. As most buildings suffering movement problems are founded on clay soils, there is an emphasis on classification of soils according to the amount of swell and shrinkage they experience with variations of water content. The table below is Table 2.1 from AS 2870, the Residential Slab and Footing Code.

Causes of Movement

Settlement due to construction

There are two types of settlement that occur as a result of construction:

- Immediate settlement occurs when a building is first placed on its foundation soil, as a result of compaction of the soil under the weight of the structure. The cohesive quality of clay soil mitigates against this, but granular (particularly sandy) soil is susceptible.
- Consolidation settlement is a feature of clay soil and may take place because of the expulsion of moisture from the soil or because of the soil's lack of resistance to local compressive or shear stresses. This will usually take place during the first few months after construction, but has been known to take many years in exceptional cases.

These problems are the province of the builder and should be taken into consideration as part of the preparation of the site for construction. Building Technology File 19 (BTF 19) deals with these problems.

Erosion

All soils are prone to erosion, but sandy soil is particularly susceptible to being washed away. Even clay with a sand component of say 10% or more can suffer from erosion.

Saturation

This is particularly a problem in clay soils. Saturation creates a bog-like suspension of the soil that causes it to lose virtually all of its bearing capacity. To a lesser degree, sand is affected by saturation because saturated sand may undergo a reduction in volume – particularly imported sand fill for bedding and blinding layers. However, this usually occurs as immediate settlement and should normally be the province of the builder.

Seasonal swelling and shrinkage of soil

All clays react to the presence of water by slowly absorbing it, making the soil increase in volume (see table below). The degree of increase varies considerably between different clays, as does the degree of decrease during the subsequent drying out caused by fair weather periods. Because of the low absorption and expulsion rate, this phenomenon will not usually be noticeable unless there are prolonged rainy or dry periods, usually of weeks or months, depending on the land and soil characteristics.

The swelling of soil creates an upward force on the footings of the building, and shrinkage creates subsidence that takes away the support needed by the footing to retain equilibrium.

Shear failure

This phenomenon occurs when the foundation soil does not have sufficient strength to support the weight of the footing. There are two major post-construction causes:

- Significant load increase.
- Reduction of lateral support of the soil under the footing due to erosion or excavation.
- In clay soil, shear failure can be caused by saturation of the soil adjacent to or under the footing.

GENERAL DEFINITIONS OF SITE CLASSES

Class	Foundation
A	Most sand and rock sites with little or no ground movement from moisture changes
S	Slightly reactive clay sites with only slight ground movement from moisture changes
M	Moderately reactive clay or silt sites, which can experience moderate ground movement from moisture changes
H	Highly reactive clay sites, which can experience high ground movement from moisture changes
E	Extremely reactive sites, which can experience extreme ground movement from moisture changes
A to P	Filled sites
P	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise

Tree root growth

Trees and shrubs that are allowed to grow in the vicinity of footings can cause foundation soil movement in two ways:

- Roots that grow under footings may increase in cross-sectional size, exerting upward pressure on footings.
- Roots in the vicinity of footings will absorb much of the moisture in the foundation soil, causing shrinkage or subsidence.

Unevenness of Movement

The types of ground movement described above usually occur unevenly throughout the building's foundation soil. Settlement due to construction tends to be uneven because of:

- Differing compaction of foundation soil prior to construction.
- Differing moisture content of foundation soil prior to construction.

Movement due to non-construction causes is usually more uneven still. Erosion can undermine a footing that traverses the flow or can create the conditions for shear failure by eroding soil adjacent to a footing that runs in the same direction as the flow.

Saturation of clay foundation soil may occur where subfloor walls create a dam that makes water pond. It can also occur wherever there is a source of water near footings in clay soil. This leads to a severe reduction in the strength of the soil which may create local shear failure.

Seasonal swelling and shrinkage of clay soil affects the perimeter of the building first, then gradually spreads to the interior. The swelling process will usually begin at the uphill extreme of the building, or on the weather side where the land is flat. Swelling gradually reaches the interior soil as absorption continues. Shrinkage usually begins where the sun's heat is greatest.

Effects of Uneven Soil Movement on Structures

Erosion and saturation

Erosion removes the support from under footings, tending to create subsidence of the part of the structure under which it occurs. Brickwork walls will resist the stress created by this removal of support by bridging the gap or cantilevering until the bricks or the mortar bedding fail. Older masonry has little resistance. Evidence of failure varies according to circumstances and symptoms may include:

- Step cracking in the mortar beds in the body of the wall or above/below openings such as doors or windows.
- Vertical cracking in the bricks (usually but not necessarily in line with the vertical beds or perpend).

Isolated piers affected by erosion or saturation of foundations will eventually lose contact with the bearers they support and may tilt or fall over. The floors that have lost this support will become bouncy, sometimes rattling ornaments etc.

Seasonal swelling/shrinkage in clay

Swelling foundation soil due to rainy periods first lifts the most exposed extremities of the footing system, then the remainder of the perimeter footings while gradually permeating inside the building footprint to lift internal footings. This swelling first tends to create a dish effect, because the external footings are pushed higher than the internal ones.

The first noticeable symptom may be that the floor appears slightly dished. This is often accompanied by some doors binding on the floor or the door head, together with some cracking of cornice mitres. In buildings with timber flooring supported by bearers and joists, the floor can be bouncy. Externally there may be visible dishing of the hip or ridge lines.

As the moisture absorption process completes its journey to the innermost areas of the building, the internal footings will rise. If the spread of moisture is roughly even, it may be that the symptoms will temporarily disappear, but it is more likely that swelling will be uneven, creating a difference rather than a disappearance in symptoms. In buildings with timber flooring supported by bearers and joists, the isolated piers will rise more easily than the strip footings or piers under walls, creating noticeable doming of flooring.

Trees can cause shrinkage and damage



As the weather pattern changes and the soil begins to dry out, the external footings will be first affected, beginning with the locations where the sun's effect is strongest. This has the effect of lowering the external footings. The doming is accentuated and cracking reduces or disappears where it occurred because of dishing, but other cracks open up. The roof lines may become convex.

Doming and dishing are also affected by weather in other ways. In areas where warm, wet summers and cooler dry winters prevail, water migration tends to be toward the interior and doming will be accentuated, whereas where summers are dry and winters are cold and wet, migration tends to be toward the exterior and the underlying propensity is toward dishing.

Movement caused by tree roots

In general, growing roots will exert an upward pressure on footings, whereas soil subject to drying because of tree or shrub roots will tend to remove support from under footings by inducing shrinkage.

Complications caused by the structure itself

Most forces that the soil causes to be exerted on structures are vertical – i.e. either up or down. However, because these forces are seldom spread evenly around the footings, and because the building resists uneven movement because of its rigidity, forces are exerted from one part of the building to another. The net result of all these forces is usually rotational. This resultant force often complicates the diagnosis because the visible symptoms do not simply reflect the original cause. A common symptom is binding of doors on the vertical member of the frame.

Effects on full masonry structures

Brickwork will resist cracking where it can. It will attempt to span areas that lose support because of subsided foundations or raised points. It is therefore usual to see cracking at weak points, such as openings for windows or doors.

In the event of construction settlement, cracking will usually remain unchanged after the process of settlement has ceased.

With local shear or erosion, cracking will usually continue to develop until the original cause has been remedied, or until the subsidence has completely neutralised the affected portion of footing and the structure has stabilised on other footings that remain effective.

In the case of swell/shrink effects, the brickwork will in some cases return to its original position after completion of a cycle, however it is more likely that the rotational effect will not be exactly reversed, and it is also usual that brickwork will settle in its new position and will resist the forces trying to return it to its original position. This means that in a case where swelling takes place after construction and cracking occurs, the cracking is likely to at least partly remain after the shrink segment of the cycle is complete. Thus, each time the cycle is repeated, the likelihood is that the cracking will become wider until the sections of brickwork become virtually independent.

With repeated cycles, once the cracking is established, if there is no other complication, it is normal for the incidence of cracking to stabilise, as the building has the articulation it needs to cope with the problem. This is by no means always the case, however, and monitoring of cracks in walls and floors should always be treated seriously.

Upheaval caused by growth of tree roots under footings is not a simple vertical shear stress. There is a tendency for the root to also exert lateral forces that attempt to separate sections of brickwork after initial cracking has occurred.

The normal structural arrangement is that the inner leaf of brickwork in the external walls and at least some of the internal walls (depending on the roof type) comprise the load-bearing structure on which any upper floors, ceilings and the roof are supported. In these cases, it is internally visible cracking that should be the main focus of attention, however there are a few examples of dwellings whose external leaf of masonry plays some supporting role, so this should be checked if there is any doubt. In any case, externally visible cracking is important as a guide to stresses on the structure generally, and it should also be remembered that the external walls must be capable of supporting themselves.

Effects on framed structures

Timber or steel framed buildings are less likely to exhibit cracking due to swell/shrink than masonry buildings because of their flexibility. Also, the doming/dishing effects tend to be lower because of the lighter weight of walls. The main risks to framed buildings are encountered because of the isolated pier footings used under walls. Where erosion or saturation cause a footing to fall away, this can double the span which a wall must bridge. This additional stress can create cracking in wall linings, particularly where there is a weak point in the structure caused by a door or window opening. It is, however, unlikely that framed structures will be so stressed as to suffer serious damage without first exhibiting some or all of the above symptoms for a considerable period. The same warning period should apply in the case of upheaval. It should be noted, however, that where framed buildings are supported by strip footings there is only one leaf of brickwork and therefore the externally visible walls are the supporting structure for the building. In this case, the subfloor masonry walls can be expected to behave as full brickwork walls.

Effects on brick veneer structures

Because the load-bearing structure of a brick veneer building is the frame that makes up the interior leaf of the external walls plus perhaps the internal walls, depending on the type of roof, the building can be expected to behave as a framed structure, except that the external masonry will behave in a similar way to the external leaf of a full masonry structure.

Water Service and Drainage

Where a water service pipe, a sewer or stormwater drainage pipe is in the vicinity of a building, a water leak can cause erosion, swelling or saturation of susceptible soil. Even a minuscule leak can be enough to saturate a clay foundation. A leaking tap near a building can have the same effect. In addition, trenches containing pipes can become watercourses even though backfilled, particularly where broken rubble is used as fill. Water that runs along these trenches can be responsible for serious erosion, interstrata seepage into subfloor areas and saturation.

Pipe leakage and trench water flows also encourage tree and shrub roots to the source of water, complicating and exacerbating the problem.

Poor roof plumbing can result in large volumes of rainwater being concentrated in a small area of soil:

- Incorrect falls in roof guttering may result in overflows, as may gutters blocked with leaves etc.

- Corroded guttering or downpipes can spill water to ground.
- Downpipes not positively connected to a proper stormwater collection system will direct a concentration of water to soil that is directly adjacent to footings, sometimes causing large-scale problems such as erosion, saturation and migration of water under the building.

Seriousness of Cracking

In general, most cracking found in masonry walls is a cosmetic nuisance only and can be kept in repair or even ignored. The table below is a reproduction of Table C1 of AS 2870.

AS 2870 also publishes figures relating to cracking in concrete floors, however because wall cracking will usually reach the critical point significantly earlier than cracking in slabs, this table is not reproduced here.

Prevention/Cure

Plumbing

Where building movement is caused by water service, roof plumbing, sewer or stormwater failure, the remedy is to repair the problem. It is prudent, however, to consider also rerouting pipes away from the building where possible, and relocating taps to positions where any leakage will not direct water to the building vicinity. Even where gully traps are present, there is sometimes sufficient spill to create erosion or saturation, particularly in modern installations using smaller diameter PVC fixtures. Indeed, some gully traps are not situated directly under the taps that are installed to charge them, with the result that water from the tap may enter the backfilled trench that houses the sewer piping. If the trench has been poorly backfilled, the water will either pond or flow along the bottom of the trench. As these trenches usually run alongside the footings and can be at a similar depth, it is not hard to see how any water that is thus directed into a trench can easily affect the foundation's ability to support footings or even gain entry to the subfloor area.

Ground drainage

In all soils there is the capacity for water to travel on the surface and below it. Surface water flows can be established by inspection during and after heavy or prolonged rain. If necessary, a grated drain system connected to the stormwater collection system is usually an easy solution.

It is, however, sometimes necessary when attempting to prevent water migration that testing be carried out to establish watertable height and subsoil water flows. This subject is referred to in BTF 19 and may properly be regarded as an area for an expert consultant.

Protection of the building perimeter

It is essential to remember that the soil that affects footings extends well beyond the actual building line. Watering of garden plants, shrubs and trees causes some of the most serious water problems.

For this reason, particularly where problems exist or are likely to occur, it is recommended that an apron of paving be installed around as much of the building perimeter as necessary. This paving

CLASSIFICATION OF DAMAGE WITH REFERENCE TO WALLS		
Description of typical damage and required repair	Approximate crack width limit (see Note 3)	Damage category
Hairline cracks	<0.1 mm	0
Fine cracks which do not need repair	<1 mm	1
Cracks noticeable but easily filled. Doors and windows stick slightly	<5 mm	2
Cracks can be repaired and possibly a small amount of wall will need to be replaced. Doors and windows stick. Service pipes can fracture. Weathertightness often impaired	5–15 mm (or a number of cracks 3 mm or more in one group)	3
Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Window and door frames distort. Walls lean or bulge noticeably, some loss of bearing in beams. Service pipes disrupted	15–25 mm but also depend on number of cracks	4



- Water that is transmitted into masonry, metal or timber building elements causes damage and/or decay to those elements.
- High subfloor humidity and moisture content create an ideal environment for various pests, including termites and spiders.
- Where high moisture levels are transmitted to the flooring and walls, an increase in the dust mite count can ensue within the living areas. Dust mites, as well as dampness in general, can be a health hazard to inhabitants, particularly those who are abnormally susceptible to respiratory ailments.

The garden

The ideal vegetation layout is to have lawn or plants that require only light watering immediately adjacent to the drainage or paving edge, then more demanding plants, shrubs and trees spread out in that order.

Overwatering due to misuse of automatic watering systems is a common cause of saturation and water migration under footings. If it is necessary to use these systems, it is important to remove garden beds to a completely safe distance from buildings.

Existing trees

Where a tree is causing a problem of soil drying or there is the existence or threat of upheaval of footings, if the offending roots are subsidiary and their removal will not significantly damage the tree, they should be severed and a concrete or metal barrier placed vertically in the soil to prevent future root growth in the direction of the building. If it is not possible to remove the relevant roots without damage to the tree, an application to remove the tree should be made to the local authority. A prudent plan is to transplant likely offenders before they become a problem.

Information on trees, plants and shrubs

State departments overseeing agriculture can give information regarding root patterns, volume of water needed and safe distance from buildings of most species. Botanic gardens are also sources of information. For information on plant roots and drains, see Building Technology File 17.

Excavation

Excavation around footings must be properly engineered. Soil supporting footings can only be safely excavated at an angle that allows the soil under the footing to remain stable. This angle is called the angle of repose (or friction) and varies significantly between soil types and conditions. Removal of soil within the angle of repose will cause subsidence.

Remediation

Where erosion has occurred that has washed away soil adjacent to footings, soil of the same classification should be introduced and compacted to the same density. Where footings have been undermined, augmentation or other specialist work may be required. Remediation of footings and foundations is generally the realm of a specialist consultant.

Where isolated footings rise and fall because of swell/shrink effect, the homeowner may be tempted to alleviate floor bounce by filling the gap that has appeared between the bearer and the pier with blocking. The danger here is that when the next swell segment of the cycle occurs, the extra blocking will push the floor up into an accentuated dome and may also cause local shear failure in the soil. If it is necessary to use blocking, it should be by a pair of fine wedges and monitoring should be carried out fortnightly.

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should extend outwards a minimum of 900 mm (more in highly reactive soil) and should have a minimum fall away from the building of 1:60. The finished paving should be no less than 100 mm below brick vent bases.

It is prudent to relocate drainage pipes away from this paving, if possible, to avoid complications from future leakage. If this is not practical, earthenware pipes should be replaced by PVC and backfilling should be of the same soil type as the surrounding soil and compacted to the same density.

Except in areas where freezing of water is an issue, it is wise to remove taps in the building area and relocate them well away from the building – preferably not uphill from it (see BTF 19).

It may be desirable to install a grated drain at the outside edge of the paving on the uphill side of the building. If subsoil drainage is needed this can be installed under the surface drain.

Condensation

In buildings with a subfloor void such as where bearers and joists support flooring, insufficient ventilation creates ideal conditions for condensation, particularly where there is little clearance between the floor and the ground. Condensation adds to the moisture already present in the subfloor and significantly slows the process of drying out. Installation of an adequate subfloor ventilation system, either natural or mechanical, is desirable.

Warning: Although this Building Technology File deals with cracking in buildings, it should be said that subfloor moisture can result in the development of other problems, notably:

The information in this and other issues in the series was derived from various sources and was believed to be correct when published.

The information is advisory. It is provided in good faith and not claimed to be an exhaustive treatment of the relevant subject.

Further professional advice needs to be obtained before taking any action based on the information provided.

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