

D. Katauskas

Consulting Geotechnical Engineer

Katauskas Family Trust T/A D.Katauskas Geotechnical Consultant
ABN 59 442 991 347

**127B Campbell Drive
Wahroonga NSW 2076
Phone: 02 9489 6341
Mob: 0409 727 831
email: dkatauskas@gmail.com**

21 December 2016
Ref: 1055-A

MCK Architecture & Interiors
Studio 401/ 104 Commonwealth Street
Surry Hills NSW 2010

Attention: Kim Saggars

Dear Kim,

Re: Geotechnical Investigation Pursuant to DA
Proposed Commercial Development
49 - 51 Arthur Street
Forestville NSW

This report presents the results of the above investigation, the purpose of which was to determine the nature of the subsurface soil, rock and groundwater conditions in order to address geotechnical matters pertaining to the proposed development, which is understood to comprise several above-ground levels over a basement carpark.

Comments and recommendations on the following geotechnical matters are presented herein:

- Excavation conditions
- Excavation support requirements
- Earth pressures on basement walls
- Suitable foundation schemes and bearing pressures
- Basement groundwater control

Investigation Method

The subsurface conditions were investigated by augering three boreholes, the locations of which are shown on the attached Figure 1, to practical refusal in the underlying sandstone bedrock. Due to the restricted access conditions, a relatively small and lightweight drill rig was used.

The fieldwork for the investigation was carried out on the 13 December 2016 under the fulltime supervision of the undersigned.

Investigation Findings

The investigation disclosed relatively straightforward subsurface conditions comprised of shallow fill or natural sandy layer ranging in thickness from approximately 0.5 to 0.7 metres, and thereafter sandstone bedrock.

Auger refusal was encountered at each borehole, at depths varying from about 1.6 to 3.0 metres below existing ground surface. Given the size and power capability of the drillrig used for this investigation, auger refusal was interpreted to occur upon encountering sandstone in the medium strength range.

No groundwater was encountered during the investigation.

Reference should be made to the attached Borehole Logs and Explanatory Notes for a detailed description and sequence of the subsurface conditions encountered.

Comments and Recommendations

Excavation Conditions

Following the removal of the relatively shallow sandy soil layer, excavation of the sandstone to an estimated depth of approximately 3.5m to 4m should be achievable, mostly by ripping using a D-10 size dozer or equivalent, assisted by rock sawing at the boundaries and the use of a medium size hydraulic rock breaker for trimming and detailed excavations.

As previously noted, the boreholes were terminated within sandstone bedrock estimated to be of medium strength. The possibility of a stronger layer occurring with depth should not be excluded, as strength variations are considered to be common.

Excavation vibrations are unavoidable and it is recommended that they be monitored. As a guide, it is recommended that a threshold peak particle velocity of 8cm/sec be not exceeded when measured at the site boundaries.

Excavation Support

Unsupported vertical excavation faces may be used for the sandstone, while shoring support will need to be provided to all vertical excavation faces through the soil cover. If space permits, temporary batter slopes of 1H:1.5V may be used.

Earth Pressure on Basement Walls

An earth pressure coefficient k of 0.4 may be used for the shallow sandy layer. Any horizontal pressure effects from the sandstone could be ignored; that is, $k = 0$.

Building Foundations

There appears to be no rational alternative but to transfer the building loads to the sandstone bedrock. For design purposes, an allowable bearing pressure of 3000 kPa may be used.

Basement Drainage

Some groundwater seepage into the basement should be expected, and such seepage may be controlled by normal sump and pump operations.

If you have any queries regarding the above, please do not hesitate to call me.

Regards,



Don Katauskas

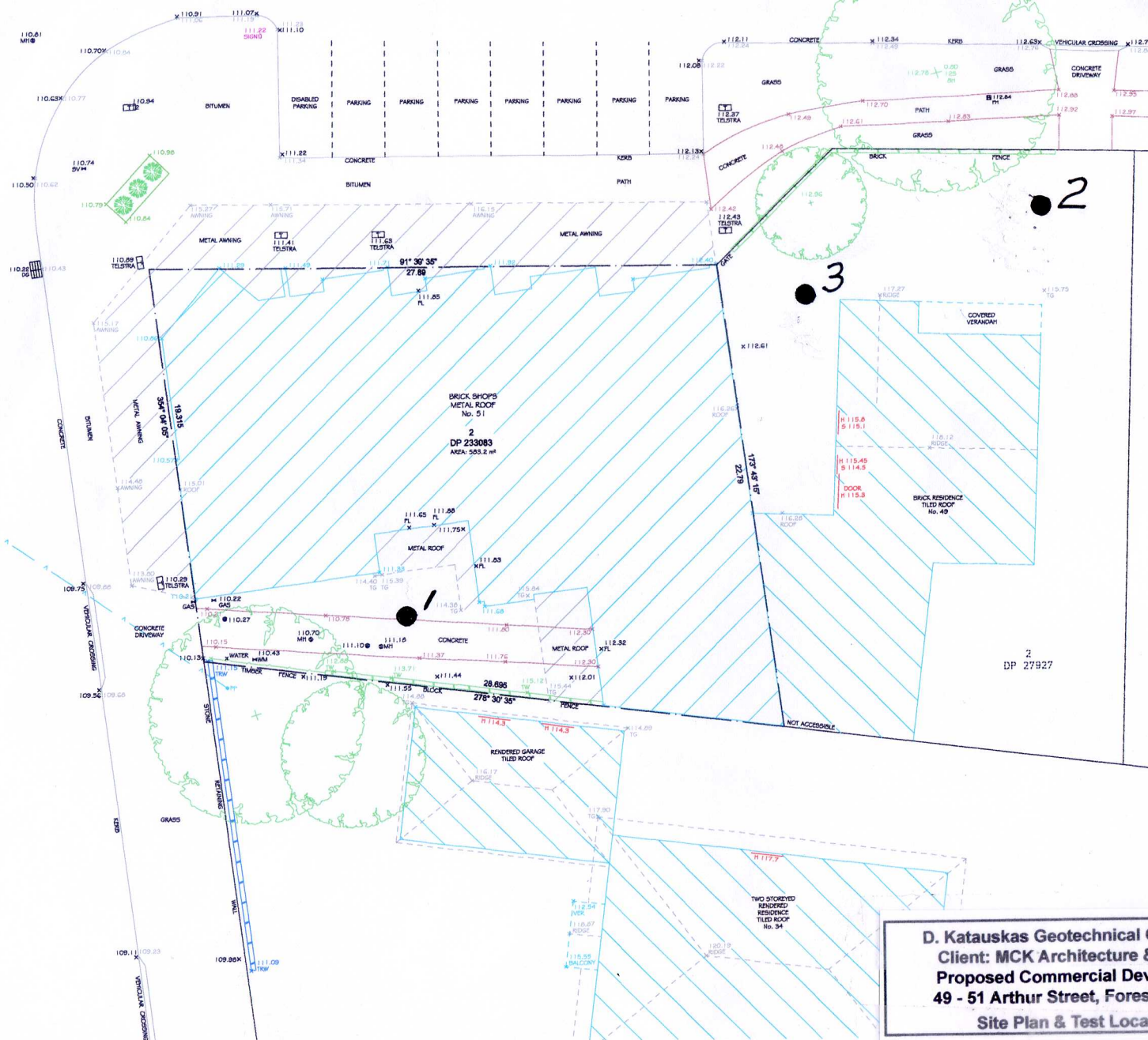
encl: Figure 1 – Site Plan & Test Locations
Borehole Logs 1 and 2
Explanatory Notes



DUKE STREET

LEGEND

- 0-DIAMETER
- 5-SPREAD
- 10-INSPECTION OPENING
- LIGHT POLE
- SIGN
- STORMWATER PIT
- SEWER MANHOLE
- POWER POLE
- + (TQ) TOP GUTTER
- x SPOT HEIGHT
- x (FL) FLOOR LEVEL
- x (TWFT) TOP WALKTOP FENCE
- x (TRM) TOP RETAINING WALL
- x (BRO) BASE ROCK OUTCROP
- x (TRO) TOP ROCK OUTCROP
- x (THRU) TOP HAND RAIL
- ◇ VALVE



D. Katauskas Geotechnical Consultant
Client: MCK Architecture & Interiors
Proposed Commercial Development
49 - 51 Arthur Street, Forestville NSW
Site Plan & Test Locations

JOB NO. 1055-A
FIGURE NO: 1

TEST LOCATION: ●

AMENDMENTS:

POSITION OF IMPROVEMENTS RELATIVE TO BOUNDARIES ARE SHOWN DIAGNOSTICALLY AND HAVE BEEN SURVEYED FOR DA PURPOSES ONLY. ALL BOUNDARY DIMENSIONS & AREA HAVE BEEN COMPILED FROM TITLE INFORMATION ONLY AND ARE SUBJECT TO FINAL SURVEY. THE POSITION AND LEVELS OF ADJOINING BUILDINGS, WINDOWS, ROOF, GUTTERS AND TREES HAVE BEEN SURVEYED REMOTELY. NO INVESTIGATION OF UNDERGROUND SERVICES HAS BEEN MADE. RELEVANT AUTHORITIES ARE TO BE NOTIFIED PRIOR TO ANY DEVELOPMENT. SERVICES SHOWN HEREON HAVE BEEN DETERMINED FROM VISUAL EVIDENCE ONLY. AUSTRALIAN HEIGHT DATUM WAS ESTABLISHED FROM SDM 1345 (RL 113.862) AND IT IS ADVISED, FOR CONSTRUCTION WORKS FROM BOUNDARIES, THAT BOUNDARIES BE MARKED ON THE GROUND PRIOR TO CONSTRUCTION. THE BOUNDARY DIMENSIONS ON THIS PLAN HAVE BEEN COMPILED FROM LAND & PROPERTY INFORMATION PLAN DP 233083.

ERIC SCERRI & ASSOCIATES PTY LTD
 LAND SURVEY CONSULTANTS
 P.O. BOX 3010 TAMARAMA 2026

Ph (02) 9386 4161 Mob 0417 492 852 Fax (02) 9386 4171

CLIENT: SAM GABRIELIAN G. MCK ARCHITECTURE
 PLAN SHOWING: DETAIL & LEVEL SURVEY
 PROPERTY: 51 ARTHUR STREET FORESTVILLE
 LG: NORTHERN BEACHES















SURVEYED: MSW	SCALE: A1 @ 1:100
DRAWN: MD	PLAN REFERENCE: 3045/16
DATUM: AHD	DATE OF SURVEY: 23 MAY 2016
SITE AREA: 563.2 m ²	SHEET 1 OF 1
COPYRIGHT	

BOREHOLE LOG

D. Katauskas

Consulting Geotechnical Engineer

No: 1

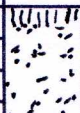
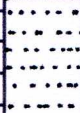
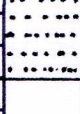
Client: MCK Architecture & Interiors						Date: 13/ 12/ 2016				
Project: Proposed Development						Job No: 1055				
Location: 49-51 Arthur Street, Forestville NSW										
Method: Landcruiser Drill Rig						RL: 111.2m Approx.		Logged: DK		Checked : DK
						Datum: AHD				
Groundwater Record	Sample	Field Tests	Depth (m)	Graphic Log	Unified Classification	Description	Moisture Condition / Weathering	Strength/ Relative Density	Hand Penetrometer Readings (kPa)	Remarks
DR						FILL: gravelly sand grey				
			1			SANDSTONE: light grey	DN	VL		
			2			as above light brown		L		
			3					L		
								L		
								L		
								L		
								L		
								L		
								L		
								L		
								L		
								L		
								L		
			4			END BHO 3.0m				
						(Refusal)				
			5							
			6							
			7							
			8							

BOREHOLE LOG

D. Katauskas

Consulting Geotechnical Engineer

No: 2

Client: MCK Architecture & Interiors						Date: 13/ 12/ 2016								
Project: Proposed Development						Job No: 1055								
Location: 49-51 Arthur Street, Forestville NSW														
Method: Landcruiser Drill Rig						RL: 113.0m Approx.			Logged: DK			Checked : DK		
						Datum: AHD								
Groundwater Record	Sample	Field Tests	Depth (m)	Graphic Log	Unified Classification	Description	Moisture Condition / Weathering	Strength/ Relative Density	Hand Penetrometer Readings (kPa)	Remarks				
DRY					SP	Topsoil over sand light grey then light brown	D	L						
			1			SANDSTONE: light grey	DW	L						
			2					L						
						END BHC 2.0m (Refusal)								
			3											
			4											
			5											
			6											
			7											
			8											

BOREHOLE LOG

D. Katauskas

Consulting Geotechnical Engineer

No: 3

Client: MCK Architecture & Interiors						Date: 13/ 12/ 2016				
Project: Proposed Development						Job No: 1055				
Location: 49-51 Arthur Street, Forestville NSW										
Method: Landcruiser Drill Rig						RL: 113.0m Approx.		Logged: DK		Checked : DK
						Datum: AHD				
Groundwater Record	Sample	Field Tests	Depth (m)	Graphic Log	Unified Classification	Description	Moisture Condition / Weathering	Strength/ Relative Density	Hand Penetrometer Readings (kPa)	Remarks
Dry			1		SP	SAND: fine to medium grained brown		L		
						SANDSTONE: light brown	DW	L to M		
			2			END BHC 1.5m (Retard)				
			3							
			4							
			5							
			6							
			7							
			8							


































D. Katauskas

Consulting Geotechnical Engineer

LOG SYMBOLS

LOG COLUMN	SYMBOL	DEFINITION
Groundwater Record	▼ ►	Standing water level. Time delay following completion of drilling may be shown. Groundwater seepage into borehole or excavation noted during drilling or excavation.
Samples	ES U50 DB DS	Soil sample taken over depth indicated, for environmental analysis. Undisturbed 50mm diameter tube sample taken over depth indicated. Bulk disturbed sample taken over depth indicated Small disturbed bag sample taken over depth indicated.
Field Tests	N = 17 4, 7, 10 N _c = 5 7 3R VNS = 25 PID = 100	Standard Penetration Test (SPT) performed between depths indicated by lines. Individual figures show blows per 150mm penetration. 'R' noted below Dynamic Cone Penetration Test performed between depths indicated by lines. Individual figures show blows per 150mm penetration for 60 degree solid cone driven by SPT hammer. 'R' refers to apparent hammer refusal within the corresponding 150mm depth increment. Vane shear reading in kPa of Undrained Shear Strength Photoionization detector reading in ppm (Soil sample headspace test)
Moisture Condition (Cohesive Soils) (Cohesionless Soils)	MC > PL MC = PL MC < PL D M W	Moisture content estimated to be greater than plastic limit. Moisture content estimated to be approximately equal to plastic limit. Moisture content estimated to be less than plastic limit. DRY - runs freely through fingers MOIST - does not run freely but no free water visible on soil surface WET - free water visible on soil surface.
Strength (Consistency) Cohesive Soils	VS S F St VSt H ()	VERY SOFT - Unconfined compressive strength less than 25 kPa. SOFT - Unconfined compressive strength 25 – 50 kPa. FIRM - Unconfined compressive strength 50 – 100 kPa STIFF - Unconfined compressive strength 100 – 200 kPa VERY STIFF - Unconfined compressive strength 200 – 400 kPa HARD - Unconfined compressive strength greater than 400 kPa. Bracketted symbol indicates estimated consistency based on tactile examination or other tests.
Density Index/ Relative density (Cohesionless Soils)	VL L MD D VD ()	Density Index (I _D) Range (%) SPT 'N' Value range (Blows/ 300mm) Very loose <15 0 – 4 Loose 15 – 35 4 – 10 Medium Dense 35 – 65 10 – 30 Dense 65 – 85 30 – 50 Very Dense >85 >50 Bracketted symbol indicates estimated density based on ease of drilling or other tests
Hand Penetrometer Readings	300 250	Numbers indicate individual test results in kPa on representative undisturbed material unless noted otherwise.
Remarks	'V' bit 'TC' bit T 60	Hardened steel 'V' bit Tungsten carbide wing bit Penetration of auger string in mm under static load of rig applied by drill head hydraulics without rotation of augers.

GRAPHIC LOG SYMBOLS FOR SOILS AND ROCKS

SOIL	ROCK	DEFECTS AND INCLUSIONS
 FILL	 CONGLOMERATE	 CLAY SEAM
 TOPSOIL	 SANDSTONE	 SHEARED OR CRUSHED SEAM
 CLAY (CL, CH)	 SHALE	 BRECCIATED OR SHATTERED SEAM/ZONE
 SILT (ML, MH)	 SILTSTONE, MUDSTONE, CLAYSTONE	 IRONSTONE GRAVEL
 SAND (SP, SW)	 LIMESTONE	 ORGANIC MATERIAL
 GRAVEL (GP, GW)	 PHYLLITE, SCHIST	
 SANDY CLAY (CL, CH)	 TUFF	OTHER MATERIALS
 SILTY CLAY (CL, CH)	 GRANITE, GABBRO	 CONCRETE
 CLAYEY SAND (SC)	 DOLERITE, DIORITE	 BITUMINOUS CONCRETE, COAL
 SILTY SAND (SM)	 BASALT, ANDESITE	 COLLUVIUM
 GRAVELLY CLAY (CL, CH)	 QUARTZITE	
 CLAYEY GRAVEL (GC)		
 SANDY SILT (ML)		
 PEAT AND ORGANIC SOILS		

Rock Description

Explanatory Sheet

D. Katauskas

Consulting Geotechnical Engineer

Classification of Weathering		
Term	Abbr:	Definition
Residual Soil	RS	Soil derived from rock weathering; mass structure & substance no longer evident. Large change in volume, soil not significantly transported.
Extremely Weathered	XW	Weathered to the extent of having soil properties i.e. disintegrates or can be remoulded in water. Original rock fabric still visible.
Distinctly Weathered	DW	Rock strength usually changed by weathering. May be highly discoloured, usually by iron staining. Porosity may be increased by leaching or decreased by deposition of weathering products in pores.
Slightly Weathered	SW	Rock slightly discoloured; shows little or no change in strength from fresh rock.
Fresh Rock	FR	Shows no evidence of decomposition or staining.

Notes:

The unconfined compressive strength is typically 10 to 25 times the point load index for homogeneous isotropic rocks.

The ratio may vary for different rock types

Rock Substance Strength Terms			
Term	Abbr:	Point Load Index I_{s50} (Mpa)	Strength Field Guide
Very Low	VL	less than 0.1	Crumbles under firm blows with sharp end of pick; can be peeled with knife. Too hard to cut triaxial sample by hand. Pieces up to 30mm thick, can be broken by finger pressure.
Low	L	0.1 to 0.3	Easily scored with a knife, indentations 1mm to 3 mm show in specimen with firm blows of the pick point, has dull sound under hammer. A piece of core, 150mm long by 50mm diameter, may be broken by hand. Sharp edges of core may be friable.
Medium	M	0.3 to 1	Readily scored with knife. Core 150mm by 50mm diameter can be broken by hand with difficulty.
High	H	1 to 3	A piece of core 150mm long by 50mm diameter cannot be broken by a pick with a single firm blow. Rock rings under hammer.
Very High	VH	3 to 10	Hand specimen breaks with pick after more than one blow. Rock rings under hammer.
Extremely High	EH	More than 10	Specimen requires many blows with geological pick to break through intact material. Rock rings under hammer.

UNIFIED SOIL CLASSIFICATION TABLE

Field Identification Procedures (Excluding particles larger than 75 μm and basing fractions on estimated weights)				Group Symbols	Typical Names	Information Required for Describing Soils	Laboratory Classification Criteria		
Coarse-grained soils More than half of material is larger than 75 μm sieve size (The 75 μm sieve size is about the smallest particle visible to naked eye)	Gravels More than half of coarse fraction is larger than 4 mm sieve size	Clean gravels (little or no fines)	Wide range in grain size and substantial amounts of all intermediate particle sizes	GW	Well graded gravels, gravel-sand mixtures, little or no fines	Give typical name; indicate approximate percentages of sand and gravel; maximum size; angularity, surface condition, and hardness of the coarse grains; local or geologic name and other pertinent descriptive information; and symbols in parentheses For undisturbed soils add information on stratification, degree of compactness, cementation, moisture conditions and drainage characteristics Example: Silty sand, gravelly; about 20% hard, angular gravel particles 12 mm maximum size; rounded and subangular sand grains coarse to fine, about 15% non-plastic fines with low dry strength; well compacted and moist in place; alluvial sand: (SM)	$C_u = \frac{D_{60}}{D_{10}}$ Greater than 4 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3 Not meeting all gradation requirements for GW		
			Predominantly one size or a range of sizes with some intermediate sizes missing	GP	Poorly graded gravels, gravel-sand mixtures, little or no fines				
		Gravels with fines (appreciable amount of fines)	Nonplastic fines (for identification procedures see ML below)	GM	Silty gravels, poorly graded gravel-sand-silt mixtures			Atterberg limits below "A" line, or PI less than 4 Above "A" line with PI between 4 and 7 are borderline cases requiring use of dual symbols	
	Plastic fines (for identification procedures, see CL below)		GC	Clayey gravels, poorly graded gravel-sand-clay mixtures	Atterberg limits above "A" line, with PI greater than 7				
	Sands More than half of coarse fraction is smaller than 4 mm sieve size	Clean sands (little or no fines)	Wide range in grain sizes and substantial amounts of all intermediate particle sizes	SW			Well graded sands, gravelly sands, little or no fines	$C_u = \frac{D_{60}}{D_{10}}$ Greater than 6 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3 Not meeting all gradation requirements for SW	
			Predominantly one size or a range of sizes with some intermediate sizes missing	SP	Poorly graded sands, gravelly sands, little or no fines		Atterberg limits below "A" line or PI less than 5 Above "A" line with PI between 4 and 7 are borderline cases requiring use of dual symbols		
Sands with fines (appreciable amount of fines)		Nonplastic fines (for identification procedures, see ML below)	SM	Silty sands, poorly graded sand-silt mixtures	Atterberg limits below "A" line with PI greater than 7				
	Plastic fines (for identification procedures, see CL below)	SC	Clayey sands, poorly graded sand-clay mixtures						
Identification Procedures on Fraction Smaller than 380 μm Sieve Size									
Fine-grained soils More than half of material is smaller than 75 μm sieve size (The 75 μm sieve size is about the smallest particle visible to naked eye)	Silt and clays liquid limit less than 50	Dry Strength (crushing characteristics)	Dilatancy (reaction to shaking)	Toughness (consistency near plastic limit)	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with slight plasticity	Give typical name; indicate degree and character of plasticity, amount and maximum size of coarse grains; colour in wet condition, odour if any, local or geologic name, and other pertinent descriptive information, and symbol in parentheses For undisturbed soils add information on structure, stratification, consistency in undisturbed and remoulded states, moisture and drainage conditions Example: Clayey silt, brown; slightly plastic; small percentage of fine sand; numerous vertical root holes; firm and dry in place; loess: (ML)		
		None to slight	Quick to slow	None				CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays
		Medium to high	None to very slow	Medium					
	Silt and clays liquid limit greater than 50	Slight to medium	Slow	Slight	OL	Organic silts and organic silts of low plasticity			
		Slight to medium	Slow to none	Slight to medium	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts			
		High to very high	None	High	CH	Inorganic clays of high plasticity, fat clays			
		Medium to high	None to very slow	Slight to medium	OH	Organic clays of medium to high plasticity			
		Highly Organic Soils				PI		Peat and other highly organic soils	

Determine percentages of gravel and sand from grain size curve

Depending on percentage of fines (fraction smaller than 75 μm sieve size) coarse grained soils are classified as follows:
Less than 5% GW, GP, SW, SP
More than 12% GM, GC, SM, SC
Borderline cases requiring use of dual symbols

Use grain size curve in identifying the fractions as given under field identification

Plasticity index

Comparing soils at equal liquid limit

Toughness and dry strength increase with increasing plasticity index

A line

CH

CL

OL

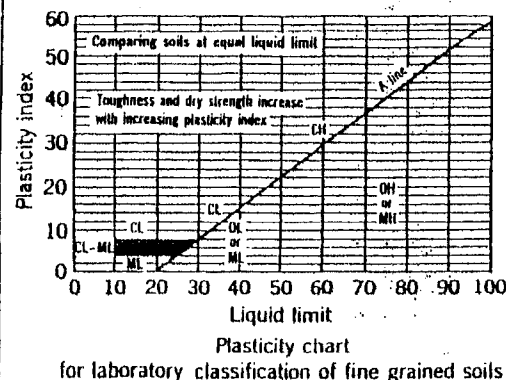
MH

OH

ML

Liquid limit

Plasticity chart for laboratory classification of fine grained soils



NOTE: 1) Soils possessing characteristics of two groups are designated by combinations of group symbols (e.g. GW-GC, well graded gravel-sand mixture with clay fines).

2) Soils with liquid limits of the order of 35 to 50 may be visually classified as being of medium plasticity.