GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Deve	Development Application for Name of Applicant							
Addı	Address of site 13 Minkara Road, Bayview							
		the minimum requirements to be addressed in a Geotechnical Risk Declaration made by ineering geologist or coastal engineer (where applicable) as part of a geotechnical report						
I,	Ben White (Insert Name)	on behalf of White Geotechnical Group Pty Ltd (Trading or Company Name)						
engine organi:	er as defined by the Ge	certify that I am a geotechnical engineer or engineering geologist or coastal eotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the above this document and to certify that the organisation/company has a current professional indemnity						
l: Please	e mark appropriate box							
	have prepared the de	etailed Geotechnical Report referenced below in accordance with the Australia Geomechanics Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for						
	am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009							
	have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.							
	have examined the sit Application only invo	te and the proposed development/alteration in detail and I am of the opinion that the Development olves Minor Development/Alteration that does not require a Geotechnical Report or Risk the my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009						
	have examined the sit Hazard and does not the Geotechnical Risk	te and the proposed development/alteration is separate from and is not affected by a Geotechnical require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with a Management Policy for Pittwater - 2009 requirements.						
□ ○ 4-	·	astal process and coastal forces analysis for inclusion in the Geotechnical Report						
Geore	Report Title: Geotechr	nical Report 13 Minkara Road, Bayview						
	Report Date: 3/6/19							
	Author: BEN WHITE							
	Author's Company/Org	ganisation: WHITE GEOTECHNICAL GROUP PTY LTD						
Docur	mentation which relate t	o or are relied upon in report preparation:						
		nechanics Society Landslide Risk Management March 2007.						
	White Geotechn	nical Group company archives.						
Develo Risk M Manag	opment Application for thi Management aspects of t gement" level for the life o	eotechnical Report, prepared for the abovementioned site is to be submitted in support of a s site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical the proposed development have been adequately addressed to achieve an "Acceptable Risk of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and easures have been identified to remove foreseeable risk.						

Signature

Name Ben White

Chartered Professional Status MScGEOLAusIMM CP GEOL

Membership No. 222757

Company White Geotechnical Group Pty Ltd

GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Name of Applicant Address of site 13 Minkara Road, Bayview The following checklist covers the minimum requirements to be addressed in a Geotechnical Risk Management Geotechnical Report. This checklist is to accompany the Geotechnical Report and its certification (Form No. 1). Geotechnical Report Details: Report Title: Geotechnical Report 13 Minkara Road, Bayview Report Date: 3/6/19 Author's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD Please mark appropriate box Comprehensive site mapping conducted 28/5/19 (date) Mapping details presented on contoured site plan with geomorphic mapping to a minimum scale of 1:200 (as appropriate) Subsurface investigation required No Justification Yes Date conducted 28/5/19 Geotechnical model developed and reported as an inferred subsurface type-section Geotechnical model developed and reported as an inferred subsurface type-section Geotechnical model developed and reported Risk assessment conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Consequence analysis Risk calculation Risk assessment for property conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Risk assessment for property conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 Opinion has been provided that the design can achieve the "Acceptable Risk Management" criteria provided that the specify Geotechnical Conditions to be applied to all four phases as described in the Geotechnical Ris	Development Application for					
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Pittwater - 2009 have been specified	for					
Additional action to remove risk where reasonable and practical have been identified and included in the report.						
☐ Risk assessment within Bushfire Asset Protection Zone.						
I am aware that Pittwater Council will rely on the Geotechnical Report, to which this checklist applies, as the basis for ensuri that the geotechnical risk management aspects of the proposal have been adequately addressed to achieve an "Acceptable R Management" level for the life of the structure, taken as at least 100 years unless otherwise stated, and justified in the Repand that reasonable and practical measures have been identified to remove foreseeable risk.	able Risk					
Signature						
Name Ben White						
Chartered Professional Status MScGEOLAusIMM CP GEOL						
Membership No. 222757						

Company White Geotechnical Group Pty Ltd



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GEOTECHNICAL INVESTIGATION:

New Shed, Tennis Court, Carport, and Awning at 13 Minkara Road, Bayview

1. Proposed Development

- 1.1 Construct a new shed with storage under on the downhill side of the property by excavating to a maximum depth of ~2.2m.
- **1.2** Construct a new tennis court on the downhill side of the property.
- **1.3** Construct a new carport on the uphill side of the office.
- **1.4** Construct a new awning on the uphill side of the house.
- **1.5** Details of the proposed development are shown on 9 drawings prepared by Blue Sky Building Designs, Project number 2018049, drawings numbered A101 to 109, dated 25/2/19.

2. Site Description

- **2.1** The site was inspected on the 28th May, 2019, and previously on the 4th December, 2018.
- 2.2 This large rural/residential property is accessed by a long brick driveway off Minkara Road. The property has a N aspect. The block is located on the gently graded upper reaches of a hillslope. The natural surface falls across the property at an average angle of \sim 5°. The slope above and below the property continues at similar angles. No signs of movement related to slope instability were observed over the land surface or in the built structures on the property.
- **2.3** At the road frontage, a long brick driveway runs across the slope to the property (Photo 1). The driveway runs to a parking area on the E side of the site, garages on the E side of the office (Photo 2), and to a carport and parking area on the uphill side of the house (Photo 3). A dam has been constructed in the SE corner of the



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property (Photo 4). The dam recently went through the council approval process that involved this firm and it is currently considered stable. An excavation has been made in the slope for the house and office buildings. The cut is supported by a stable ~1.5m high sandstone block retaining wall (Photo 5). A pool has been cut into the slope to the W of the house (Photo 6). The water level of the pool indicates no ground movement has occurred in the shell of the pool since its construction. A creek runs down and under the W side of the property (Photo 7). A stable timber outbuilding has been constructed in the SW corner of the property (Photo 8). A large lawn area encompasses the majority of the downhill side of the property (Photo 9). Another dam has been constructed near the entrance to the property that will be removed as part of the proposed works (Photo 10). Competent Medium Strength Sandstone outcrops above this dam (Photo 11). The earthworks for the proposed tennis court (including a cut and fill) had already been completed prior to our first inspection (Photo 12). The earthworks were subject to a separate approval process and are currently considered stable.

3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by Hawkesbury Sandstone. It is described as a medium to coarse grained quartz sandstone with very minor shale and laminite lenses.

4. Subsurface Investigation

Twelve Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil, the relative density of the compacted crushed sandstone for the tennis court, and the depth to bedrock. The locations of the tests are shown on the site plan. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural



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rock surface. This is not expected to be an issue for the testing on this site and the results are as follows:

DCP TEST RESULTS – Dynamic Cone Penetrometer						
Equipment: 9kg hammer, 510mm drop, conical tip. Standard: AS1289.6.3.2 - 1997						
Depth(m) Blows/0.3m	DCP 1 (~RL120.1)	DCP 2 (~RL120.1)	DCP 3 (~RL120.0)	DCP 4 (~RL120.0)	DCP5 (~RL123.5)	DCP6 (~RL122.5)
0.0 to 0.3	27	17	25	25	7	Rock
0.3 to 0.6	#	#	25	18	8	Exposed at Surface
0.6 to 0.9			20	27	25	
0.9 to 1.2			12	20	#	
1.2 to 1.5			9	10		
1.5 to 1.8			8	7		
1.8 to 2.1			15	12		
2.1 to 2.4			8	14		
2.4 to 2.7			#	#		
	Refusal on Rock @ 0.1m	Refusal on Rock @ 0.1m	Refusal on Rock @ 2.3m	End of Test @ 2.4m	Refusal on Rock @ 0.8m	

#refusal/end of test. F = DCP fell after being struck showing little resistance through all or part of the interval.

DCP TEST RESULTS – Dynamic Cone Penetrometer						
Equipment: 9	Equipment: 9kg hammer, 510mm drop, conical tip. Standard: AS1289.6.3.2 - 199					
Depth(m) Blows/0.3m	DCP7 (~RL121.5)	DCP8 (~RL120.6)	DCP9 (~RL127.1)	DCP10 (~RL127.1)	DCP11 (~RL127.3)	DCP12 (~RL127.3)
0.0 to 0.3	3	8	7	5	6	18
0.3 to 0.6	8	7	25	25	#	#
0.6 to 0.9	17	6	20	#		
0.9 to 1.2	#	#	#			
	Refusal on Rock @ 0.9m	Refusal on Rock @ 0.9m	Refusal on Rock @ 0.8m	Refusal on Rock @ 0.6m	Refusal on Rock @ 0.1m	Refusal on Rock @ 0.3m

#refusal/end of test. F = DCP fell after being struck showing little resistance through all or part of the interval.



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DCP Notes:

- DCP1 Refusal on rock @ 0.1m, DCP bouncing off rock surface, yellow sandstone on wet tip.
- DCP2 Refusal on rock @ 0.1m, DCP bouncing off rock surface, clean dry tip.
- DCP3 Refusal on rock @ 2.3m, DCP bouncing off rock surface, yellow sand on damp tip.
- DCP4 End of test @ 2.4m, DCP still very slowly going down, muddy wet tip.
- DCP5 Refusal on rock @ 0.8m, DCP bouncing off rock surface, white impact dust on dry tip.
- DCP6 Rock exposed at surface.
- DCP7 Refusal on rock @ 0.9m, DCP bouncing off rock surface, brown sand on wet tip.
- DCP8 Refusal on rock @ 0.9m, DCP bouncing off rock surface, brown sand on wet tip.
- DCP9 Refusal on rock @ 0.8m, DCP bouncing off rock surface, wet muddy tip, test taken below $\sim 1.5m$ high retaining wall.
- DCP10 Refusal on rock @ 0.6m, DCP thudding, wet muddy tip, test taken below ~1.5m high retaining wall.
- DCP11 Refusal on rock @ 0.1m, DCP bouncing off rock surface, white impact dust on dry tip.
- DCP12 Refusal on rock @ 0.3m, DCP bouncing off rock surface, white impact dust on dry tip.

5. Geological Observations/Interpretation

The surface features of the block are controlled by the outcropping and underlying sandstone bedrock that steps down the property forming sub-horizontal benches between the steps. Where the grade is steeper, the steps are larger, and the benches narrower. Where the slope eases, the opposite is true. Where the rock is not exposed, it is overlain by natural sandy soils and firm to stiff sandy clays that fill the bench step formation. In DCPs 5 to 12, where it was not exposed, rock was encountered at depths of between 0.1 to 0.9m below the current surface, being slightly deeper due to the stepped nature of the underlying rock. The exposed sandstone across the site is estimated to be Medium Strength and a similar strength rock is expected to underly the entire site. See Type Section attached for a diagrammatical representation of the expected ground materials.

The earthworks for the proposed tennis court consist of a cut and fill (Photo 12). Competent Medium Strength Sandstone was observed to be outcropping through the low cut and DCPs 1 & 2 confirm that the sandstone underlies the surface at shallow depths across the uphill



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side. The ground tests confirm that the fill placed across the downhill side has been

adequately compacted to a consistency of hard clay/weathered rock. The fill overlies the

natural surface at a maximum depth of ~1.2m. Medium Strength Sandstone was then

encountered at a maximum depth of ~2.4m below the current surface.

6. Groundwater

Ground water seepage is expected to move over the buried surface of the rock and through

the cracks. As a creek flows down the W side of the block (Photo 7), we expect groundwater

seepage to be slightly higher across the block as slope seepage will move toward the creek.

Due to the slope and elevation of the block, the water table is expected to be many metres

below the base of the proposed excavation.

7. Surface Water

Apart from the flowing creek down the W side of the site, no evidence of surface flows were

observed on the property during the inspection. It is expected that normal sheet wash will

move onto the site from above the property during heavy down pours.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed above, below, or beside the property. The vibrations

from the proposed excavation are a potential hazard (Hazard One). A loose boulder, wedge,

or similar geological defect toppling onto the work site during the excavation process is a

potential hazard (Hazard Two).

RISK ANALYSIS SUMMARY ON THE NEXT PAGE



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Risk Analysis Summary

HAZARDS	Hazard One	Hazard Two
TYPE	The vibrations produced during the proposed excavation impacting on the surrounding structures.	A loose boulder, wedge, or similar geological defect toppling onto the work site during the excavation process.
LIKELIHOOD	'Possible' (10 ⁻³)	'Possible' (10 ⁻³)
CONSEQUENCES TO PROPERTY	'Medium' (15%)	'Medium' (20%)
RISK TO PROPERTY	'Moderate' (2 x 10 ⁻⁴)	'Moderate' (2 x 10 ⁻⁴)
RISK TO LIFE	5.3 x 10 ⁻⁷ /annum	4.6 x 10 ⁻⁵ /annum
COMMENTS	This level of risk to property is 'UNACCEPTABLE'. To move risk to 'ACCEPTABLE' levels the recommendations in Section 12 are to be followed.	This level of risk to life and property is 'UNACCEPTABLE'. To move risk to 'ACCEPTABLE' levels the recommendations in Section 13 are to be followed.

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.

10. Stormwater

There is fall to the creek that runs down the W side of the property (Photo 7). Roof water from the development is to be piped to the creek through any tanks that may be required by the regulating authorities. A diffuser is to be installed at the outlet of any new stormwater pipes that divert stormwater to the creek channel.



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11. Excavations

An excavation to a maximum depth of ~2.2m is required to construct the proposed shed. The

excavation is expected to be almost entirely through Medium Strength Sandstone.

It is envisaged that excavations through sandy soil and sandy clays can be carried out with a

bucket and excavations through rock will require grinding or rock sawing and breaking.

12. Vibrations

The proposed excavation is set back sufficiently from any surrounding structures or

boundaries so that vibrations from the excavation will not exceed tolerable limits for building

or infrastructure damage.

13. Excavation Support Requirements

No structures or boundaries will be within the zone of influence of the excavation.

The soil portions of the cut batters are to be battered temporarily at 1.0 Vertical to 2.0

Horizontal (30°) until the retaining walls are in place. Medium Strength Sandstone or better

will stand at vertical angles unsupported subject to approval by the geotechnical consultant.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion

works. The materials and labour to construct the retaining walls are to be organised so on

completion of the excavations they can be constructed as soon as possible. The excavations

are to be carried out during a dry period. No excavations are to commence if heavy or

prolonged rainfall is forecast.

Upon completion of the excavation, it is recommended the cut faces be supported with

retaining walls to prevent any potential future movement of joint blocks in the cut face that

can occur over time, when unfavourable jointing is obscured behind the excavation face.

Additionally, retaining walls will help control seepage and to prevent minor erosion and

sediment movement.



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During the excavation process, the geotechnical consultant is to inspect the cut batters in 1.5m intervals as they are lowered to ensure the ground materials are as expected and no wedges or other geological defects are present that could require additional support.

All excavation spoil is to be removed from site.

14. Retaining Walls

For cantilever or singly-propped retaining walls, it is suggested the design be based on a triangular pressure distribution of lateral pressures using the parameters shown in Table 1.

Table 1 - Likely Earth Pressures for Retaining Walls

	Earth Pressure Coefficients				
Unit	Unit weight (kN/m³)	'Active' K _a	'At Rest' K₀		
Sandy Soil	20	0.4	0.55		
Medium Strength Sandstone	24	0.00	0.01		

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the wall, do not account for any surcharge loads, and assume retaining walls are fully drained. Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining walls are to have sufficient back-wall drainage and be backfilled immediately behind the wall with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e. Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining walls, the likely hydrostatic pressures are to be accounted for in the structural design.



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15. Foundations

A concrete slab and shallow piers supported directly off Medium Strength Sandstone is a

suitable footing for the proposed shed. This material is expected to be exposed across most

of the base of the excavation. Where it is not exposed, and where the footprint of the

proposed shed does not fall over the excavation, piers will be required to maintain a uniform

bearing material.

Shallow piers supported directly off Medium Strength Sandstone is a suitable footing for the

proposed awning on the uphill side of the house. This material is expected to be encountered

at shallow depths.

The proposed carport slab on the uphill side of the office is to be supported on shallow piers

taken to the underlying Medium Strength Sandstone expected at ~0.6m below the current

surface in this location.

A maximum allowable bearing pressure of 800kPa can be assumed for footings on Medium

Strength Sandstone.

The density testing that was carried out on the earthworks for the proposed tennis court

confirmed the fill has been adequately compacted for a maximum allowable bearing pressure

of 100kPa.

Naturally occurring vertical cracks known as joints commonly occur in sandstone. These are

generally filled with soil and are the natural seepage paths through the rock. They can extend

to depths of several metres and are usually relatively narrow but can range between 0.1 to

0.8m wide. If a pad footing falls over a joint in the rock, the construction process is simplified

if with the approval of the structural engineer the joint can be spanned or, alternatively, the

footing can be repositioned so it does not fall over the joint.

NOTE: If the contractor is unsure of the footing material required, it is more cost effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on



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footing depth and material. This mostly prevents unnecessary over excavation in clay like

shaly rock but can be valuable in all types of geology.

16. Inspections

The client and builder are to familiarise themselves with the following required inspections

as well as council geotechnical policy. We cannot provide geotechnical certification for the

owner or the regulating authorities if the following inspections have not been carried out

during the construction process.

During the excavation process, the geotechnical consultant is to inspect the cut faces

as they are lowered in 1.5m intervals to ensure ground materials are as expected and

that there are no wedges or other defects present in the rock that may require

additional support.

All footings are to be inspected and approved by the geotechnical consultant while

the excavation equipment is still onsite and before steel reinforcing is placed or

concrete is poured.

White Geotechnical Group Pty Ltd.

electe

Ben White M.Sc. Geol., AuslMM., CP GEOL.

No. 222757

Engineering Geologist



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Photo 1



Photo 2



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Photo 3



Photo 4



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Photo 5



Photo 6



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Photo 7



Photo 8



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Photo 9



Photo 10



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Photo 11



Photo 12



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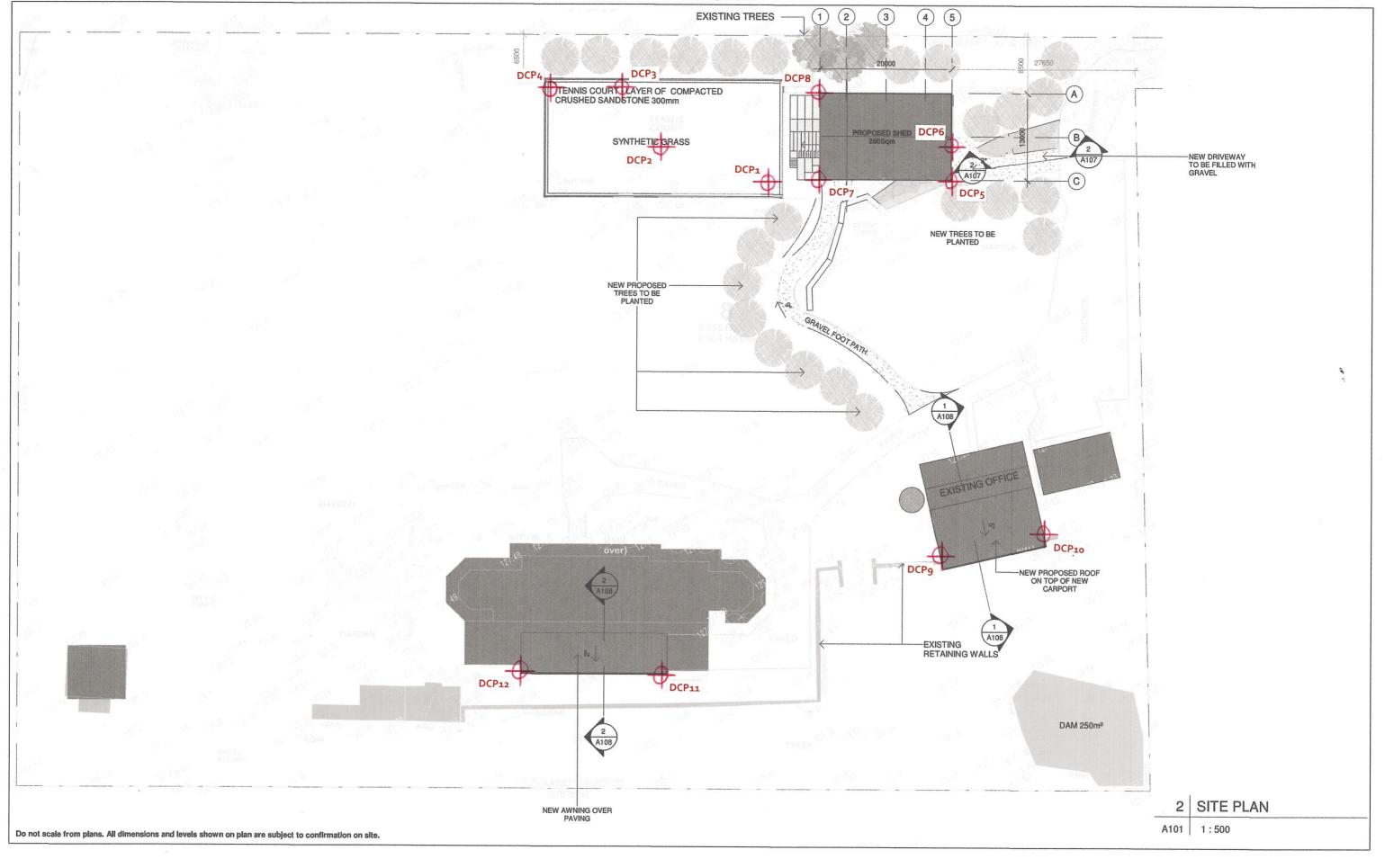
Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.

SITE PLAN – showing test locations



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AT: 13 Minkara Rd, Bayview

FOR: 3rd Solution Investment Pty Ltd

NEW PROPOSED SHED

PROJECT TITLE:

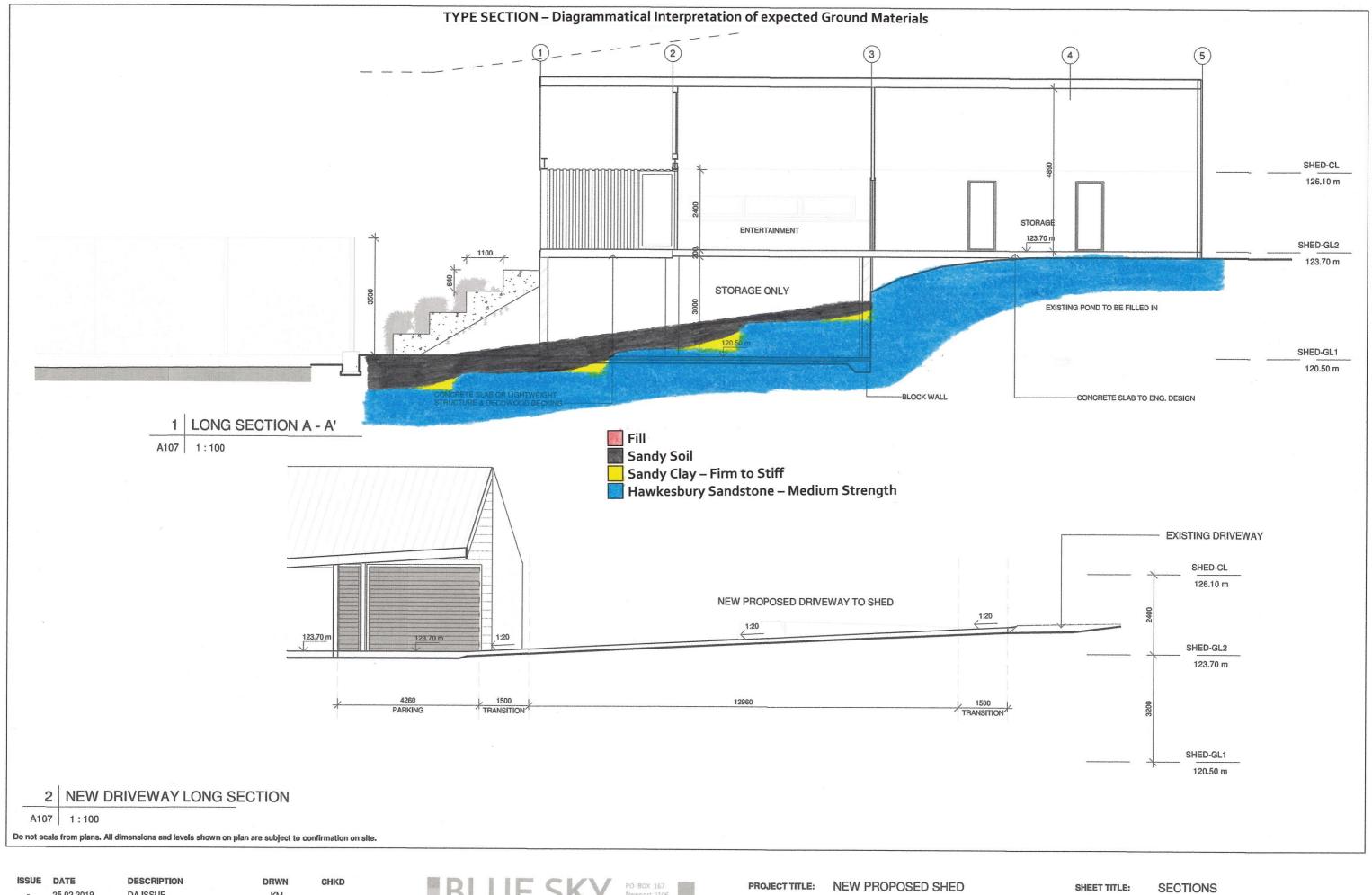
SHEET TITLE: SITE PLAN

A101

1:500

SHEET NO:

SCALE A3:



25.02.2019 DA ISSUE



2018049 PROJECT NO .:

A107

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FOR:

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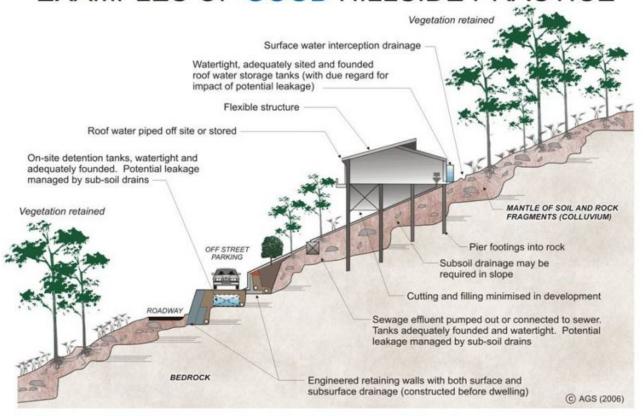
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EXAMPLES OF GOOD HILLSIDE PRACTICE



EXAMPLES OF POOR HILLSIDE PRACTICE

