GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Deve	elopment Application	T	
		Name of Applicant	
Addı	ress of site	40 Bilwara Avenue Bilgola Plateau	
		the minimum requirements to be addressed in a Geotechnical Risk Declaration made by gineering geologist or coastal engineer (where applicable) as part of a geotechnical re	report
Ι,	Ben White	on behalf of White Geotechnical Group Pty Ltd	
	(Insert Name)	(Trading or Company Name)	

on this the <u>3/7/20</u> certify that I am a geotechnical engineer or engineering geologist or coastal engineer as defined by the Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the above organisation/company to issue this document and to certify that the organisation/company has a current professional indemnity policy of at least \$10million.

I:

Please mark appropriate box

- have prepared the detailed Geotechnical Report referenced below in accordance with the Australia Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
- am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater 2009
- have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.
- have examined the site and the proposed development/alteration in detail and I am of the opinion that the Development Application only involves Minor Development/Alteration that does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
- have examined the site and the proposed development/alteration is separate from and is not affected by a Geotechnical Hazard and does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater 2009 requirements.
- have provided the coastal process and coastal forces analysis for inclusion in the Geotechnical Report

Geotechnical Report Details:

Report Title: Geotechnical Report 40 Bilwara Avenue Bilgola Plateau

Report Date: 3/7/20

Author: **BEN WHITE**

Author's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD

Documentation which relate to or are relied upon in report preparation:

Australian Geomechanics Society Landslide Risk Management March 2007.

White Geotechnical Group company archives.

I am aware that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a Development Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	Select
Name	Ben White
Chartered Professional Sta	tus MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Pty Ltd

GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

	Nonment Application for	
2010	Name of Application for	
Addr	ress of site 40 Bilwara Avenue Bilgola Plateau	
	llowing checklist covers the minimum requirements to be addressed in a Geotechnical Risk Management Ge t. This checklist is to accompany the Geotechnical Report and its certification (Form No. 1).	eotechnical
	chnical Report Details:	
керо	ort Title: Geotechnical Report 40 Bilwara Avenue Bilgola Plateau	
Repo	ort Date: 3/7/20	
Autho	or: BEN WHITE	
Auth	or's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD	
Auto	or s companyorganisation. White Georechnicae Groop PTT ETD	
lease	e mark appropriate box	
\boxtimes	Comprehensive site mapping conducted 23/06/20 (date)	
\leq	Mapping details presented on contoured site plan with geomorphic mapping to a minimum scale of 1:200 (as a	opropriate)
\triangleleft	Subsurface investigation required	
	 □ No Justification ☑ Yes Date conducted 23/06/20 	
3	Yes Date conducted <u>23/06/20</u> Geotechnical model developed and reported as an inferred subsurface type-section	
3	Geotechnical model developed and reported as an interred substituace type-section	
2	□ Above the site	
	\boxtimes On the site	
	⊠ Below the site	
	Beside the site	
\triangleleft	Geotechnical hazards described and reported	
\triangleleft	Risk assessment conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009	
	☑ Consequence analysis	
	☑ Frequency analysis	
\leq	Risk calculation	
\triangleleft	Risk assessment for property conducted in accordance with the Geotechnical Risk Management Policy for Pitty	
\leq	Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pit	
\leq	Assessed risks have been compared to "Acceptable Risk Management" criteria as defined in the Geotechnical	Risk
\triangleleft	Management Policy for Pittwater - 2009 Opinion has been provided that the design can achieve the "Acceptable Risk Management" criteria provided that	at the
	specified conditions are achieved.	
3	Design Life Adopted:	
	⊠ 100 years	
	□ Other	
	specify Geotechnical Conditions to be applied to all four phases as described in the Geotechnical Risk Management Po Pittwater - 2009 have been specified	olicy for
\triangleleft		
3	Additional action to remove risk where reasonable and practical have been identified and included in the report.	

I am aware that Pittwater Council will rely on the Geotechnical Report, to which this checklist applies, as the basis for ensuring that the geotechnical risk management aspects of the proposal have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated, and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	felit
Name	Ben White
Chartered Professional Sta	atus MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Pty Ltd



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GEOTECHNICAL INVESTIGATION:

Alterations and Additions at 40 Bilwara Avenue, Bilgola Plateau.

1. Proposed Development

- 1.1 Construct a rumpus room on the downhill side of the house below the existing deck by excavating to a maximum depth of ~1.3m
- **1.2** Demolish and replace the existing deck.
- **1.3** Details of the proposed development are shown on 4 drawings prepared by Jo Willmore Designs, drawings numbered DA-01 to DA-04, dated June 2020.

2. Site Description

2.1 The site was inspected on the 23rd of June, 2020.

2.2 This residential property is on the low side of the road and has a NE aspect. It is located on the moderately graded upper reaches of a hillslope. The natural slope falls at an average angle of ~9° from the uphill boundary of the property to a ~2m outcropping sandstone bedrock rock face located a short distance below the house. Below the rock face the natural slope continues at an angle of ~12°. The slope above the property decreases in grade and the slope below the property increases in grade.

2.3 At the road frontage a concrete driveway runs to the existing house (Photo 1). The cut for the driveway and house is supported by stable low sandstone block and concrete block retaining walls. The two storey rendered brick house is supported by brick walls and brick piers (Photos 1 & 2). The supporting walls and piers stand vertical and show no significant signs of movement (Photo 3). A timber deck extends off the downhill side of the house and will be replaced as part of the proposed works (Photo 2). Fill provides level lawn areas on the downhill side of the house stack (Photos 4 & 5). The fill is supported by stable low sandstone block and sandstone stack



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rock retaining walls. Medium Strength Sandstone bedrock outcrops between the upper and lower lawn (Photo 6). The rock face is ~2m high and is in good condition. No signs of slope instability were observed on the property. The adjoining neighbouring properties were observed to be in good order as seen from the street and subject property

3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by Hawkesbury Sandstone. It is described as a medium to coarse grained quartz sandstone with very minor shale and laminite lenses.

4. Subsurface Investigation

One auger hole was put down to identify the soil materials. Three Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil and the depth to weathered rock. The locations of the tests are shown on the site plan. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural rock surface. This is not expected to be an issue for the testing on this site. But due to the possibility that the actual ground conditions vary from our interpretation there should be allowances in the excavation and foundation budget to account for this. We refer to the appended "Important Information about Your Report" to further clarify. The results are as follows:

TEST RESULTS ON NEXT PAGE



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AUGER HOLE 1 (~RL108.4) – AH1 (photo 7)

Depth (m)	Material Encountered
0.0 to 0.1	TOPSOIL, sandy soil, dark brown, fine to medium grained, damp with
	fine trace organic matter.
0.1 to 0.7	SAND, grey and orange, medium grained, damp.
0.7 to 1.1	CLAYEY SAND, derived from very low strength sandstone, orange
	brown and light grey, medium to course grained, damp.

Refusal @ 1.1m auger grinding on rock. No watertable encountered.

DCP TEST RESULTS – Dynamic Cone Penetrometer				
Equipment: 9kg ham	mer, 510mm drop, conical tip.		Standard: AS1289.6.3.2 - 1997	
Depth(m) Blows/0.3m	DCP 1 (~RL107.1)	DCP 2 (~RL107.0)	DCP 3 (~RL108.4)	
0.0 to 0.3	14	7	4	
0.3 to 0.6	40	4	4	
0.6 to 0.9	12	#	5	
0.9 to 1.2	10		18	
1.2 to 1.5	12		#	
1.5 to 1.8	#			
	Refusal @ 1.4m	Refusal @ 0.4m	Refusal @ 1.1m	

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

DCP Notes:

- DCP1 Refusal @ 1.4m, DCP bouncing, light brown sand on wet tip.
- DCP2 Refusal @ 0.4m, DCP bouncing, white and brown impact dust on moist tip.
- DCP3 Refusal @ 1.1m, DCP bouncing, light brown sand on wet tip.

5. **Geological Observations/Interpretation**

The surface features of the block are controlled by the underlying sandstone bedrock that steps down the property forming sub-horizontal benches between the steps. Where the

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grade is steeper, the steps are larger and the benches narrower. Where the slope eases, the opposite is true. The rock is overlain by fill, sandy soil, sand and clayey sand that fills the bench step formation. Fill provides level lawn areas on the downhill side of the property. In the test locations, the depth to rock ranged to depths of between ~0.4 to ~1.4m below the current surface. The sandstone underlying the property is estimated to be Medium Strength or better. See Type Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and through the cracks in the rock.

Due to the slope and elevation of the block, the water table in the location is expected to be many metres below the proposed works.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. Normal sheet wash from the slope above will be intercepted by the street drainage system for Bilwara Avenue above.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed above or beside the property. The moderate slope that falls across the property and continues below is a potential hazard (**Hazard One**). The proposed excavation is a potential hazard until retaining structures are in place (**Hazard Two**). The vibrations from the proposed excavation are a potential hazard (**Hazard Three**). The proposed excavation undercutting the footings of the existing house causing failure is a potential hazard (**Hazard Four**).



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Geotechnical Hazards and Risk Analysis - Risk Analysis Summary

HAZARDS	Hazard One	Hazard Two
ТҮРЕ	The moderate slope that falls across the property and continues below failing and impacting on the property.	The proposed excavation collapsing onto the worksite before retaining walls are in place.
LIKELIHOOD	'Unlikely' (10 ⁻⁴)	'Possible' (10 ⁻³)
CONSEQUENCES TO PROPERTY	'Medium' (12%)	'Medium' (15%)
RISK TO PROPERTY	'Low' (2 x 10 ⁻⁵)	'Moderate' (2 x 10 ⁻⁴)
RISK TO LIFE	8.3 x 10 ⁻⁷ /annum	8.3 x 10 ⁻⁶ /annum
COMMENTS	This level of risk is 'ACCEPTABLE'.	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk to 'ACCEPTABLE' levels, the recommendations in Section 13 are to be followed.

HAZARDS	Hazard Three	Hazard Four
ТҮРЕ	The vibrations produced during the	The proposed excavation undercutting
	proposed excavation impacting on	the footings of the existing house
	the surrounding structures.	causing failure.
LIKELIHOOD	'Possible' (10 ⁻³)	'Possible' (10 ⁻³)
CONSEQUENCES	'Medium' (15%)	'Medium' (35%)
TO PROPERTY		
RISK TO	'Moderate' (2 x 10 ⁻⁴)	'Moderate' (2 x 10 ⁻⁴)
PROPERTY		
RISK TO LIFE	8.3 x 10 ⁻⁷ /annum	8.3 x 10 ⁻⁶ /annum
COMMENTS	This level of risk to property is	This level of risk to life and property is
	'UNACCEPTABLE'. To move risk to	'UNACCEPTABLE'. To move risk to
	'ACCEPTABLE' levels the	'ACCEPTABLE' levels, the
	recommendations in Sections 11 &	recommendations in Section 13 are to
	12 are to be followed.	be followed.

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

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9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.

10. Stormwater

No significant stormwater runoff will be created by the proposed development.

11. Excavations

An excavation to maximum depth of ~1.3m will be required to construct the proposed rumpus room. The excavation is expected to be through topsoil, sand and clayey sand, with Medium Strength Sandstone expected at depths of between ~0.4m to ~1.4m. It is envisaged that excavations through soil, sand and clayey sand can be carried out with a machine and bucket and excavations through Medium Strength Sandstone or better will require grinding or rock sawing and breaking.

12. Vibrations

Possible vibrations generated during excavations through soil, sand and clayey sand will be below the threshold limit for building damage.

Excavations through Medium Strength Rock or better should be carried out to minimise the potential to cause vibration damage to the subject house and neighbouring properties to the W and E. Close controls by the contractor over rock excavation are recommended so excessive vibrations are not generated.

Excavation methods are to be used that limit peak particle velocity to 10mm/sec at the subject house and property boundaries. Vibration monitoring will be required to verify this is achieved.

If a milling head is used to grind the rock, vibration monitoring will not be required. Alternatively, if rock sawing is carried out around the perimeter of the excavation boundaries



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in not less than 1.0m lifts, a rock hammer up to 300kg could be used to break the rock without vibration monitoring. Peak particle velocity will be less than 10mm/sec at the subject house and property boundaries using this method provided the saw cuts are kept well below the rock to broken.

It is worth noting that vibrations that are below thresholds for building damage may be felt by the occupants of the subject house and neighbouring properties.

13. Excavations Support Requirements

An excavation to maximum depth of ~1.3m will be required to construct the proposed rumpus room. The excavation will come flush with some of the supporting brick piers of the existing house. The supporting bricks piers/walls are to be propped and supported with beams if they are to be removed or underpinned to rock prior to the excavation, if they are to remain. Once these works are complete the proposed excavation can commence.

Where underpinning isn't necessary, the cut batters through soil, sand and clayey sand will stand at near-vertical angles for a short period of time until the retaining walls are in place, provided the cut batters are kept from becoming saturated. Medium Strength Sandstone or better will stand at vertical angles unsupported subject to approval by the geotechnical consultant.

All unsupported cut batters are to be covered to prevent access of water in wet weather and loss of moisture in dry weather. The materials and labour to construct the retaining walls are to be organised so on completion of the excavation they can be constructed as soon as possible. The excavation is to be carried out during a dry period. No excavations are to commence if heavy or prolonged rainfall is forecast. If the retaining walls are not constructed within a few days of the excavation being completed temporary shoring will be required.

All excavation spoil is to be removed from site or be supported by engineered retaining walls.

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15. Retaining Structures

For cantilever or singly propped retaining structures it is suggested the design be based on a triangular distribution of lateral pressures using the parameters shown in Table 1.

Table 1 – Likely	/ Earth Pressures for Retaining Structures

	Earth Pressure Coefficients			
Unit	Unit weight (kN/m³)	'Active' Ka	'At Rest' K₀	
Soil, Sand, Clayey Sand	20	0.40	0.55	
Medium Strength Sandstone	24	0.00	0.01	

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure, do not account for any surcharge loads and assume retaining structures are fully drained.

Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining structures are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e. Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining structures the full hydrostatic pressures are to be accounted for in the retaining structure design.

16. Foundations

The proposed rumpus room is expected to be seated in Medium Strength Sandstone. This is a suitable bearing material. Where the rock drops away, shallow piers will be required to



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maintain a uniform bearing material across the structure. A maximum allowable bearing pressure of 1000kPa can be assumed for footings on Medium Strength Sandstone.

The foundations of the existing house/timber deck are currently unknown. Ideally, footings should be founded on the same footing material across the structure. Where the footing material does change across the structure construction joints or similar are to be installed to prevent differential settlement, where the structure cannot tolerate such movement in accordance with a class S site.

Naturally occurring vertical cracks (known as joints) commonly occur in sandstone. These are generally filled with soil and are the natural seepage paths through the rock. They can extend to depths of several metres and are usually relatively narrow but can range between 0.1 to 0.8m wide. If a footing falls over a joint in the rock, the construction process is simplified if with the approval of the structural engineer the joint can be spanned or alternatively the footing can be repositioned so it does not fall over the joint.

NOTE: If the contractor is unsure of the footing material required it is more cost effective to get the geotechnical professional on site at the start of the footing excavation to advise on footing depth and material. This mostly prevents unnecessary over excavation in clay like shaly rock but can be valuable in all types of geology.

17. Inspections

The client and builder are to familiarise themselves with the following required inspections as well as council geotechnical policy. We cannot provide geotechnical certification for the Occupation Certificate if the following inspections have not been carried out during the construction process.

 All footings are to be inspected and approved by the geotechnical consultant while the excavation equipment is still onsite and before steel reinforcing is placed or concrete is poured.



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White Geotechnical Group Pty Ltd.

Fulit

Ben White M.Sc. Geol., AusIMM., CP GEOL. No. 222757 Engineering Geologist



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Photo 1



Photo 2

White Geotechnical Group ABN 96164052715

www.whitegeo.com.au Phone 027900 3214 Info@whitegeo.com.au Shop 1/5 South Creek Rd, Dee Why



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Photo 3



Photo 4



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Photo 5



Photo 6

White Geotechnical Group ABN 96164052715

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Photo 7: Downhole is from top to bottom

www.whitegeo.com.au Phone 027900 3214 Info@whitegeo.com.au Shop 1/5 South Creek Rd, Dee Why



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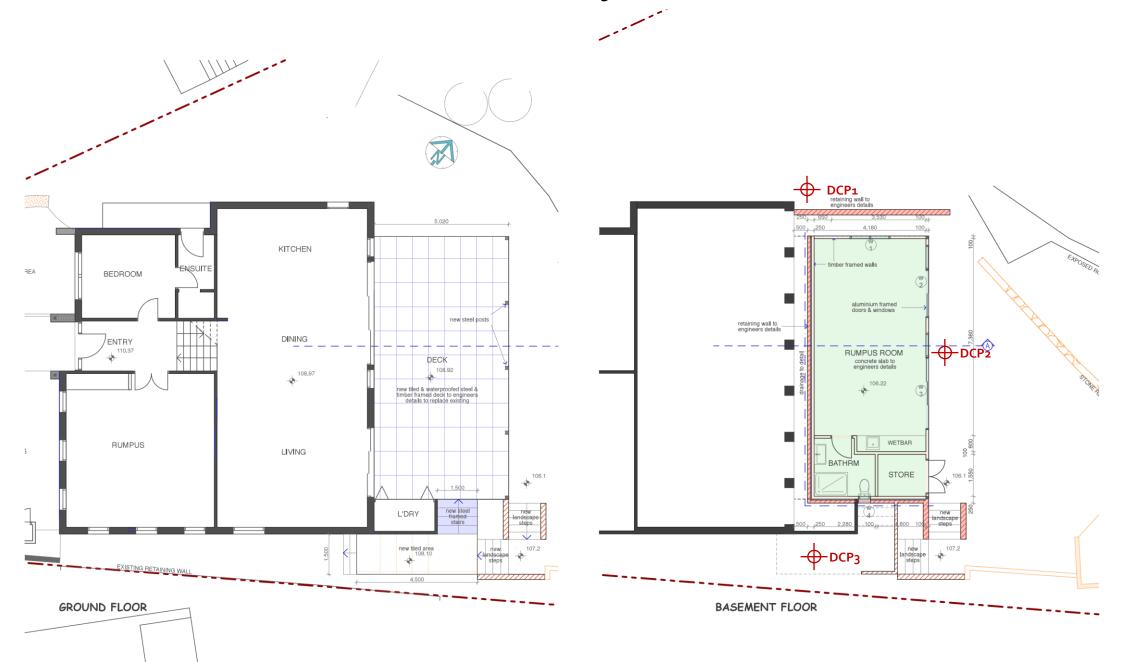
Important Information about Your Report

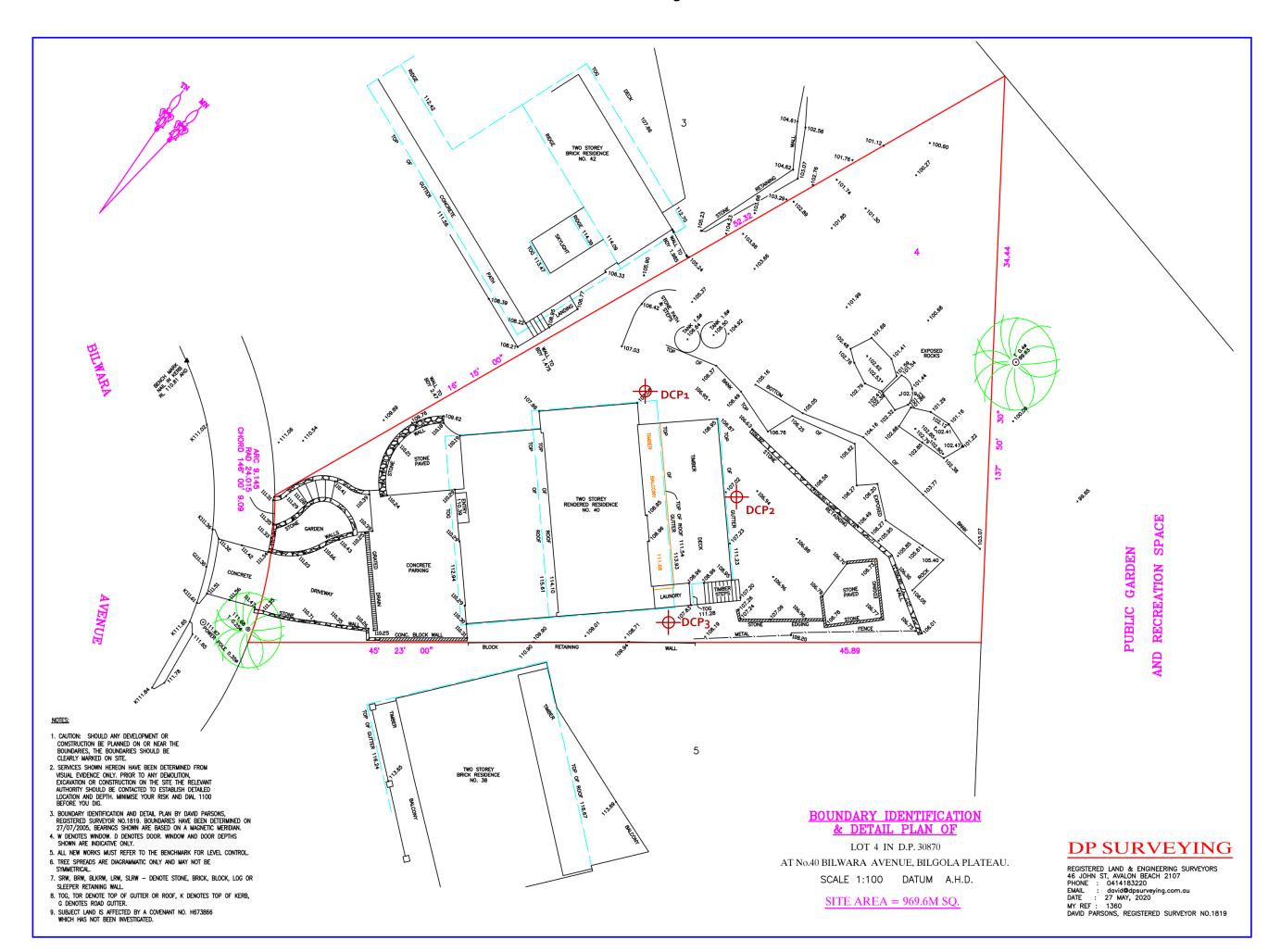
It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

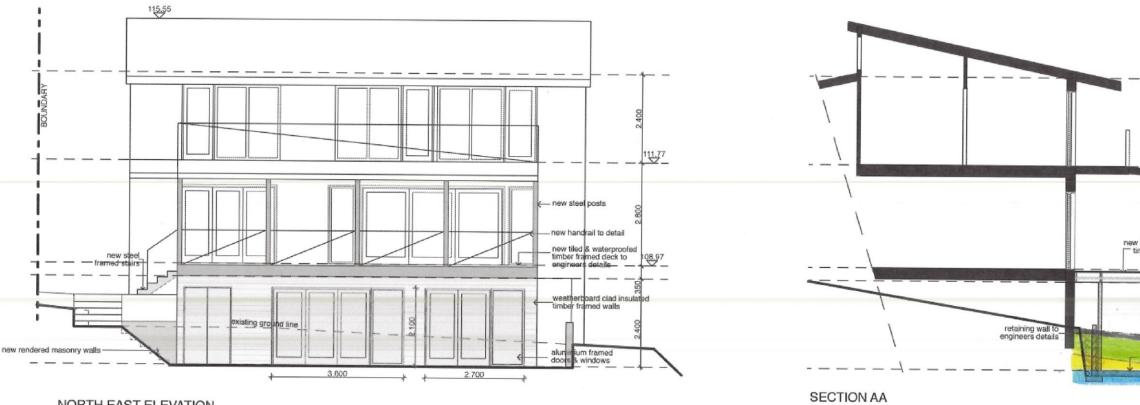
With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.

SITE PLAN – showing test locations







NORTH EAST ELEVATION

Topsoil **S**and **Clayey Sand**

AMENDMENTS	JO WILLMORE DESIGNS 11 Hudson Parade Clareville NSW 2107	PROPOSED ALTERATIONS & ADDITIONS for: P& K. Ponton at: 40 Bilwarra Avenue	drawing title ELEVATION & S
	9918 2479 ABN 27 370 370 173	BILGOLA PLATEAU	NOTE: Use figured dimension only Do not scale off drawings . All lew dimensions to be verified prior to of work

	date: JUNE 2020
ECTION	scale: 1:100 (A3)
ls and construction	drawing number DA-03

ON & SI

		2,400
		111.77
tiled & waterproofed nber framed deck	c new steel posts	08.97
RUMPUS ROOM	aluminium framed doors & windows	320
concrete slab to engineers details	- approximate existing ground	

Hawkesbury Sandstone – Medium Strength



EXAMPLES OF **POOR** HILLSIDE PRACTICE

