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Northern Beaches Council 1 Boondah Road WARRIEWOOD NSW 2106

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PRELIMINARY ACID SULFATE SOIL ASSESSMENT PROPOSED ALTERATIONS AND ADDITIONS NORTH NARRABEEN SURF LIFE SAVING CLUB, OCEAN STREET, NORTH NARRABEEN, NSW

1 INTRODUCTION

Northern Beaches Council ('the client') commissioned JK Environments (JKE) to undertake a preliminary acid sulfate soil (ASS) assessment for the proposed alterations and additions at North Narrabeen Surf Life Saving Club, Ocean Street, North Narrabeen, NSW. For this assessment, the development area is referred to as 'the site' and the North Narrabeen Surf Life Saving Club property is referred to as 'the wider property'. The site location is shown on Figure 1 and the investigation was limited to the approximate extent of the ground floor alterations as shown on Figure 2 attached in the appendices.

The investigation was undertaken generally in accordance with a JKE proposal (Ref: EP58713BR) of 31 May 2023 and written acceptance from Northern Beaches Council by email of 7 June 2023. A geotechnical investigation was undertaken in conjunction with the ASS assessment by JK Geotechnics and the results are presented in a separate report (Ref: 36107PErpt).

The aims of the assessment were to establish whether ASS may be disturbed during the proposed development works, and to assess whether an ASS management plan (ASSMP) is required.

1.1 Assessment Guidelines and Background

The ASS assessment and preparation of this report were undertaken with reference to the National Acid Sulfate Soil Guidance (2018) documents and the Acid Sulfate Soil Management Advisory Committee (ASSMAC) Acid Sulfate Soil Manual (1998)¹.

¹ Acid Sulfate Soils Management Advisory Committee (ASSMAC), (1998). Acid Sulfate Soils Manual (ASS Manual 1998)





ASS materials include potential acid sulfate soils (PASS or sulfidic soil materials) and actual acid sulfate soils (AASS or sulfuric soil materials). These are often found in the same profile, with AASS overlying PASS. AASS and PASS are defined further as follows:

- PASS are soil materials which contain Reduced Inorganic Sulfur (RIS) such as pyrite. The field pH of these soils in their undisturbed state is usually more than pH 4 and is commonly neutral to alkaline (pH 7–9). These soil materials are invariably saturated with water in their natural state. Their texture may be peat, clay, loam, silt or sand and is often dark grey in colour and soft in consistence, but these materials may also exhibit colours that are dark brown, or medium to pale grey to white; and
- AASS are soil materials which contained RIS such as pyrite that have undergone oxidation. This oxidation results in low pH (that is pH less than 4) and often a yellow (jarosite) and/or orange to red mottling (ferric iron oxides) in the soil profile. Actual ASS contains Actual Acidity, and commonly also contains RIS (the source of Potential Sulfuric Acidity) as well as Retained Acidity.

Further background information on ASS and the assessment process is provided in the appendices.

1.2 Proposed Development Details

Based on the details provided, it is understood that the proposed development includes alterations and additions, including a ground-level extension, BBQ renewal, associated landscaping words, internal refurbishments and first floor additions. Soil disturbance is expected to be limited to the extent necessary for foundation works. Bulk excavation is not proposed as part of the proposed development.

2 SITE INFORMATION

2.1 Site Information and Description

Site Address:	North Narrabeen Surf Life Saving Club, Ocean Street, North Narrabeen, NSW
Lot & Deposited Plan:	Lots 3, 6 and 8, Section 63 in DP5768, Lots 1 and 2 in DP339162 and Lots A and B in DP376822
Current Land Use:	Surf Life Saving Club
Site Area (m ²):	8,100
Site Elevation (metres Australian Height Datum – mAHD approx.)	10-12
Geographical Location (approx.) (approx. centre of	Latitude: -33.704965
club building):	Longitude: 151.304953

Table 2-1: Site Identification



The wider property is located in a predominantly residential and commercial area of Narrabeen and is bound by Ocean Street to the west and North Narrabeen Beach to the east. South Creek, an estuarine waterway, is located approximately 90m to the north of the site. The investigation area was confined to the approximate extent of the ground floor alterations proposed for the development as shown on Figure 2 attached in the appendices.

The regional topography is characterised by an east facing hillside that falls towards Narrabeen Beach. The wider property is located at the toe of the hillside and slopes down to the east at approximately 1-2°. The site itself is generally level. Parts of the site and the wider property appeared to have been levelled to accommodate the existing development.

At the time of the inspection, the wider property included a 1-2 storey building of predominantly brick and metal construction (the surf life saving club), grassed areas, children's play equipment and footpaths and driveways. Brick retaining walls (approximately 1.6m high) were observed in the north and west of the wider property. Bushland shrubs and low vegetation over sand dunes were observed to the north of the wider property.

The site was located in the north-east of the wider property, adjacent to the north of the existing club building (refer to Figure 2 attached in the appendices). The site was predominantly sealed with brick pavers and concrete pavement, with a 'u'-shaped brick wall (approximately 1.6m high) in the northern portion. An unsealed sand pathway extended along the northern boundary of the site and provided access to the beach to the north-east of the site.

2.2 Regional Geology

The geological map of Sydney (1983)² indicates the site and surrounds to be underlain by various Quaternary aged deposits, including medium to fine marine sand overlying quartz sand, minor shell content and interdune swale, silty and fine sand. Silty to peaty quartz sand, silt and clay with common shell layers is anticipated to the west of the site and coarse quartz sand with varying amounts of shell fragments is anticipated to the north and east of the site.

2.3 Acid Sulfate Soil Risk Map

A review of the ASS risk maps prepared by Department of Land and Water Conservation (1997)³ indicates that the site is mapped as an Aeolian sandplain is located in an area classed as having low probability of ASS occurrence at depths greater than 3m below the ground surface.

² Department of Mineral Resources, (1983). 1:100,000 Geological Map of Sydney (Series 9130)

³ Department of Land and Water Conservation, (1997). 1:25,000 Acid Sulfate Soil Risk Map (Series 9130S1, Ed 2)



2.4 Warringah Council Local Environmental Plan (LEP) 2011

A review of the Warringah council LEP indicates that the site is located in a Class 4 ASS risk area. JKE note that South Creek, an estuarine waterway located approximately 90m north of the site, is located in a Class 1 ASS risk area (refer to appendices for further details on each risk class).

3 INVESTIGATION REQUIREMENTS AND ASSESSMENT CRITERIA

3.1 Investigation Requirements

The National Acid Sulfate Soil Guidance (2018) requires sampling to a depth of 1m beyond the depth of disturbance (including the depth of any groundwater disturbance). A summary of the sampling densities and analysis requirements outlined in the *National Acid Sulfate Soil Guidance: National acid sulfate soils sampling and identification methods manual* (2018) is provided in the following tables:

Type of disturbance	Extent of site	Sample point frequency
Small volumes ($\leq 1000 \text{ m}^3$) – prior to disturbance	Volume of disturbance (m ³)	Number of boreholes
	< 250	2
	251–500	3
	501–1000	4
Large volumes (> 1000 m ³) – prior to disturbance	Project area (ha)	Number of boreholes
	<1	4
	1-2	6
	2-3	8
	3-4	10
	>4	10 plus 2 per additional hectare
Linear	Width and volume	Intervals (m)
	Minor ¹	100
	Major ²	50
Existing stockpiles & verification testing	Volume (m ³)	Number of samples
	<250	2
	251-500	3
	1,000	4
	>1,000	4 plus 1 per additional 500m ³

Table 3-1: Minimum Soil Sampling Densities for ASS Investigations

¹ Minor Linear Disturbance – for example underground services, narrow shallow drains (less than 1 m below ground level).

² Major Linear Disturbance – for example roads, railways, canals, deep sewer, wide drains, deep drains and dredging projects[#].

[#] Further guidance is provided in the Guidelines for the dredging of acid sulfate soil sediments and associated dredge spoil management (Simpson et al. 2017).



Volume of	Maximum dis	Maximum disturbance depth									
disturbed soils	< 1 m	1–2 m	2-3 m	3-4 m							
≤ 250m ³	3	4	5	6							
251-500m ³	4	5	6	7							
500–1,000m ³	5	6	7	8							

Table 3-2: Minimum Number of Soil Samples to be Submitted for Laboratory Analysis (small-scale disturbance)

Note: Small scale is considered less than or equal to 1,000 m³ and does not involve dewatering or groundwater pumping (excluding linear disturbances). Number of samples to be analysed per total volume of soil to be disturbed, not per borehole. Depth of disturbance to be measured from ground surface. Borehole depth must be at least 1 m below maximum proposed depth of disturbance.

The investigation component of this assessment was designed to address the minimum sampling density and analysis frequency. The sampling density and analysis frequency were considered to be adequate given the localised extent and shallow depths of soil disturbance proposed.

3.2 Action Criteria

The action criteria presented in the *National Acid Sulfate Soil Guidance: National acid sulfate soils sampling and identification methods manual* (2018) are summarised in the following table:

Type of material	Type of material		Net Acidity						
Texture range*	Approximate	1–1000 t materials	s disturbed	> 1000 t materials disturbed					
(NCST 2009)	clay content (%)	% S-equiv. (oven-dried basis)	mol H⁺/t (oven- dried basis)	% S-equiv. (oven-dried basis)	mol H ⁺ /t (oven- dried basis)				
Fine - light medium to heavy clays	>40	≥0.10	≥62	≥0.03	≥18				
Medium - clayey sand to light clays	5–40	≥0.06	≥36	≥0.03	≥18				
Coarse and Peats - sands to loamy sands	<5	≥0.03	≥18	≥0.03	≥18				

Table 3-3: ASS Action Criteria Based on Soil Texture and Volume of Material Being Disturbed

* If bulk density values are not available for the conversion of cubic meters to tonnes of soil, then default bulk densities, based on the soil texture, may be used.

The action criteria for coarse texture soils were used for this assessment.

3.3 Field Tests

The soil field tests commonly used for investigations for ASS materials include field pH (pH_F) and field pH peroxide (pH_{FOX}) tests. The pH_F test can help identify Actual ASS. While a pH_F of less than or equal to pH 4 is indicative of the presence of Actual ASS, it is not conclusive of the presence of ASS on its own, as naturally occurring, non ASS soils such as many organic soils (for example peats) and heavily leached soils may also have pH_F less than or equal to pH 4. To identify an Actual ASS other evidence must be presented that indicates the low pH_F has been mainly caused by the oxidation of reduced inorganic sulfur. Such information includes the



presence of jarosite in the soil layer/horizon, or the location of other Actual ASS or PASS materials within the sampling location or in the nearby vicinity.

The difference between the pH_F and the pH_{FOX} is helpful in the preliminary identification of PASS. Combined, the pH_F and pH_{FOX} results can be a useful aid with soil sample selection for laboratory analysis. Additional Information in relation to interpretation of the pH field tests is provided in the appendices.

4 INVESTIGATION PROCEDURE

4.1 Subsurface Investigation and Soil Sampling Methods

Field work was undertaken on 21 June 2023. Soil samples were collected from one location (TP/BH2) excavated for the concurrent JK Geotechnics investigation and three additional locations (BH5 to BH7 inclusive) drilled for the ASS assessment. The sampling locations were drilled to a maximum borehole depth of approximately 2.1m below ground level (BGL). The sampling locations are shown on the attached Figure 2.

The sample locations were drilled using hand equipment. JKE note that TP/BH2 was excavated as a test pit to a depth of approximately 0.5mBGL. A borehole was subsequently drilled at the base of the test pit and extended to a depth of approximately 2mBGL.

Soil samples were obtained at various depths, based on observations made during the field investigation. All samples were placed in plastic bags and sealed with plastic ties with minimal headspace. Each sample was labelled with a unique job number, the sampling location, sampling depth and date. All samples were recorded on the borehole logs and test pit cross-section attached in the appendices.

The samples were preserved by immediate storage in an insulated sample container with ice and returned to the JKE office. Samples were subsequently delivered in the insulated sample container (on ice) to a NATA registered laboratory for analysis under standard chain of custody (COC) procedures.

4.2 Laboratory Analysis

Samples for this assessment were analysed for ASS field tests (including pH_F and pH_{FOX}) and using the chromium reducible sulfur (S_{CR}) acid base accounting analytical methods. All tests/analysis were performed at the laboratory and JKE did not carry out the testing in the field due to time constraints. Samples were Analysed by Envirolab Services (NATA Accreditation Number – 2901). Reference should be made to the laboratory reports (Ref: 326110 and 326110-A) attached in the appendices for further information regarding the laboratory methods used.



5 RESULTS OF THE INVESTIGATION

5.1 Subsurface Conditions

A summary of the subsurface soil conditions encountered during the investigation is presented in the table below. Reference should be made to the borehole logs test pit cross-section attached in the appendices for further details.

Profile	Description
Pavement	Pavement was encountered at the surface in TP/BH2 and BH5 and ranged in thickness from approximately 75mm to 100mm.
Fill	 Fill soil was encountered in BH6 and BH7 and extended to depths of approximately 0.3m to 0.6mBGL. The fill typically comprised sand and contained inclusions of gravel, shells, slag, and glass and ceramic fragments. No odorous fill soil was encountered.
Natural Soil	Aeolian sand was encountered beneath the pavement in TP/BH2 and BH5, and beneath the fill in BH6 and BH7. The natural sand extended to the terminal depth of the boreholes at a maximum depth of approximately 2.1mBGL. Trace concentrations of shell were encountered in BH7. No organic or peaty odours were encountered.
Bedrock	Bedrock was not encountered in the boreholes drilled for the assessment.
Groundwater	Seepage was not encountered in the boreholes drilled for assessment.

Table 5-1: Summary of subsurface conditions

5.2 Laboratory Results

The soil laboratory results were assessed against the action criteria adopted for the assessment. The results are presented in the attached report tables and are summarised below.

Table 5-2: Summary of Results

Analysis	Ν	Comments
pH _F and pH _{FOX}	20	The pH _F results ranged from pH 8.5 to pH 10.8. The pH _{FOX} results ranged from pH 6.2 to pH 6.8. The maximum difference from pH _F to pH _{FOX} was 4 pH units.
pH _{FOX} reaction rates	20	All samples recorded reaction rates classed as 'low'. Five samples were selected for analysis of ASS characteristics using acid base accounting methods. The samples were selected based on a combination of the pH _F and pH _{FOX} results, and to provide spatial coverage and vertical distribution through the soil profiles.
Net Acidity % S- equiv.	5	Net acidity results were all below the laboratory PQL of 0.005 %w/w S and well below the action criterion of 0.03%w/w S.



Analysis	Ν	Comments
Net Acidity mol H ⁺ /t	5	Net acidity results were all below the laboratory PQL of 5molH ⁺ /t and well below the action criterion of 18molH ⁺ /t.
Scr%	5	The S_{CR} % results were all below the laboratory PQL of 0.005%. These results indicated that the soils did not contain significant oxidisable sulfur concentrations.
Liming Rate	5	The liming rate required for neutralisation was <0.75kgCaCO ₃ /tonne.

N: Total number (primary samples)

6 CONCLUSION

Based on the weight of evidence collected and evaluated for this assessment, there is considered to be a low potential for ASS materials (AASS or PASS) to be disturbed to a depth of approximately 2mBGL during the proposed development described in Section 1.2 of this report. On this basis, an ASSMP is not considered necessary for the proposed development.

7 LIMITATIONS

The report limitations are outlined below:

- JKE accepts no responsibility for any unidentified AASS or PASS issues at the site. Any unexpected problems/subsurface features that may be encountered during development works should be inspected by an environmental consultant as soon as possible;
- This report has been prepared based on site conditions which existed at the time of the investigation; scope of work and limitation outlined in the JKE proposal; and terms of contract between JKE and the client (as applicable);
- The conclusions presented in this report are based on investigation of conditions at specific locations, chosen to be as representative as possible under the given circumstances, visual observations of the site and immediate surrounds and documents reviewed as described in the report;
- Subsurface soil and rock conditions encountered between investigation locations may be found to be different from those expected. Groundwater conditions may also vary, especially after climatic changes;
- The investigation and preparation of this report have been undertaken in accordance with accepted practice for environmental consultants, with reference to applicable environmental regulatory authority and industry standards, guidelines and the assessment criteria outlined in the report;
- Where information has been provided by third parties, JKE has not undertaken any verification process, except where specifically stated in the report;
- JKE accept no responsibility for potentially asbestos containing materials that may exist at the site. These materials may be associated with demolition of pre-1990 constructed buildings or fill material at the site;
- JKE have not and will not make any determination regarding finances associated with the site;



- Additional investigation work may be required in the event of changes to the proposed development or landuse. JKE should be contacted immediately in such circumstances;
- This report has been prepared for the particular project described and no responsibility is accepted for the use of any part of this report in any other context or for any other purpose;
- Copyright in this report is the property of JKE. JKE has used a degree of care, skill and diligence normally exercised by consulting professionals in similar circumstances and locality. No other warranty expressed or implied is made or intended. Subject to payment of all fees due for the investigation, the client alone shall have a licence to use this report;
- If the client, or any person, provides a copy of this report to any third party, such third party must not rely on this report except with the express written consent of JKE; and
- Any third party who seeks to rely on this report without the express written consent of JKE does so entirely at their own risk and to the fullest extent permitted by law, JKE accepts no liability whatsoever, in respect of any loss or damage suffered by any such third party.

If you have any questions concerning the contents of this letter please do not hesitate to contact us.

Kind Regards

Craig Ridley Associate | Environmental Scientist



Vittal Boggaram Principal Associate | Environmental Scientist

Appendices:

Appendix A: Report Figures Appendix B: Laboratory Results Summary Table Appendix C: Information on Acid Sulfate Soils Appendix D: Borehole & Test Pit Logs Appendix E: Laboratory Reports & COC Documents



Appendix A: Report Figures

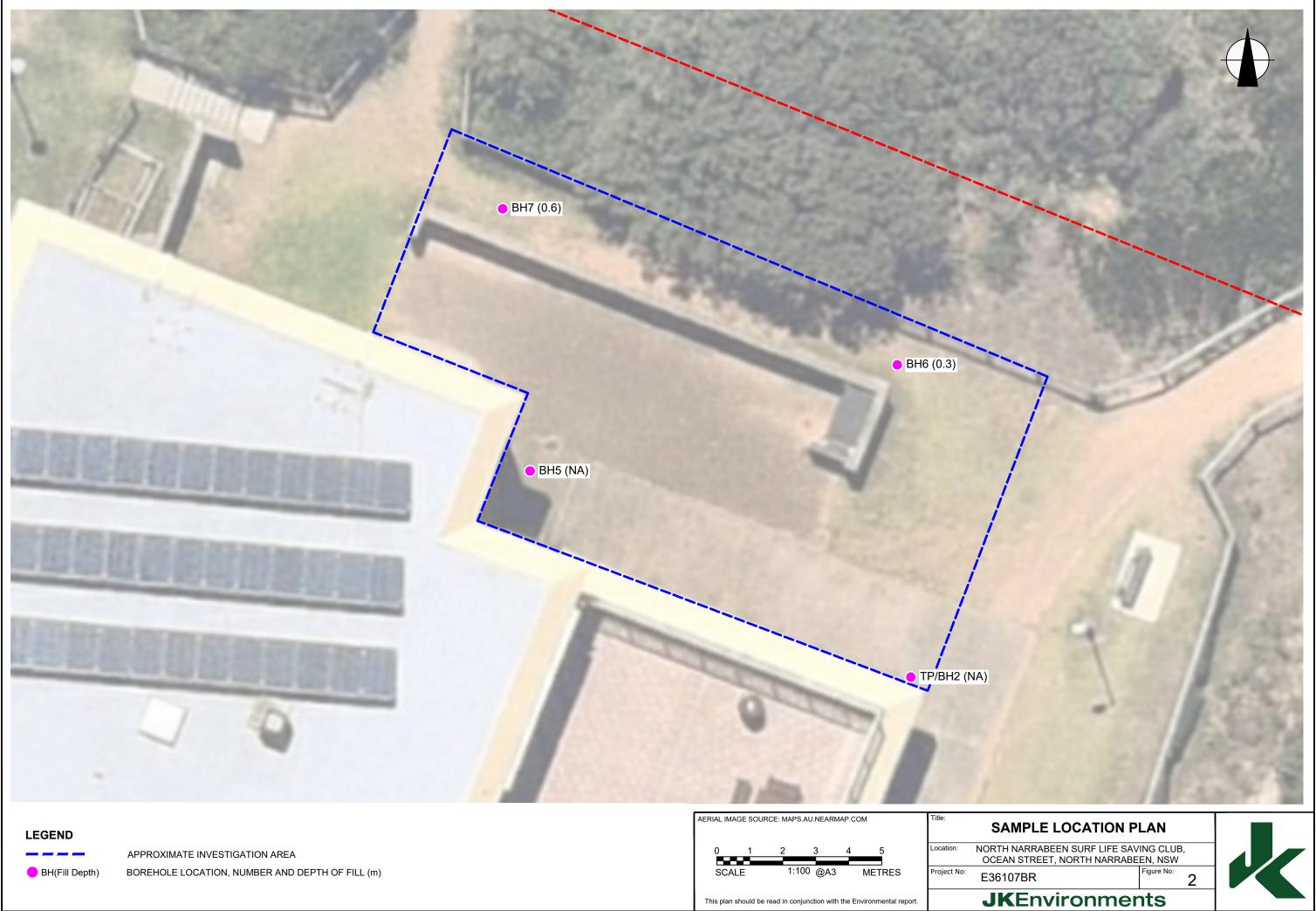




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This plan should be read in conjunction with the Environmental report.

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Appendix B: Laboratory Results Summary Table





ABBREVIATIONS AND EXPLANATIONS FOR ACID SULFATE SOIL TABLE

Abbreviations used in the Tables:

ANC _{BT}	Acid Neutralising Capacity - Back Titration
ANCE	Excess Acid Neutralising Capacity
CaCO ₃	Calcium Carbonate
kg	kilogram
mol H⁺/t	moles hydrogen per tonne
pHF	Field pH
pHFOX	Field peroxide pH
рН _{ксі}	Pottasium chloride pH
S	Sulfur
SCr	The symbol given to the result from the Chromium Reducible Sulfur method
S _{NAS}	Net Acid Soluble Sulfur
% w/w	Percentage by mass

Results have been assessed against the criteria specified in Table 1.1 of National Acid sulfate Soil Guidance - National acid sulfate soil identification and laboratory method manual. Water Quality Australia. June 2018



Soil Texture: Coarse		Soil Texture: Coarse		Analysis		pH,	F and pH _{FOX}			Actual Acidity (Titratable Actual Acidity - TAA)	Potential Su	lfidic Acidity	Retained Acidity	Acid Neutralising Capacity (ANC _{BT})	a-Net Acidity without ANCE	s-Net Acidity without ANCE	Liming Rate - withou ANCE
			pH _F	pH _{FOX}	Reaction	pH _F - pH _{FOX}	рН _{ксL}	(mol H [*] /t)	(% SCr)	(mol H ⁺ /t)	(%S _{NAS})	(% CaCO₃)	(mol H ⁺ /t)	(%w/w S)	(kg CaCO₃/tonne)		
National Acid	Sulfate Soils												40	0.02			
Guidance	(2018)		-	-	-	-	-	-	-	-	-	-	18	0.03	-		
Sample	Sample Depth																
Reference	(m)	Sample Description															
BH2	0.08-0.2	Sand	9.9	6.4	Low reaction	3.5	9.1	<5	< 0.005	<3	[NT]	6.6	<5	< 0.005	<0.75		
3H2 [LAB_DUP]	0.08-0.2	Laboratory Duplicate	-	-	-	-	9.2	<5	< 0.005	<3	[NT]	6.4	<5	< 0.005	<0.75		
BH2	0.4-0.5	Sand	9.9	6.5	Low reaction	3.4	-	-	-	-	-	-	-	-	-		
BH2	0.9-1.0	Sand	9.6	6.7	Low reaction	2.9	-	-	-	-	-	-	-	-	-		
BH2	1.5-1.6	Sand	9.7	6.7	Low reaction	3	9.4	<5	< 0.005	<3	[NT]	6.7	<5	< 0.005	<0.75		
BH2	1.9-2.0	Sand	9.7	6.7	Low reaction	3	-	-	-	-	-	-	-	-	-		
BH5	0.1-0.2	Sand	10.8	6.8	Low reaction	4	-	-	-	-	-	-	-	-	-		
BH5	0.5-0.6	Sand	9.8	6.5	Low reaction	3.3	9.2	<5	< 0.005	<3	[NT]	7	<5	< 0.005	<0.75		
BH5	1.0-1.1	Sand	9.8	6.7	Low reaction	3.1	-	-	-	-	-	-	-	-	-		
BH5	1.5-1.6	Sand	9.7	6.5	Low reaction	3.2	-	-	-	-	-	-	-	-	-		
BH5	1.9-2.0	Sand	9.5	6.7	Low reaction	2.8	-	-	-	-	-	-	-	-	-		
BH6	0-0.1	F: Sand	8.5	6.2	Low reaction	2.3	-	-	-	-	-	-	-	-	-		
BH6	0.5-0.6	Sand	9.1	6.5	Low reaction	2.6	-	-	-	-	-	-	-	-	-		
BH6	1.0-1.1	Sand	9.4	6.4	Low reaction	3	9.6	<5	< 0.005	<3	[NT]	5	<5	< 0.005	<0.75		
BH6	1.5-1.6	Sand	9.5	6.5	Low reaction	3	-	-	-	-	-	-	-	-	-		
BH6	1.9-2.0	Sand	9.5	6.5	Low reaction	3	-	-	-	-	-	-	-	-	-		
BH7	0-0.1	F: Sand	9	6.3	Low reaction	2.7	-	-	-	-	-	-	-	-	-		
BH7	0.5-0.6	F: Sand	9	6.5	Low reaction	2.5	-	-	-	-	-	-	-	-	-		
BH7	1.0-1.1	Sand	9.3	6.4	Low reaction	2.9	-	-	-	-	-	-	-	-	-		
BH7	1.5-1.6	Sand	9.3	6.6	Low reaction	2.7	-	-	-	-	-	-	-	-	-		
BH7	2.0-2.1	Sand	9.3	6.6	Low reaction	2.7	9	<5	< 0.005	<3	[NT]	5.2	<5	<0.005	<0.75		
tal Number -fC			20	20	20	20	6	6	6	6	-	6	6	6	6		
Fotal Number of Samples Minimum Value					20 2.3	9	6 <5	<0.005	<3		5	6 <5	<0.005	6			
			8.5 6.2	-						-		-		<0.75			
aximum Value			10.8	6.8	-	4	9.6	<5	< 0.005	<3	-	7	<5	< 0.005	<0.75		



Appendix C: Information on Acid Sulfate Soils





A. <u>Background</u>

Acid Sulfate Soil (ASS) is formed from iron rich alluvial sediments and sulfate (found in seawater) in the presence of sulfate reducing bacteria and plentiful organic matter. These conditions are generally found in mangroves, salt marsh vegetation or tidal areas and at the bottom of coastal rivers and lakes. ASS materials are distinguished from other soil or sediment materials (referred to as 'soil materials' throughout the National Acid Sulfate Soils Guidance) by having properties and behaviour that have either:

- 1) Been affected considerably by the oxidation of Reduced Inorganic Sulfur (RIS), or
- 2) The capacity to be affected considerably by the oxidation of their RIS constituents.

Acid sulfate soil materials include potential acid sulfate soils (PASS or sulfidic soil materials) and actual acid sulfate soils (AASS or sulfuric soil materials). These are often found in the same profile, with AASS overlying PASS. PASS and AASS are defined further below:

- PASS are soil materials which contain RIS such as pyrite. The field pH of these soils in their undisturbed state is usually more than pH 4 and is commonly neutral to alkaline (pH 7–9). These soil materials are invariably saturated with water in their natural state. Their texture may be peat, clay, loam, silt or sand and is often dark grey in colour and soft in consistence, but these materials may also exhibit colours that are dark brown, or medium to pale grey to white; and
- AASS are soil materials which contained RIS such as pyrite that have undergone oxidation. This oxidation results in low pH (that is pH less than 4) and often a yellow (jarosite) and/or orange to red mottling (ferric iron oxides) in the soil profile. Actual ASS contains Actual Acidity, and commonly also contains RIS (the source of Potential Sulfuric Acidity) as well as Retained Acidity.

B. <u>The ASS Planning Maps</u>

The ASS planning maps provide an indication of the relative potential for disturbance of ASS to occur at locations within the council area. These maps do not provide an indication of the actual occurrence of ASS at a site or the likely severity of the conditions.

The maps are divided into five classes dependent upon the type of activities/works that if undertaken, may represent an environmental risk through the development of acidic conditions associated with ASS:

Risk Class	Description
Class 1	All works.
Class 2	All works below existing ground level and works by which the water table is likely to be lowered.
Class 3	Works at depths beyond 1m below existing ground level or works by which the water table is likely to be lowered beyond 1m below existing ground level.
Class 4	Works at depths beyond 2m below existing ground level or works by which the water table is likely to be lowered beyond 2m below existing ground level.
Class 5	Works within 500m of adjacent Class 1, 2, 3, 4 land which are likely to lower the water table below 1m AHD on the adjacent land.

Table 1: Risk Classes

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C. The ASS Risk Maps

The ASS risk maps provide an indication of the probability of occurrence of ASS materials at a particular location based on interpretation from geological and soil landscape maps. The maps provide classes based on high probability, low probability, no known occurrence and areas of disturbed terrain (site specific assessment necessary) and the likely depth at which ASS materials are likely to be encountered.

D. Interpretation of ASS Field Tests

Tables A1 and A2 below provide some guidance on the interpretation of pH_F and pH_{FOX} test results, as detailed in the *National Acid Sulfate Soil Guidance: National acid sulfate soils sampling and identification methods manual* (2018):

pH value	Result	Comments
pH _F ≤ 4, jarosite not observed in the soil layer/horizon	May indicate an AASS indicating previous oxidation of RIS or may indicate naturally occurring, non ASS soils.	Generally not conclusive as naturally occurring, non ASS soils, such as many organic soils (for example peats) and heavily leached soils, often also return $pH_F \le 4$.
pH _F ≤ 4, jarosite observed in the soil layer/horizon	The soil material is an AASS.	Jarosite and other iron precipitate minerals in ASS such as schwertmannite require a pH < 4 to form and indicate prior oxidation of RIS.
pH _F > 7	Expected in waterlogged, unoxidised, or poorly drained soils.	Marine muds commonly have a pH > 7 which reflects a seawater (pH 8.2) influence. Oxidation of samples with H_2O_2 can help indicate if the soil materials contain RIS.

Table A1: Interpretation of some pH_F test ranges

Source: Adapted from DER (2015a).

pH value and reaction	Result	Comments
Strong reaction of soil with H ₂ O ₂ (that is X or V)	Useful indicator of the presence of RIS but cannot be used alone	Organic rich substrates such as peat and coffee rock, and soil constituents like manganese oxides, can also cause a reaction. Care must be exercised in interpreting these results. Laboratory analyses are required to confirm if appreciable RIS is present.
pH _{FOX} value at least one unit below field pH _F and strong reaction with H ₂ O ₂ (that is X or V)	May indicate PASS	The difference between pH _F and pH _{FOX} is termed the Δ pH. Generally the larger the Δ pH the more indicative of PASS. The lower the final pH _{FOX} the better the likelihood of an appreciable RIS content. For example, a change from pH _F of 8 to pH _{FOX} of 7 (that is a Δ pH of 1) would not indicate PASS, however, a unit change from pH _F of 3.5 to pH _{FOX} of 2.5 would be indicative of PASS. Laboratory analyses are required to confirm if appreciable RIS is present.
pH _{FOX} < 3, large ΔpH and a strong reaction with H ₂ O ₂ (that is X or V)	Strongly indicates PASS	The lower the pH_{FOX} below 3, the greater the likelihood that appreciable RIS is present. A combination of all three parameters – pH_{FOX} , ΔpH and reaction strength – gives the

Table A2: Interpretation of pH_{FOX} test results

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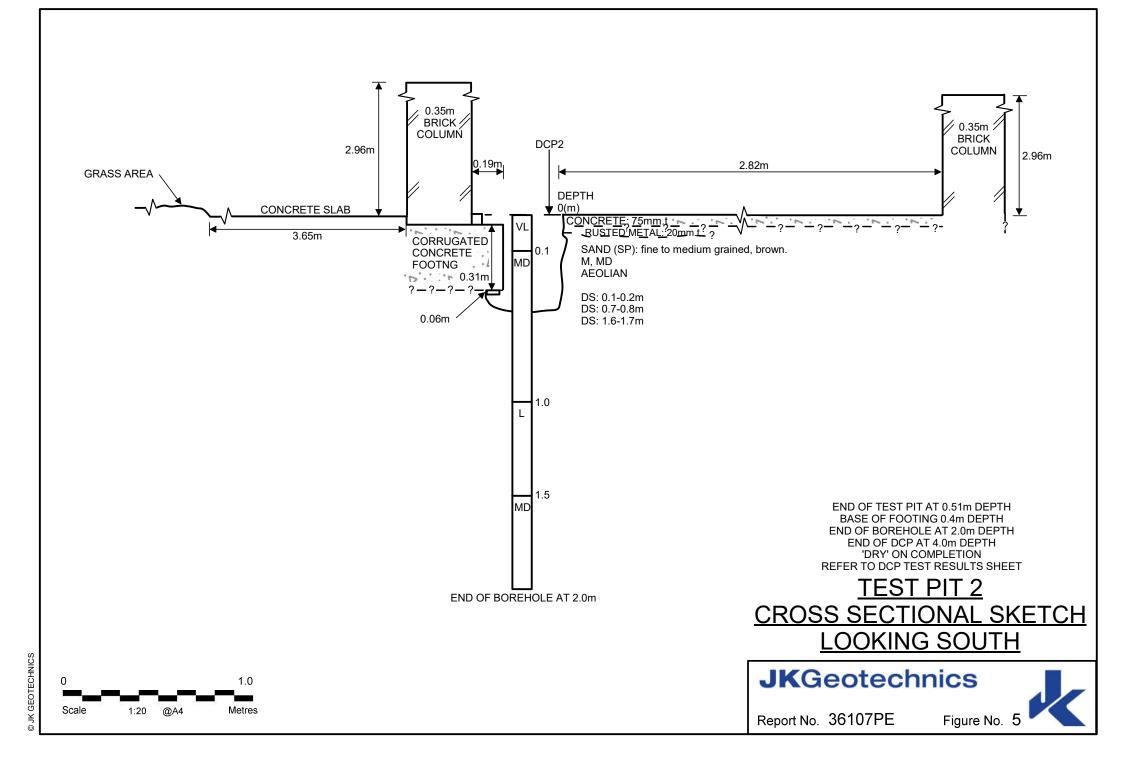
pH value and reaction	Result	Comments
		best indication of PASS. Laboratory analyses are required to confirm that appreciable RIS is present.
A pH _{FOX} 3–4 and Low, Medium or Strong reaction with H ₂ O ₂	Inconclusive	RIS may be present; however, organic matter may also be responsible for the decrease in pH. Laboratory analyses are required to confirm the presence of RIS.
рН _{FOX} 4—5	Inconclusive	RIS may be present in small quantities, or poorly reactive under rapid oxidation, or the sample may contain shell/ carbonate which neutralises some or all acid produced on oxidation. Equally, the pH _{FOX} value may be due to the production of organic acids with no RIS present. Laboratory analyses are required to confirm if appreciable RIS is present.
$pH_{FOX} > 5$, small or no ΔpH , but Low, Medium or Strong reaction with H_2O_2	Inconclusive	For neutral to alkaline pHF with shell or white concretions, the fizz test with 1 M HCl can be used to identify the presence of carbonates. Laboratory analyses are required to confirm if appreciable RIS is present and further testing is required to confirm that effective self- neutralising materials are present.

Source: Adapted from DER (2015a).



Appendix D: Borehole & Test Pit Logs

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JKEnvironments ENVIRONMENTAL LOG

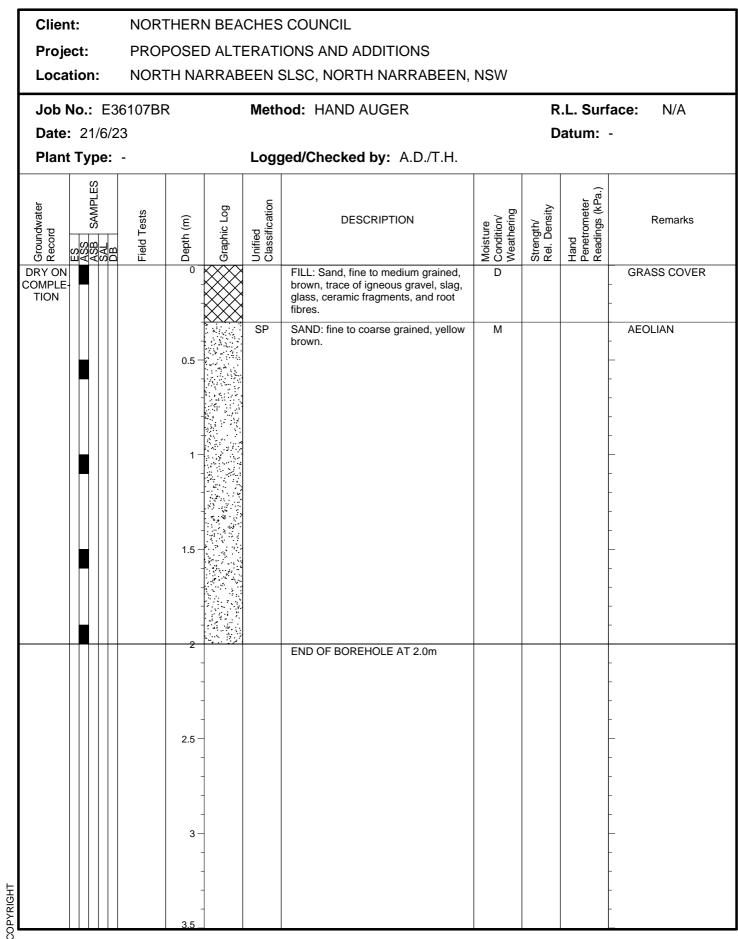
Environmental logs are not to be used for geotechnical purposes



Clie	ent:		NORT	DRTHERN BEACHES COUNCIL							
	ject:				OSED ALTERATIONS AND ADDITIONS						
Loc	cation	า:	NORT	TH NARRABEEN SLSC, NORTH NARRABEEN, NSW							
Job	No.:	: E30	6107BF	R Method: HAND AUGER R.L. Surface: N/A						ace: N/A	
	e: 2					_			D	atum: -	
Pla	nt Ty		-			Logg	jed/Checked by: A.D./T.H.				
Groundwater Record	ES ASS	ASB SAMPLES SAL DB	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
DRY C COMPL	N			0			CONCRETE: 100mm.t				_
TION						SP	SAND: fine to coarse grained, yellow brown.	Μ			AEOLIAN
				- 2			END OF BOREHOLE AT 2.0m			-	
				-							
				-							
				2.5 —							_
				-							
				-							
				3-							-
				-							
LHS				-							
COPYRIGHT				- 3.5 _							

JKEnvironments ENVIRONMENTAL LOG

Environmental logs are not to be used for geotechnical purposes



Log No. BH6 1/1

JKEnvironments ENVIRONMENTAL LOG

Environmental logs are not to be used for geotechnical purposes



Clien Proje Loca	ect:	NORTHERN BEACHES COUNCIL PROPOSED ALTERATIONS AND ADDITIONS NORTH NARRABEEN SLSC, NORTH NARRABEEN, NSW										
Job N	lo.: E3	6107BF	र		Meth	od: HAND AUGER		R	.L. Surf	ace: N/A		
	21/6/2 Type:				Logo	red/Checked by: A D /T H		D	atum:	-		
undwater ord	ASS SAL DB DB SAL DB	d Tests	Depth (m)	Graphic Log	Unified Classification	Logged/Checked by: A.D./T.H.		Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks		
DRY ON COMPLE- TION			0.5 -			FILL: Sand, fine to medium grained, brown, trace of igneous gravel, shells and root fibres.	D Condition/ Weathering			GRASS COVER		
			- - 1 -		SP	SAND: fine to coarse grained, yellow brown, trace of shells.	М			AEOLIAN		
			1.5 -							- - -		
			2 -			END OF BOREHOLE AT 2.1m				-		
			2.5 -	-						-		
			3-							- - -		
			3.5	-						-		



ENVIRONMENTAL LOGS EXPLANATION NOTES

INTRODUCTION

These notes have been provided to amplify the environmental report in regard to classification methods, field procedures and certain matters relating to the logging of soil and rock. Not all notes are necessarily relevant to all reports.

Where geotechnical borehole logs are utilised for environmental purpose, reference should also be made to the explanatory notes included in the geotechnical report. Environmental logs are not suitable for geotechnical purposes.

The ground is a product of continuing natural and man-made processes and therefore exhibits a variety of characteristics and properties which vary from place to place and can change with time. Environmental studies include gathering and assimilating limited facts about these characteristics and properties in order to understand or predict the behaviour of the ground on a particular site under certain conditions. This report may contain such facts obtained by inspection, excavation, probing, sampling, testing or other means of investigation. If so, they are directly relevant only to the ground at the place where and time when the investigation was carried out.

DESCRIPTION AND CLASSIFICATION METHODS

The methods of description and classification of soils and rocks used in this report are based on Australian Standard 1726:2017 *'Geotechnical Site Investigations'*. In general, descriptions cover the following properties – soil or rock type, colour, structure, strength or density, and inclusions. Identification and classification of soil and rock involves judgement and the Company infers accuracy only to the extent that is common in current geoenvironmental practice.

Soil types are described according to the predominating particle size and behaviour as set out in the attached soil classification table qualified by the grading of other particles present (eg. sandy clay) as set out below:

Soil Classification	Particle Size
Clay	< 0.002mm
Silt	0.002 to 0.075mm
Sand	0.075 to 2.36mm
Gravel	2.36 to 63mm
Cobbles	63 to 200mm
Boulders	> 200mm

Non-cohesive soils are classified on the basis of relative density, generally from the results of Standard Penetration Test (SPT) as below:

Relative Density	SPT 'N' Value (blows/300mm)
Very loose (VL)	< 4
Loose (L)	4 to 10
Medium dense (MD)	10 to 30
Dense (D)	30 to 50
Very Dense (VD)	> 50

Cohesive soils are classified on the basis of strength (consistency) either by use of a hand penetrometer, vane shear, laboratory testing and/or tactile engineering examination. The strength terms are defined as follows.

Classification	Unconfined Compressive Strength (kPa)	Indicative Undrained Shear Strength (kPa)		
Very Soft (VS)	≤25	≤12		
Soft (S)	> 25 and \leq 50	> 12 and \leq 25		
Firm (F)	> 50 and \leq 100	> 25 and \leq 50		
Stiff (St)	$>$ 100 and \leq 200	> 50 and ≤ 100		
Very Stiff (VSt)	$>$ 200 and \leq 400	$>$ 100 and \leq 200		
Hard (Hd)	> 400	> 200		
Friable (Fr)	Strength not attainable – soil crumbles			

Rock types are classified by their geological names, together with descriptive terms regarding weathering, strength, defects, etc. Where relevant, further information regarding rock classification is given in the text of the report. In the Sydney Basin, 'shale' is used to describe fissile mudstone, with a weakness parallel to bedding. Rocks with alternating inter-laminations of different grain size (eg. siltstone/claystone and siltstone/fine grained sandstone) are referred to as 'laminite'.

INVESTIGATION METHODS

The following is a brief summary of investigation methods currently adopted by the Company and some comments on their use and application. All methods except test pits, hand auger drilling and portable Dynamic Cone Penetrometers require the use of a mechanical rig which is commonly mounted on a truck chassis or track base.

Test Pits: These are normally excavated with a backhoe or a tracked excavator, allowing close examination of the insitu soils and 'weaker' bedrock if it is safe to descend into the pit. The depth of penetration is limited to about 3m for a backhoe and up to 6m for a large excavator. Limitations of test pits are the problems associated with disturbance and difficulty of reinstatement and the consequent effects on close-by structures. Care must be taken if construction is to be carried out near test pit locations to either properly recompact the backfill during construction or to design and construct the



structure so as not to be adversely affected by poorly compacted backfill at the test pit location.

Hand Auger Drilling: A borehole of 50mm to 100mm diameter is advanced by manually operated equipment. Refusal of the hand auger can occur on a variety of materials such as obstructions within any fill, tree roots, hard clay, gravel or ironstone, cobbles and boulders, and does not necessarily indicate rock level.

Continuous Spiral Flight Augers: The borehole is advanced using 75mm to 115mm diameter continuous spiral flight augers, which are withdrawn at intervals to allow sampling and insitu testing. This is a relatively economical means of drilling in clays and in sands above the water table. Samples are returned to the surface by the flights or may be collected after withdrawal of the auger flights, but they can be very disturbed and layers may become mixed. Information from the auger sampling (as distinct from specific sampling by SPTs or undisturbed samples) is of limited reliability due to mixing or softening of samples by groundwater, or uncertainties as to the original depth of the samples. Augering below the groundwater table is of even lesser reliability than augering above the water table.

Rock Augering: Use can be made of a Tungsten Carbide (TC) bit for auger drilling into rock to indicate rock quality and continuity by variation in drilling resistance and from examination of recovered rock cuttings. This method of investigation is quick and relatively inexpensive but provides only an indication of the likely rock strength and predicted values may be in error by a strength order. Where rock strengths may have a significant impact on construction feasibility or costs, then further investigation by means of cored boreholes may be warranted.

Wash Boring: The borehole is usually advanced by a rotary bit, with water being pumped down the drill rods and returned up the annulus, carrying the drill cuttings. Only major changes in stratification can be assessed from the cuttings, together with some information from "feel" and rate of penetration.

Mud Stabilised Drilling: Either Wash Boring or Continuous Core Drilling can use drilling mud as a circulating fluid to stabilise the borehole. The term 'mud' encompasses a range of products ranging from bentonite to polymers. The mud tends to mask the cuttings and reliable identification is only possible from intermittent intact sampling (eg. from SPT and U50 samples) or from rock coring, etc.

Continuous Core Drilling: A continuous core sample is obtained using a diamond tipped core barrel. Provided full core recovery is achieved (which is not always possible in very low strength rocks and granular soils), this technique provides a very reliable (but relatively expensive) method of investigation. In rocks, NMLC or HQ triple tube core barrels, which give a core of about 50mm and 61mm diameter, respectively, is usually used with water flush. The length of core recovered is compared to the length drilled and any length not recovered is shown as NO CORE. The location of NO CORE recovery is determined on site by the supervising engineer; where the location is uncertain, the loss is placed at the bottom of the drill run.

Standard Penetration Tests: Standard Penetration Tests (SPT) are used mainly in non-cohesive soils, but can also be used in cohesive soils, as a means of indicating density or strength and also of obtaining a relatively undisturbed sample. The test procedure is

described in Australian Standard 1289.6.3.1–2004 (R2016) 'Methods of Testing Soils for Engineering Purposes, Soil Strength and Consolidation Tests – Determination of the Penetration Resistance of a Soil – Standard Penetration Test (SPT)'.

The test is carried out in a borehole by driving a 50mm diameter split sample tube with a tapered shoe, under the impact of a 63.5kg hammer with a free fall of 760mm. It is normal for the tube to be driven in three successive 150mm increments and the 'N' value is taken as the number of blows for the last 300mm. In dense sands, very hard clays or weak rock, the full 450mm penetration may not be practicable and the test is discontinued.

The test results are reported in the following form:

• In the case where full penetration is obtained with successive blow counts for each 150mm of, say, 4, 6 and 7 blows, as

N = 13 4, 6, 7

 In a case where the test is discontinued short of full penetration, say after 15 blows for the first 150mm and 30 blows for the next 40mm, as

> N > 30 15, 30/40mm

The results of the test can be related empirically to the engineering properties of the soil.

A modification to the SPT is where the same driving system is used with a solid 60° tipped steel cone of the same diameter as the SPT hollow sampler. The solid cone can be continuously driven for some distance in soft clays or loose sands, or may be used where damage would otherwise occur to the SPT. The results of this Solid Cone Penetration Test (SCPT) are shown as 'N_c' on the borehole logs, together with the number of blows per 150mm penetration.

LOGS

The borehole or test pit logs presented herein are an interpretation of the subsurface conditions, and their reliability will depend to some extent on the frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will enable the most reliable assessment, but is not always practicable or possible to justify on economic grounds. In any case, the boreholes or test pits represent only a very small sample of the total subsurface conditions.

The terms and symbols used in preparation of the logs are defined in the following pages.

Interpretation of the information shown on the logs, and its application to design and construction, should therefore take into account the spacing of boreholes or test pits, the method of drilling or excavation, the frequency of sampling and testing and the possibility of other than 'straight line' variations between the boreholes or test pits. Subsurface conditions between boreholes or test pits may vary significantly from conditions encountered at the borehole or test pit locations.



GROUNDWATER

Where groundwater levels are measured in boreholes, there are several potential problems:

- Although groundwater may be present, in low permeability soils it may enter the hole slowly or perhaps not at all during the time it is left open.
- A localised perched water table may lead to an erroneous indication of the true water table.
- Water table levels will vary from time to time with seasons or recent weather changes and may not be the same at the time of construction.
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must be washed out of the hole or 'reverted' chemically if reliable water observations are to be made.

More reliable measurements can be made by installing standpipes which are read after the groundwater level has stabilised at intervals ranging from several days to perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from perched water tables or surface water.

FILL

The presence of fill materials can often be determined only by the inclusion of foreign objects (eg. bricks, steel, etc) or by distinctly unusual colour, texture or fabric. Identification of the extent of fill materials will also depend on investigation methods and frequency. Where natural soils similar to those at the site are used for fill, it may be difficult with limited testing and sampling to reliably assess the extent of the fill.

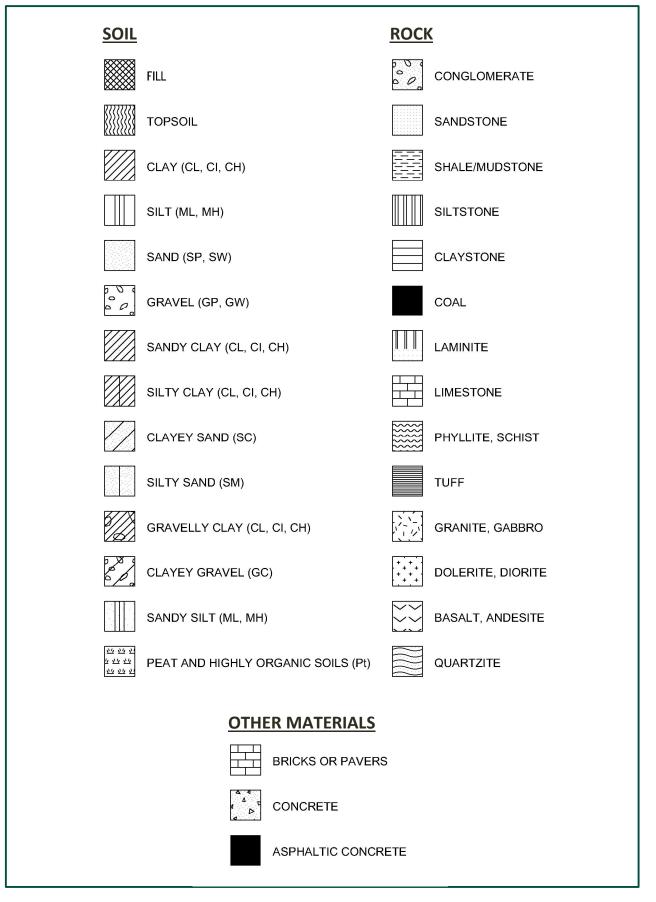
The presence of fill materials is usually regarded with caution as the possible variation in density and material type is much greater than with natural soil deposits. Consequently, there is an increased risk of adverse environmental characteristics or behaviour. If the volume and nature of fill is of importance to a project, then frequent test pit excavations are preferable to boreholes.

LABORATORY TESTING

Laboratory testing has not been undertaken to confirm the soil classification and rock strengths indicated on the environmental logs unless noted in the report.



SYMBOL LEGENDS



CLASSIFICATION OF COARSE AND FINE GRAINED SOILS

Ma	Group Major Divisions Symbol		Typical Names	Field Classification of Sand and Gravel	Laboratory Classification		
ianis	GRAVEL (more than half of coarse fraction is larger than 2.36mm		Gravel and gravel-sand mixtures, little or no fines	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	≤ 5% fines	C _u >4 1 <c<sub>c<3</c<sub>	
oversize fraction is			Gravel and gravel-sand mixtures, little or no fines, uniform gravels	Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	≤ 5% fines	Fails to comply with above	
		GM	Gravel-silt mixtures and gravel- sand-silt mixtures	'Dirty' materials with excess of non-plastic fines, zero to medium dry strength	≥ 12% fines, fines are silty	Fines behave as silt	
of sail exd	20 0005mm		Gravel-clay mixtures and gravel- sand-clay mixtures	'Dirty' materials with excess of plastic fines, medium to high dry strength	≥ 12% fines, fines are clayey	Fines behave as clay	
than 65% sater than	SAND (more than half of coarse fraction is smaller than 2.36mm) SM		Sand and gravel-sand mixtures, little or no fines	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	≤ 5% fines	Cu>6 1 <cc<3< td=""></cc<3<>	
ail (mare. gn			Sand and gravel-sand mixtures, little or no fines	Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	≤ 5% fines	Fails to comply with above	
egraineds	2.36mm)	SM	Sand-silt mixtures	'Dirty' materials with excess of non-plastic fines, zero to medium dry strength	≥ 12% fines, fines are silty		
Coarse	SC SC		Sand-clay mixtures	'Dirty' materials with excess of plastic fines, medium to high dry strength	≥ 12% fines, fines are clayey	N/A	

					Laboratory Classification		
Majo	or Divisions	Group Symbol	Typical Names	Dry Strength	Dilatancy	Toughness	% < 0.075mm
gnbu	SILT and CLAY (low to medium plasticity) CL, Cl OL SILT and CLAY (low to medium plasticity) CL, Cl OL SILT and CLAY (high plasticity) CH OH		Inorganic silt and very fine sand, rock flour, silty or clayey fine sand or silt with low plasticity	None to low	Slow to rapid	Low	Below A line
of sail exdu 0.075mm)			CL, Cl Inorganic clay of low to medium plasticity, gravelly clay, sandy clay		None to slow	Medium	Above A line
an 35% ss than			Organic silt	Low to medium	Slow	Low	Below A line
onisle	SILT and CLAY		Inorganic silt	Low to medium	None to slow	Low to medium	Below A line
soils (m te fracti	(high plasticity)	СН	Inorganic clay of high plasticity	High to very high	None	High	Above A line
regrained	regrained. Oversiz		Organic clay of medium to high plasticity, organic silt	Medium to high	None to very slow	Low to medium	Below A line
.=	Highly organic soil	Pt	Peat, highly organic soil	-	-	-	-

Laboratory Classification Criteria

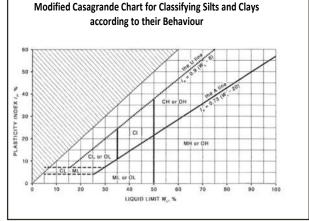
A well graded coarse grained soil is one for which the coefficient of uniformity Cu > 4 and the coefficient of curvature $1 < C_c < 3$. Otherwise, the soil is poorly graded. These coefficients are given by:

$$C_U = \frac{D_{60}}{D_{10}}$$
 and $C_C = \frac{(D_{30})^2}{D_{10}D_{60}}$

Where D_{10} , D_{30} and D_{60} are those grain sizes for which 10%, 30% and 60% of the soil grains, respectively, are smaller.

NOTES:

- 1 For a coarse grained soil with a fines content between 5% and 12%, the soil is given a dual classification comprising the two group symbols separated by a dash; for example, for a poorly graded gravel with between 5% and 12% silt fines, the classification is GP-GM.
- 2 Where the grading is determined from laboratory tests, it is defined by coefficients of curvature (C_c) and uniformity (C_u) derived from the particle size distribution curve.
- 3 Clay soils with liquid limits > 35% and ≤ 50% may be classified as being of medium plasticity.
- 4 The U line on the Modified Casagrande Chart is an approximate upper bound for most natural soils.



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LOG SYMBOLS

Log Column	Symbol	Definition				
Groundwater Record	—	Standing water level. Ti	me delay following compl	etion of drilling/excavation may be shown.		
	— с —	Extent of borehole/test	pit collapse shortly after o	drilling/excavation.		
		Groundwater seepage i	nto borehole or test pit no	oted during drilling or excavation.		
Samples	ES	Sample taken over dept	h indicated, for environm	ental analysis.		
	U50	Undisturbed 50mm diar	neter tube sample taken	over depth indicated.		
	DB		aken over depth indicated			
	DS	-	nple taken over depth ind			
	ASB		lepth indicated, for asbes	-		
	ASS		lepth indicated, for acid s	-		
	SAL	Soil sample taken over o	lepth indicated, for salinit	y analysis.		
	PFAS	Soil sample taken over o	lepth indicated, for analys	sis of Per- and Polyfluoroalkyl Substances.		
Field Tests	N = 17 4, 7, 10		150mm penetration. 'Refu	tween depths indicated by lines. Individual isal' refers to apparent hammer refusal within		
	N _c = 5	Solid Cone Penetration	Test (SCPT) performed b	etween depths indicated by lines. Individual		
	7	figures show blows per 150mm penetration for 60° solid cone driven by SPT hammer. 'R' refers to apparent hammer refusal within the corresponding 150mm depth increment.				
	3R					
	VNS = 25	Vane shear reading in kPa of undrained shear strength.				
	PID = 100	Photoionisation detector reading in ppm (soil sample headspace test).				
	FID = 100					
Moisture Condition	w > PL	Moisture content estimated to be greater than plastic limit.				
(Fine Grained Soils)	w≈PL	Moisture content estimated to be approximately equal to plastic limit.				
	w < PL	Moisture content estimated to be less than plastic limit.				
	w≈LL w>LL	Moisture content estimated to be near liquid limit. Moisture content estimated to be wet of liquid limit.				
(Coorse Crained Saile)						
(Coarse Grained Soils)	D	DRY – runs freely through fingers.				
	M W	MOIST – does not run freely but no free water visible on soil surface. WET – free water visible on soil surface.				
Strongth (Consistoney)						
Strength (Consistency) Cohesive Soils	VS S		fined compressive streng			
	F		SOFT- unconfined compressive strength > 25kPa and \leq 50kPa.FIRM- unconfined compressive strength > 50kPa and \leq 100kPa.			
	St					
	VSt			th > 100kPa and \leq 200kPa.		
	Hd			th > 200kPa and \leq 400kPa.		
	Fr		fined compressive streng			
	()		gth not attainable, soil cru			
		assessment.	cates estimated consiste	ncy based on tactile examination or other		
Density Index/ Relative Density			Density Index (I _D) Range (%)	SPT 'N' Value Range (Blows/300mm)		
(Cohesionless Soils)	VL	VERY LOOSE	≤15	0-4		
	L	LOOSE	$>$ 15 and \leq 35	4-10		
	MD	MEDIUM DENSE	$>$ 35 and \leq 65	10-30		
	D	DENSE	$>$ 65 and \leq 85	30 – 50		
	VD	VERY DENSE	> 85	> 50		
	()	Bracketed symbol indica	ates estimated density bas	sed on ease of drilling or other assessment.		



Log Column	Symbol	Definition			
Hand Penetrometer Readings	300 250	Measures reading in kPa of unconfined compressive strength. Numbers indicate individual test results on representative undisturbed material unless noted otherwise.			
Remarks	'V' bit	Hardened steel '	/' shaped bit.		
	'TC' bit	Twin pronged tu	ngsten carbide bit.		
	T_{60}	Penetration of au without rotation	iger string in mm under static load of rig applied by drill head hydraulics of augers.		
	Soil Origin	The geological or	igin of the soil can generally be described as:		
		RESIDUAL	 soil formed directly from insitu weathering of the underlying rock. No visible structure or fabric of the parent rock. 		
		EXTREMELY WEATHERED	 soil formed directly from insitu weathering of the underlying rock. Material is of soil strength but retains the structure and/or fabric of the parent rock. 		
		ALLUVIAL	 soil deposited by creeks and rivers. 		
		ESTUARINE	 soil deposited in coastal estuaries, including sediments caused by inflowing creeks and rivers, and tidal currents. 		
		MARINE	 soil deposited in a marine environment. 		
		AEOLIAN	 soil carried and deposited by wind. 		
		COLLUVIAL	 soil and rock debris transported downslope by gravity, with or without the assistance of flowing water. Colluvium is usually a thick deposit formed from a landslide. The description 'slopewash' is used for thinner surficial deposits. 		
		LITTORAL	 beach deposited soil. 		



Classification of Material Weathering

Term	Term		viation	Definition	
Residual Soil		R	RS	Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are no longer visible but the soil has not been significantly transported.	
Extremely Weathered		xw		Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are still visible.	
Highly Weathered	Distinctly Weathered	,		The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable. Rock strength is significantly changed by weathering. Some primary minerals have weathered to clay minerals. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores.	
Moderately Weathered	(Note 1)	MW		The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable, but shows little or no change of strength from fresh rock.	
Slightly Weathered		SW		Rock is partially discoloured with staining or bleaching along joints but shows little or no change of strength from fresh rock.	
Fresh		FR		Rock shows no sign of decomposition of individual minerals or colour changes.	

NOTE 1: The term 'Distinctly Weathered' is used where it is not practicable to distinguish between 'Highly Weathered' and 'Moderately Weathered' rock. 'Distinctly Weathered' is defined as follows: '*Rock strength usually changed by weathering.* The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores'. There is some change in rock strength.

Rock Material Strength Classification

			Guide to Strength		
Term	Abbreviation	Uniaxial Compressive Strength (MPa)	Point Load Strength Index Is ₍₅₀₎ (MPa)	Field Assessment	
Very Low Strength	VL	0.6 to 2	0.03 to 0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxial sample by hand. Pieces up to 30mm thick can be broken by finger pressure.	
Low Strength	L	2 to 6	0.1 to 0.3	Easily scored with a knife; indentations 1mm to 3mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150mm long by 50mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.	
Medium Strength	М	6 to 20	0.3 to 1	Scored with a knife; a piece of core 150mm long by 50mm diameter can be broken by hand with difficulty.	
High Strength	н	20 to 60	1 to 3	A piece of core 150mm long by 50mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.	
Very High Strength	VH	60 to 200	3 to 10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.	
Extremely High Strength	EH	> 200	> 10	Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.	



Appendix E: Laboratory Reports & COC Documents





CERTIFICATE OF ANALYSIS 326110

Client Details	
Client	JK Environments
Attention	C Ridley
Address	PO Box 976, North Ryde BC, NSW, 1670

Sample Details	
Your Reference	E36107BR, North Narrabeen
Number of Samples	20 Soil
Date samples received	21/06/2023
Date completed instructions received	21/06/2023

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Report Details					
Date results requested by	28/06/2023				
Date of Issue	28/06/2023				
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Accredited for compliance with ISO/IEC 17025 - Testing. Tests not covered by NATA are denoted with *					

Results Approved By Diego Bigolin, Inorganics Supervisor <u>Authorised By</u> Nancy Zhang, Laboratory Manager



Client Reference: E36107BR, North Narrabeen

sPOCAS field test						
Our Reference		326110-1	326110-2	326110-3	326110-4	326110-5
Your Reference	UNITS	BH2	BH2	BH2	BH2	BH2
Depth		0.08-0.2	0.4-0.5	0.9-1.0	1.5-1.6	1.9-2.0
Date Sampled		21/06/2023	21/06/2023	21/06/2023	21/06/2023	21/06/2023
Type of sample		Soil	Soil	Soil	Soil	Soil
Date prepared	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
Date analysed	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
pH⊧ (field pH test)	pH Units	9.9	9.9	9.6	9.7	9.7
pHFOX (field peroxide test)	pH Units	6.4	6.5	6.7	6.7	6.7
Reaction Rate*	-	Low reaction				

sPOCAS field test						
Our Reference		326110-6	326110-7	326110-8	326110-9	326110-10
Your Reference	UNITS	BH5	BH5	BH5	BH5	BH5
Depth		0.1-0.2	0.5-0.6	1.0-1.1	1.5-1.6	1.9-2.0
Date Sampled		21/06/2023	21/06/2023	21/06/2023	21/06/2023	21/06/2023
Type of sample		Soil	Soil	Soil	Soil	Soil
Date prepared	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
Date analysed	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
pH _F (field pH test)	pH Units	10.8	9.8	9.8	9.7	9.5
pH _{FOX} (field peroxide test)	pH Units	6.8	6.5	6.7	6.5	6.7
Reaction Rate*	-	Low reaction				

sPOCAS field test						
Our Reference		326110-11	326110-12	326110-13	326110-14	326110-15
Your Reference	UNITS	BH6	BH6	BH6	BH6	BH6
Depth		0-0.1	0.5-0.6	1.0-1.1	1.5-1.6	1.9-2.0
Date Sampled		21/06/2023	21/06/2023	21/06/2023	21/06/2023	21/06/2023
Type of sample		Soil	Soil	Soil	Soil	Soil
Date prepared	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
Date analysed	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
pH⊧ (field pH test)	pH Units	8.5	9.1	9.4	9.5	9.5
pH _{FOX} (field peroxide test)	pH Units	6.2	6.5	6.4	6.5	6.5
Reaction Rate*	-	Low reaction				

Client Reference: E36107BR, North Narrabeen

sPOCAS field test						_
Our Reference		326110-16	326110-17	326110-18	326110-19	326110-20
Your Reference	UNITS	BH7	BH7	BH7	BH7	BH7
Depth		0-0.1	0.5-0.6	1.0-1.1	1.5-1.6	2.0-2.1
Date Sampled		21/06/2023	21/06/2023	21/06/2023	21/06/2023	21/06/2023
Type of sample		Soil	Soil	Soil	Soil	Soil
Date prepared	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
Date analysed	-	22/06/2023	22/06/2023	22/06/2023	22/06/2023	22/06/2023
pH⊧ (field pH test)	pH Units	9.0	9.0	9.3	9.3	9.3
pHFOX (field peroxide test)	pH Units	6.3	6.5	6.4	6.6	6.6
Reaction Rate*	-	Low reaction				

Method ID	Methodology Summary
Inorg-063	pH- measured using pH meter and electrode. Soil is oxidised with Hydrogen Peroxide or extracted with water. To ensure accurate results these tests are recommended to be done in the field as pH may change with time thus these results may not be representative of true field conditions.

QUALITY CONTROL: sPOCAS field test						Du	Spike Recovery %			
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date prepared	-			[NT]	[NT]		[NT]	[NT]	22/06/2023	
Date analysed	-			[NT]	[NT]		[NT]	[NT]	22/06/2023	
pH _F (field pH test)	pH Units		Inorg-063	[NT]	[NT]		[NT]	[NT]	99	
pH _{FOX} (field peroxide test)	pH Units		Inorg-063	[NT]	[NT]	[NT]	[NT]	[NT]	99	[NT]

Result Definiti	ons
NT	Not tested
NA	Test not required
INS	Insufficient sample for this test
PQL	Practical Quantitation Limit
<	Less than
>	Greater than
RPD	Relative Percent Difference
LCS	Laboratory Control Sample
NS	Not specified
NEPM	National Environmental Protection Measure
NR	Not Reported

Quality Contro	ol Definitions
Blank	This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.
Duplicate	This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.
Matrix Spike	A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.
LCS (Laboratory Control Sample)	This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.
Surrogate Spike	Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

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Guideline limits for Rinse Water Quality reported as per analytical requirements and specifications of AS 4187, Amdt 2 2019, Table 7.2

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: >10xPQL - RPD acceptance criteria will vary depending on the analytes and the analytical techniques but is typically in the range 20%-50% – see ELN-P05 QA/QC tables for details; <10xPQL - RPD are higher as the results approach PQL and the estimated measurement uncertainty will statistically increase.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals (not SPOCAS); 60-140% for organics/SPOCAS (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Where matrix spike recoveries fall below the lower limit of the acceptance criteria (e.g. for non-labile or standard Organics <60%), positive result(s) in the parent sample will subsequently have a higher than typical estimated uncertainty (MU estimates supplied on request) and in these circumstances the sample result is likely biased significantly low.

Measurement Uncertainty estimates are available for most tests upon request.

Analysis of aqueous samples typically involves the extraction/digestion and/or analysis of the liquid phase only (i.e. NOT any settled sediment phase but inclusive of suspended particles if present), unless stipulated on the Envirolab COC and/or by correspondence. Notable exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, total recoverable metals and PFAS where solids are included by default.

Samples for Microbiological analysis (not Amoeba forms) received outside of the 2-8°C temperature range do not meet the ideal cooling conditions as stated in AS2031-2012.



SAMPLE RECEIPT ADVICE

Client Details	
Client	JK Environments
Attention	C Ridley

Sample Login Details	
Your reference	E36107BR, North Narrabeen
Envirolab Reference	326110
Date Sample Received	21/06/2023
Date Instructions Received	21/06/2023
Date Results Expected to be Reported	28/06/2023

Sample Condition	
Samples received in appropriate condition for analysis	Yes
No. of Samples Provided	20 Soil
Turnaround Time Requested	Standard
Temperature on Receipt (°C)	11
Cooling Method	Ice
Sampling Date Provided	YES

Comments Nil

Please direct any queries to:

Aileen Hie	Jacinta Hurst							
Phone: 02 9910 6200	Phone: 02 9910 6200							
Fax: 02 9910 6201	Fax: 02 9910 6201							
Email: ahie@envirolab.com.au	Email: jhurst@envirolab.com.au							

Analysis Underway, details on the following page:



Sample ID	sPOCAS field test
BH2-0.08-0.2	\checkmark
BH2-0.4-0.5	• • <t< td=""></t<>
BH2-0.9-1.0	✓
BH2-1.5-1.6	\checkmark
BH2-1.9-2.0	✓
BH5-0.1-0.2	✓
BH5-0.5-0.6	✓
BH5-1.0-1.1	✓
BH5-1.5-1.6	✓
BH5-1.9-2.0	✓
BH6-0-0.1	\checkmark
BH6-0.5-0.6	\checkmark
BH6-1.0-1.1	\checkmark
BH6-1.5-1.6	\checkmark
BH6-1.9-2.0	✓
BH7-0-0.1	✓
BH7-0.5-0.6	✓
BH7-1.0-1.1	\checkmark
BH7-1.5-1.6	\checkmark
BH7-2.0-2.1	\checkmark

The '\screw' indicates the testing you have requested. THIS IS NOT A REPORT OF THE RESULTS.

Additional Info

Sample storage - Waters are routinely disposed of approximately 1 month and soils approximately 2 months from receipt.

Requests for longer term sample storage must be received in writing.

Please contact the laboratory immediately if observed settled sediment present in water samples is to be included in the extraction and/or analysis (exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, Total Recoverable metals and PFAS analysis where solids are included by default.

TAT for Micro is dependent on incubation. This varies from 3 to 6 days.

SAMPLE AND CHAIN OF CUSTODY FORM

<u>TO:</u> ENVIROLAB S						300				FROM	<u>/l:</u>		-	-			
ENVIROLAB SERVICES PTY LTD 12 ASHLEY STREET		JKE Job Number: E36107BR					Þ										
CHATSWOOD NSW 2067						JKEnvironments											
P: (02) 99106200			Date Result	s STAN	DARD		•		REAR OF 115 WICKS ROAD								
F: (02) 99106)	F: (02) 99106201			Required:						MACQUARIE PARK, NSW 2113							
Attention: Ai	leen			Page:	1 of 1		-	1		P: 02-9888 5000 F: 02-9888 5001 Attention: Craig Ridley							
	<u> </u>					1						_			s.com	<u>au</u>	
Location:		Narrabeen							Samp				sky on	lce			
Sampler:	AD/CE	<u> </u>					_	<u>г</u>		Te	sts Re	quire	d 1				
Date Sampled	Lab Ref:	Sample Number	Depth (m)	Sample Container	Sample Description	SCr extended	pH field test (pHF apHFOX)										
21/06/2023	1	вна	0.08-0.2	P	Sand		x										
21/06/2023	3	вна	0.4-0.5	P	Sand		x										
21/06/2023	3	вн2	0.9-1.0	Р	Sand		x										
21/06/2023	4	8Н2	1.5-1.6	Р	Sand		x										
21/06/2023	5	вна	1.9-2.0	P	Sand		х										
21/06/2023	6	BH5	0.1-0.2	Р	Sand		х										
21/06/2023	7	вн5	0.5-0.6	Р	Sand ₂		х										
21/06/2023	8	вн5	1.0-1.1	Р	Sand		х										
21/06/2023	9	вна	1.5-1.6	Р	Sand		x										
21/06/2023	10	BHŚ	1.9-2.0	Р	Sand		x										
21/05/2023	11	вне	0-0.1	Р	F: Sand		х		_								
21/06/2023	12	вне	0.5-0.6	Р	Sand		х										
21/06/2023	13	вна	1.0-1.1	Р	Sand		x										
21/05/2023	14	внб	1.5-1.6	Р	Sand		х										
21/06/2023	15	вна	1.9-2.0	Р	Sand		х										
21/06/2023	16	вн7	0-0.1	Р	F: Sand		х										
21/06/2023	17	BH7	0.5-0.6	Р	F: Sand		х							ات کەر			
21/06/2023	18	BH7	1.0-1.1	Р	Sand		х		E	้างเสิด	LAB	<u>-</u> -	1	2 Ashi	ey St 2067		
21/06/2023		BH7	1.5-1.6	Р	Sand		х			C. 00.	ľ.	ļ į	h: (02	9910	6200		
21/06/2023	20,	BH7	2.0-2.1	P	Sand		х		J		<u>¤.</u> 3	261	(0	~			
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Remarks (con	ments	/detection lim	its required):	1		Samp	le Conta	iners:				L	I				
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Relinquished	Вү:			Date:		_	astic Bag I	_	_	Recei	ved B				Date:		
LAD				21/06/	23	12:	45	44S)	EL	5	U	14	(nt 0	Date: 2[/	61	23



CERTIFICATE OF ANALYSIS 326110-A

Client Details	
Client	JK Environments
Attention	Alexis Diodati
Address	PO Box 976, North Ryde BC, NSW, 1670

Sample Details	
Your Reference	E36107BR, North Narrabeen
Number of Samples	additional analysis
Date samples received	21/06/2023
Date completed instructions received	30/06/2023

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Report Details		
Date results requested by	07/07/2023	
Date of Issue	07/07/2023	
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Accredited for compliance with ISO/IEC 17025 - Testing. Tests not covered by NATA are denoted with *		

<u>Results Approved By</u> Nick Sarlamis, Assistant Operation Manager <u>Authorised By</u> Nancy Zhang, Laboratory Manager



Chromium Suite						
Our Reference		326110-A-1	326110-A-4	326110-A-7	326110-A-13	326110-A-20
Your Reference	UNITS	BH2	BH2	BH5	BH6	BH7
Depth		0.08-0.2	1.5-1.6	0.5-0.6	1.0-1.1	2.0-2.1
Date Sampled		21/06/2023	21/06/2023	21/06/2023	21/06/2023	21/06/2023
Type of sample		Soil	Soil	Soil	Soil	Soil
Date prepared	-	06/07/2023	06/07/2023	06/07/2023	06/07/2023	06/07/2023
Date analysed	-	06/07/2023	06/07/2023	06/07/2023	06/07/2023	06/07/2023
pH _{kcl}	pH units	9.1	9.4	9.2	9.6	9.0
s-TAA pH 6.5	%w/w S	<0.01	<0.01	<0.01	<0.01	<0.01
TAA pH 6.5	moles H+ /t	<5	<5	<5	<5	<5
Chromium Reducible Sulfur	%w/w	<0.005	<0.005	<0.005	<0.005	<0.005
a-Chromium Reducible Sulfur	moles H+ /t	<3	<3	<3	<3	<3
S _{HCI}	%w/w S	[NT]	[NT]	[NT]	[NT]	[NT]
Sксi	%w/w S	[NT]	[NT]	[NT]	[NT]	[NT]
Snas	%w/w S	[NT]	[NT]	[NT]	[NT]	[NT]
ANC _{BT}	% CaCO₃	6.6	6.7	7.0	5.0	5.2
s-ANC _{BT}	%w/w S	2.1	2.1	2.2	1.6	1.7
s-Net Acidity	%w/w S	<0.005	<0.005	<0.005	<0.005	<0.005
a-Net Acidity	moles H+ /t	<5	<5	<5	<5	<5
Liming rate	kg CaCO₃ /t	<0.75	<0.75	<0.75	<0.75	<0.75
a-Net Acidity without ANCE	moles H+ /t	<5	<5	<5	<5	<5
Liming rate without ANCE	kg CaCO₃ /t	<0.75	<0.75	<0.75	<0.75	<0.75
s-Net Acidity without ANCE	%w/w S	<0.005	<0.005	<0.005	<0.005	0.0050

Method ID	Methodology Summary
Inorg-068	Chromium Reducible Sulfur - Hydrogen Sulfide is quantified by iodometric titration after distillation to determine potential acidity.
	Net acidity including ANC has a safety factor of 1.5 applied.
	Neutralising value (NV) of 100% is assumed for liming rate.
	The recommendation that the SHCL concentration be multiplied by a factor of 2 to ensure retained acidity is not underestimated, has not been applied in the SHCL result. However, it has been applied in the SNAS calculation: SNAS % = (SHCL-SKCL)x2

QUALIT	Y CONTROL	Chromiu	m Suite			Du	plicate		Spike Red	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date prepared	-			06/07/2023	1	06/07/2023	06/07/2023		06/07/2023	
Date analysed	-			06/07/2023	1	06/07/2023	06/07/2023		06/07/2023	
pH _{kcl}	pH units		Inorg-068	[NT]	1	9.1	9.2	1	98	
s-TAA pH 6.5	%w/w S	0.01	Inorg-068	<0.01	1	<0.01	<0.01	0	[NT]	
ТАА рН 6.5	moles H+/t	5	Inorg-068	<5	1	<5	<5	0	99	
Chromium Reducible Sulfur	%w/w	0.005	Inorg-068	<0.005	1	<0.005	<0.005	0	101	
a-Chromium Reducible Sulfur	moles H+/t	3	Inorg-068	<3	1	<3	<3	0	[NT]	
S _{HCI}	%w/w S	0.005	Inorg-068	<0.005	1		[NT]		[NT]	
S _{KCI}	%w/w S	0.005	Inorg-068	<0.005	1		[NT]		[NT]	
S _{NAS}	%w/w S	0.005	Inorg-068	<0.005	1		[NT]		[NT]	
ANC _{BT}	% CaCO₃	0.05	Inorg-068	<0.05	1	6.6	6.4	3	101	
s-ANC _{BT}	%w/w S	0.05	Inorg-068	<0.05	1	2.1	2.1	0	[NT]	
s-Net Acidity	%w/w S	0.005	Inorg-068	<0.005	1	<0.005	<0.005	0	[NT]	
a-Net Acidity	moles H ⁺ /t	5	Inorg-068	<5	1	<5	<5	0	[NT]	
Liming rate	kg CaCO₃/t	0.75	Inorg-068	<0.75	1	<0.75	<0.75	0	[NT]	
a-Net Acidity without ANCE	moles H*/t	5	Inorg-068	<5	1	<5	<5	0	[NT]	
Liming rate without ANCE	kg CaCO₃/t	0.75	Inorg-068	<0.75	1	<0.75	<0.75	0	[NT]	
s-Net Acidity without ANCE	%w/w S	0.005	Inorg-068	<0.005	1	<0.005	<0.005	0	[NT]	

Result Definiti	ons
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Where matrix spike recoveries fall below the lower limit of the acceptance criteria (e.g. for non-labile or standard Organics <60%), positive result(s) in the parent sample will subsequently have a higher than typical estimated uncertainty (MU estimates supplied on request) and in these circumstances the sample result is likely biased significantly low.

Measurement Uncertainty estimates are available for most tests upon request.

Analysis of aqueous samples typically involves the extraction/digestion and/or analysis of the liquid phase only (i.e. NOT any settled sediment phase but inclusive of suspended particles if present), unless stipulated on the Envirolab COC and/or by correspondence. Notable exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, total recoverable metals and PFAS where solids are included by default.

Samples for Microbiological analysis (not Amoeba forms) received outside of the 2-8°C temperature range do not meet the ideal cooling conditions as stated in AS2031-2012.



SAMPLE RECEIPT ADVICE

Client Details	
Client	JK Environments
Attention	Alexis Diodati

Sample Login Details	
Your reference	E36107BR, North Narrabeen
Envirolab Reference	326110-A
Date Sample Received	21/06/2023
Date Instructions Received	30/06/2023
Date Results Expected to be Reported	07/07/2023

Sample Condition	
Samples received in appropriate condition for analysis	Yes
No. of Samples Provided	additional analysis
Turnaround Time Requested	Standard
Temperature on Receipt (°C)	11
Cooling Method	Ice
Sampling Date Provided	YES

Comments Nil

Please direct any queries to:

Aileen Hie	Jacinta Hurst
Phone: 02 9910 6200	Phone: 02 9910 6200
Fax: 02 9910 6201	Fax: 02 9910 6201
Email: ahie@envirolab.com.au	Email: jhurst@envirolab.com.au

Analysis Underway, details on the following page:



Sample ID	Chromium Suite	On Hold
BH2-0.08-0.2	\checkmark	
BH2-0.4-0.5		✓
BH2-0.9-1.0		\checkmark
BH2-1.5-1.6	\checkmark	
BH2-1.9-2.0		\checkmark
BH5-0.1-0.2		\checkmark
BH5-0.5-0.6	\checkmark	
BH5-1.0-1.1		\checkmark
BH5-1.5-1.6		\checkmark
BH5-1.9-2.0		✓ ✓ ✓
BH6-0-0.1		\checkmark
BH6-0.5-0.6		\checkmark
BH6-1.0-1.1	\checkmark	
BH6-1.5-1.6		✓
BH6-1.9-2.0		✓ ✓ ✓ ✓
BH7-0-0.1		\checkmark
BH7-0.5-0.6		\checkmark
BH7-1.0-1.1		\checkmark
BH7-1.5-1.6		\checkmark
BH7-2.0-2.1	\checkmark	

The '\' indicates the testing you have requested. THIS IS NOT A REPORT OF THE RESULTS.

Additional Info

Sample storage - Waters are routinely disposed of approximately 1 month and soils approximately 2 months from receipt.

Requests for longer term sample storage must be received in writing.

Please contact the laboratory immediately if observed settled sediment present in water samples is to be included in the extraction and/or analysis (exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, Total Recoverable metals and PFAS analysis where solids are included by default.

TAT for Micro is dependent on incubation. This varies from 3 to 6 days.

Ming To

From:	Alexis Diodati <adiodati@jkenvironments.com.au></adiodati@jkenvironments.com.au>
Sent:	Friday, 30 June 2023 1:17 PM
To:	Samplereceipt
Subject:	Additional Analysis for Registration 326110 (JKE Ref: E36107BR North Narrabeen)
Categories:	Additional

CAUTION: This email originated from outside of the organisation. Do not act on instructions, click links or open attachments unless you recognise the sender and know the content is authentic and safe.

Hi team,

Could we please order the SCr (extended) suite analysis on the samples below (standard TAT)

Ref: 32610-A 7A7: Stanclard Due: 07/07/2023

 BH2
 0.08-0.2
 (1)

 BH2
 1.5-1.6
 (4-)

 BH5
 0.5-0.6
 (1)

 BH6
 1.0-1.1
 (13)

 BH7
 2.0-2.1
 (20)

Thank you

Regards Alexis Diodati Environmental Scientist



JKEnvironments

PO Box 976 NORTH RYDE BC NSW 1670 115 Wicks Road MACQUARIE PARK NSW 2113

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