GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Devel	opment Application	n for Name of Applicant	
Δddre	ss of site	34 Lumeah Avenue, Elanora Heights	
		ers the minimum requirements to be addressed in a Geotechnical Risk Declaration made by engineering geologist or coastal engineer (where applicable) as part of a geotechnical repo	ort
l,	Ben White (Insert Name)	on behalf of White Geotechnical Group Pty Ltd (Trading or Company Name)	
on this t	ho 1	1/3/21 certify that I am a geotechnical engineer or engineering geologist or coast	stal
enginee organisa	r as defined by the	e Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the about this document and to certify that the organisation/company has a current professional indemr	ove
: Please	mark appropriate b	oox	
\boxtimes		e detailed Geotechnical Report referenced below in accordance with the Australia Geomechan de Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy	
\boxtimes	accordance with the	chnically verify that the detailed Geotechnical Report referenced below has been prepared the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Management Policy for Pittwater - 2009	
	with Section 6.0 o assessment for the	ne site and the proposed development in detail and have carried out a risk assessment in accordar of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the reproposed development are in compliance with the Geotechnical Risk Management Policy and further detailed geotechnical reporting is not required for the subject site.	risk
	have examined the Application only Assessment and h	he site and the proposed development/alteration in detail and I am of the opinion that the Development/or involves Minor Development/Alteration that does not require a Geotechnical Report or R hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 20	lisk
	Hazard and does	ne site and the proposed development/alteration is separate from and is not affected by a Geotechni not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance w Risk Management Policy for Pittwater - 2009 requirements.	
		e coastal process and coastal forces analysis for inclusion in the Geotechnical Report	
Geotec	nnical Report Detai	ils:	
	Report Title: Geote Report Date: 1/3/2	echnical Report 34 Lumeah Avenue, Elanora Heights 21	
	Author: BEN WHI	ITE	
	Author's Company	//Organisation: WHITE GEOTECHNICAL GROUP PTY LTD	
Docum	entation which rela	ate to or are relied upon in report preparation:	
	Australian Ge	eomechanics Society Landslide Risk Management March 2007.	
	White Geoted	chnical Group company archives.	
Develop	ment Application for	e Geotechnical Report, prepared for the abovementioned site is to be submitted in support of this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechni of the proposed development have been adequately addressed to achieve an "Acceptable R	ical

Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature

Ben White

<u>Chartered Professional Status</u> <u>MScGEOLAusIMM CP GEOL</u>

<u>Membership No.</u> <u>222757</u>

Company White Geotechnical Group Pty Ltd

Name

GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Development Application for					
	Name of Applicant				
Addres	s of site	34 Lumeah Avenue, E	Elanora Heights		
Report. 7	This checklist is to ac	company the Geotechnical I	to be addressed in a Geotechnical Risk Management Geotechn Report and its certification (Form No. 1).	ical	
Geotech	nical Report Details	s: Report 34 Lumeah Avenu	In Flanora Hoights		
Report	Title. Geoleciilicai R	eport 34 Lumean Avent	de, Elanora Heights		
Report	Date: 1/3/21				
	BEN WHITE				
Author	's Company/Organi	isation: WHITE GEOTECHN	NICAL GROUP PTY LTD		
Please m	nark appropriate bo	×			
\boxtimes	Comprehensive site	mapping conducted 9/12/20 (date)			
\boxtimes	Mapping details pres Subsurface investiga	sented on contoured site plan v	with geomorphic mapping to a minimum scale of 1:200 (as appropriat	e)	
	⊠ Yes	Date conducted 9/12/20			
\boxtimes			inferred subsurface type-section		
\boxtimes	Geotechnical hazard				
	☐ Above				
	⊠ On the □ Below				
	☐ Beside				
\boxtimes		ls described and reported			
\boxtimes		•	e Geotechnical Risk Management Policy for Pittwater - 2009		
		quence analysis	·		
		ency analysis			
	Risk calculation				
\boxtimes			ance with the Geotechnical Risk Management Policy for Pittwater - 20		
\boxtimes	Assessed risks have	been compared to "Acceptable	rdance with the Geotechnical Risk Management Policy for Pittwater - le Risk Management" criteria as defined in the Geotechnical Risk	2009	
\boxtimes	•	ovided that the design can ach	nieve the "Acceptable Risk Management" criteria provided that the		
	specified conditions				
	Design Life Adopted ⊠ 100 ye				
	□ Other	als			
	- Other	specify			
	Geotechnical Conditi Pittwater - 2009 have	ions to be applied to all four ph	hases as described in the Geotechnical Risk Management Policy for		
\boxtimes			and practical have been identified and included in the report.		
	Risk assessment wit	hin Bushfire Asset Protection 2	Zone.		
I am aware that Pittwater Council will rely on the Geotechnical Report, to which this checklist applies, as the basis for ensuring that the geotechnical risk management aspects of the proposal have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated, and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.					
	Signature				
		Name	Ben White		
		Chartered Professional Stat	tus MScGEOLAusIMM CP GEOL		
		Membership No.	222757		

Company White Geotechnical Group Pty Ltd



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GEOTECHNICAL INVESTIGATION:

New House and Pool at 34 Lumeah Avenue, Elanora Heights

1. Proposed Development

- **1.1** Demolish the existing house, leaving the existing garage walls and garage foundations intact.
- 1.2 Construct a new house. Construct a new store room and lift connecting the garage level and ground floor level of the house.
- 1.3 Install a new pool by excavating to a maximum depth of ~2m.
- 1.4 Details of the proposed development are shown on 13 drawings prepared by Envirotecture, project number K35, drawings numbered 10.01, 11.01 to 03, 21.01 to 03, 30.01, 30.02, 40.01, 60.01, 63.01, 70.01 and 91.01, Revision A, dated 23/2/21.

2. Site Description

- **2.1** The site was inspected on the 9th of December, 2020.
- 2.2 This residential property is on the high side of the road and has a W aspect. It is located on the gently graded middle reaches of a hillslope. The natural slope falls across the property at an average angle of ~6°. The slopes above and below the property continue at similar angles.
- 2.3 At the road frontage, a concrete driveway runs to a garage under the downhill side of the house (Photos 1 & 2). Between the road frontage and the house is a gently sloping lawn. Medium Strength Hawkesbury Sandstone bedrock is outcropping on the S side of the house (Photo 3). The single storey brick house with garage below is supported by brick walls and a concrete slab (Photos 2 & 4). The external supporting walls show no significant signs of movement. A concrete patio with roof above extends



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off the uphill side of the house (Photo 5). A gently sloping lawn extends from the uphill side of the patio (Photo 6). No signs of slope instability were observed on the property. The adjoining neighbouring properties were observed to be in good order as seen from the street and subject property.

3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by Hawkesbury Sandstone. It is described as a medium to coarse grained quartz sandstone with very minor shale and laminite lenses.

4. Subsurface Investigation

One auger hole was put down to identify the soil materials. Five Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil and the depth to weathered rock. The locations of the tests are shown on the site plan. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural rock surface. This is not expected to be an issue for the testing on this site. But due to the possibility that the actual ground conditions vary from our interpretation there should be allowances in the excavation and foundation budget to account for this. We refer to the appended "Important Information about Your Report" to further clarify. The results are as follows:

AUGER HOLE 1 (~RL78.6) – AH1 (photo 7)

Depth (m)	Material Encountered
0.0 to 0.6	TOPSOIL, sandy soil, dark brown, moist, fine to medium grained with
	fine trace organic matter.
0.6 to 1.0	SANDY CLAY, light orange/brown, soft to firm, damp.
1.0 to 1.3	SANDY CLAY, white and orange red, firm to stiff, damp.
1.0 to 1.3	SANDY CLAY, white and orange red, firm to stiff, damp.

Refusal @ 1.3m auger grinding on rock surface. No watertable encountered.



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DCP TEST RESULTS – Dynamic Cone Penetrometer					
Equipment: 9kg hammer, 510mm drop, conical tip. Standa				andard: AS1289.6	5.3.2 - 1997
Depth(m) Blows/0.3m	DCP 1 (~RL75.4)	DCP 2 (~RL76.0)	DCP 3 (~RL78.1)	DCP 4 (~RL78.6)	DCP 5 (~RL77.6)
0.0 to 0.3	9	#	7	4	5
0.3 to 0.6	8		21	5	8
0.6 to 0.9	15		33	6	21
0.9 to 1.2	15		40	15	40
1.2 to 1.5	#		#	10	#
1.5 to 1.8				#	
	Refusal @ 0.9m	Rock exposed at surface	End of Test @ 1.1m	Refusal @ 1.3m	End of Test @ 1.2m

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

DCP Notes:

DCP1 – Refusal on rock @ 0.9m, DCP bouncing off rock surface, white sandstone fragments on dry tip.

DCP2 – Rock exposed at surface.

DCP3 – End of Test @ 1.1m, DCP still very slowly going down, white sandstone fragments on dry tip.

DCP4 – Refusal on rock @ 1.3m, DCP bouncing thudding, white impact dust and dark brown soil on dry tip

DCP5 – End of Test @ 1.2m, DCP still very slowly going down, white impact dust on dry tip and orange red clay on collar.

5. Geological Observations/Interpretation

The surface features of the block are controlled by the underlying sandstone bedrock that steps down the property forming sub-horizontal benches between the steps. Where the grade is steeper, the steps are larger and the benches narrower. Where the slope eases, the opposite is true. The rock is overlain by sandy topsoil and sandy clays that fill the bench step formation. In the test locations, the depth to rock ranged from the surface to ~1.3m below. The sandstone underlying the property is estimated to be Medium Strength or better. See Type Section attached for a diagrammatical representation of the expected ground materials.



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6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and

through the cracks in the rock.

Due to the slope and elevation of the block, the water table in the location is expected to be

many metres below the proposed works.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. It is

expected that normal sheet wash will move onto the site from above the property during

heavy down pours.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed above, below or beside the property. The proposed

excavation is a potential hazard until retaining structures are in place (Hazard One). The

vibrations from the proposed excavation are a potential hazard (Hazard Two).

RISK ANALYSIS SUMMARY ON NEXT PAGE



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Geotechnical Hazards and Risk Analysis - Risk Analysis Summary

HAZARDS	Hazard One	Hazard Two	
TYPE	The proposed excavation for the pool collapsing onto the worksite before retaining structures are in place.	The vibrations produced during the proposed excavation for the pool impacting on the surrounding structures.	
LIKELIHOOD	'Possible' (10 ⁻³)	'Possible' (10 ⁻³)	
CONSEQUENCES TO PROPERTY	'Medium' (15%)	'Medium' (15%)	
RISK TO PROPERTY	'Moderate' (2 x 10 ⁻⁴)	'Moderate' (2 x 10⁻⁴)	
RISK TO LIFE	8.3 x 10 ⁻⁶ /annum	5.3 x 10 ⁻⁷ /annum	
COMMENTS	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk to 'ACCEPTABLE' levels, the recommendations in Section 13 are to be followed.	This level of risk to property is 'UNACCEPTABLE'. To move risk to 'ACCEPTABLE' levels the recommendations in Sections 11 & 12 are to be followed.	

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.

10. Stormwater

The fall is to Lumeah Avenue. All stormwater from the proposed development is to be piped to the street drainage system through any tanks that may be required by the regulating authorities.



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11. Excavations

An excavation to a maximum depth of ~2m will be required to install the proposed pool. The

excavation is expected to be through topsoil and sandy clay, with Medium Strength Sandstone

expected at depths from between ~1.2m to ~1.3m below the current surface.

It is envisaged that excavations through soil and clay can be carried out with a machine and

bucket and excavations through Medium Strength Sandstone or better will require grinding

or rock sawing and breaking.

12. Vibrations

Possible vibrations generated during excavations through soil and clay will be below the

threshold limit for building damage.

Excavations through Medium Strength Rock or better should be carried out to minimise the

potential to cause vibration damage to the N neighbouring house. The excavation for the pool

is set back ~2.5m from the N neighbouring house. Close controls by the contractor over rock

excavation are recommended so excessive vibrations are not generated.

Excavation methods are to be used that limit peak particle velocity to 10mm/sec at the

property boundaries. Vibration monitoring will be required to verify this is achieved.

If a milling head is used to grind the rock, vibration monitoring will not be required.

Alternatively, if rock sawing is carried out around the perimeter of the excavation boundaries

in not less than 1.0m lifts, a rock hammer up to 300kg could be used to break the rock without

vibration monitoring. Peak particle velocity will be less than 10mm/sec at the property

boundaries using this method provided the saw cuts are kept well below the rock to broken.

It is worth noting that vibrations that are below thresholds for building damage may be felt

by the occupants of the neighbouring properties.



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13. Excavations Support Requirements

An excavation to maximum depth of ~2m will be required to install the proposed pool. Given

the depth to rock shown by the test results, the excavation is set back sufficiently from the

surrounding structures and boundaries.

The cut batters through soil and clay will stand at near-vertical angles for a short period of

time until the pool structure is installed, provided the cut batters are kept from becoming

saturated. Medium Strength Sandstone or better will stand at vertical angles unsupported

subject to approval by the geotechnical consultant.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion

works. All unsupported cut batters through soil and clay are to be covered to prevent access

of water in wet weather and loss of moisture in dry weather. The materials and labour to

construct the pool structure are to be organised so on completion of the excavation they can

be constructed as soon as possible. The excavation is to be carried out during a dry period.

No excavations are to commence if heavy or prolonged rainfall is forecast. If the cut batters

remain unsupported for more than a few days before the commencement of pool

construction they are to be temporarily supported with typical pool shoring such as form ply

or similar until the pool structure is in place.

All excavation spoil is to be removed from site or be supported by engineered retaining walls.

14. Retaining Structures

For cantilever or singly propped retaining structures it is suggested the design be based on a

triangular distribution of lateral pressures using the parameters shown in Table 1.

TABLE 1 ON NEXT PAGE



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Table 1 – Likely Earth Pressures for Retaining Structures

	Earth Pressure Coefficients			
Unit	Unit weight (kN/m³)	'Active' Ka	'At Rest' K₀	
Topsoil	20	0.40	0.55	
Residual Clays	20	0.35	0.45	
Medium Strength Sandstone	24	0.00	0.01	

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure, do not account for any surcharge loads and assume retaining structures are fully drained.

Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining structures are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e. Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining structures the full hydrostatic pressures are to be accounted for in the retaining structure design.

15. Foundations

The proposed pool is expected to be seated in Medium Strength Sandstone. This is a suitable bearing material. Any new foundations for the proposed house is to be supported on spread footings or piers taken to Medium Strength Sandstone. A maximum allowable bearing pressure of 1000kPa can be assumed for footings on Medium Strength Sandstone.



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The foundations of the existing garage are currently unknown (but are expected to be

supported on Medium Strength Sandstone). Ideally, footings should be founded on the same

footing material across the structure. Where the footing material does change across the

structure construction joints or similar are to be installed to prevent differential settlement,

where the structure cannot tolerate such movement.

Naturally occurring vertical cracks (known as joints) commonly occur in sandstone. These are

generally filled with soil and are the natural seepage paths through the rock. They can extend

to depths of several metres and are usually relatively narrow but can range between 0.1 to

0.8m wide. If a footing falls over a joint in the rock, the construction process is simplified if

with the approval of the structural engineer the joint can be spanned or alternatively the

footing can be repositioned so it does not fall over the joint.

NOTE: If the contractor is unsure of the footing material required it is more cost effective to

get the geotechnical professional on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over excavation in clay like

shaly rock but can be valuable in all types of geology.

16. Inspections

The client and builder are to familiarise themselves with the following required inspection as

well as council geotechnical policy. We cannot provide geotechnical certification for the

Occupation Certificate if the following inspection has not been carried out during the

construction process.

• All footings are to be inspected and approved by the geotechnical consultant while

the excavation equipment is still onsite and before steel reinforcing is placed or

concrete is poured.



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White Geotechnical Group Pty Ltd.

Ben White M.Sc. Geol., AusIMM., CP GEOL.

Bulut

No. 222757

Engineering Geologist.



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Photo 1



Photo 2



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Photo 3



Photo 4



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Photo 5



Photo 6



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Photo 7: AH1 – Downhole is from top to bottom.



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Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

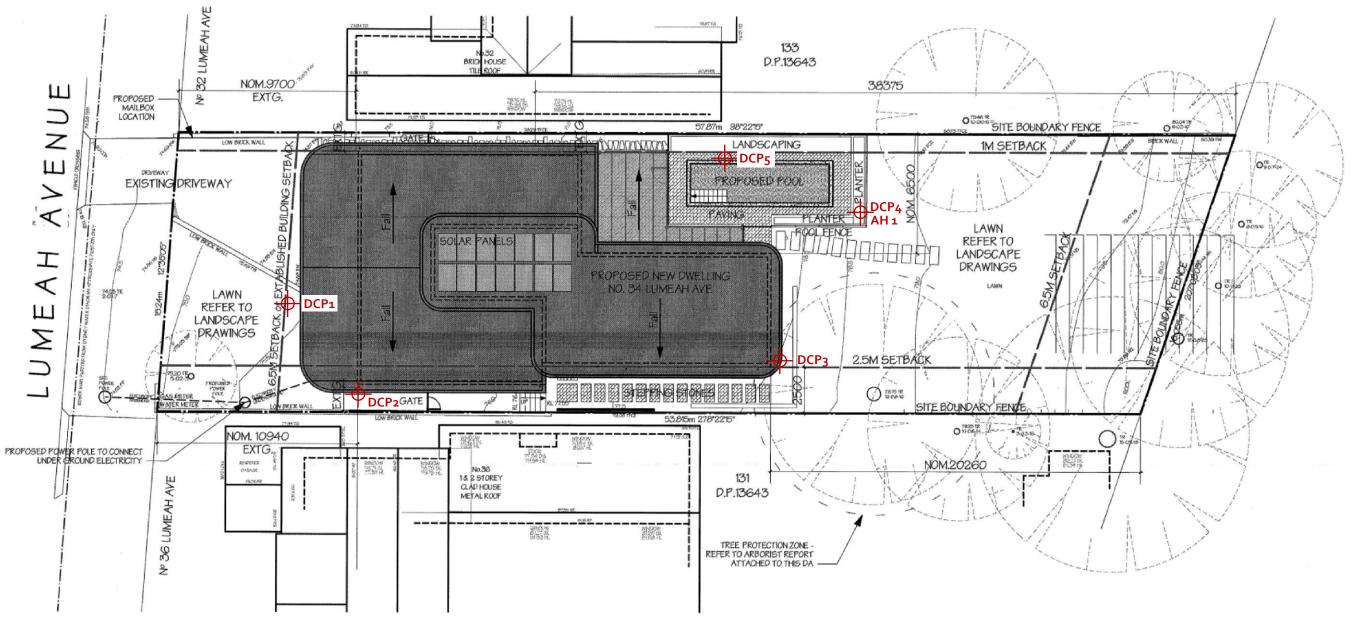
With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove
 different from those described in this report, it is advisable to contact White Geotechnical Group
 immediately, as problems relating to the ground works phase of construction are far easier and
 less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes
 to suit the previous experience of the contractors involved). If alternative design and construction
 processes are required to those described in this report, contact White Geotechnical Group. We
 are familiar with a variety of techniques to reduce risk and can advise if your proposed methods
 are suitable for the site conditions.

SITE PLAN – showing test locations

GENERAL NOTES

- BUILDING TO INCORPORATE BASIX COMMITMENTS TO COMPLY WITH THE ATTACHED BASIX CERTIFICATE NUMBER: 1163084S DATED 23 FEBRUARY 2021
- SMOKE ALARMS TO BE INSTALLED IN ACCORDANCE WITH AS 3786-2014 'SMOKE ALARMS' AND PART 3.72 'SMOKE ALARMS' OF THE BCA (NB. SMOKE ALARMS TO BE INTERCONNECTED WHERE THERE IS MORE THAN ONE ALARM
- TERMITE MANAGEMENT TO COMPLY WITH AS3660-2014 TERMITE MANAGEMENT NEW BUILDING WORK'
- GLAZING TO COMPLY WITH AS1288-2006 'GLASS IN BUILDINGS SELECTION AND INSTALLATION' AND AS 2047-1999 'WINDOWS IN BUILDINGS SELECTION AND INSTALLATION'
- WATERPROOFING OF WET AREAS TO COMPLY WITH AS3740 WATERPROOFING OF WET AREAS IN RESIDENTIAL BUILDINGS'. NO AIR DRIED LIQUID APPLIED TO MEMBRANES SHALL BE USED.
- ALL HOT WATER PIPES SHOULD BE INSULATED AS PER AS3500.4:2018
 ALL REQUIRED FACILITIES FOR A CLASS 1 BUILDING TO BE INSTALLED AS REQUIRED BY PART 3.8.2.2 'REQUIRED FACILITIES' OF THE BCA
- DOORS TO FULLY ENCLOSED SANITARY COMPARTMENTS TO COMPLY WITH PART 3.8.3 'FACILITIES' OF THE BCA
- STAIR CONSTRUCTION TO COMPLY WITH PART 3.9.1 'STAIR CONSTRUCTION OF THE BCA (NB. ALL STAIR TREADS TO HAVE A SURFACE THAT IS SLIP RESISTANT IN ACCORDANCE WITH PART 3.9.1.3
- BALUSTRADES CONSTRUCTION TO COMPLY WITH PART 3.9.2.3 'BALUSTRADES' OF THE BCA
- ALL NEW OPENABLE WINDOWS WITHIN A BEDROOM WITH A FLOOR LEVEL 2M OR MORE ABOVE A SURFACE BENEATH TO BE PROTECTED IN ACCORDANCE WITH PART 3.9.2.5 OF THE BCA
- DAMP PROOF MEMBRANE MUST BE HIGH IMPACT, O.2mm THICK POLYETHYLENE FILM
- ALL BUILDING WORK TO BE LOCATED WHOLLY WITHIN THE ALLOTMENT BOUNDARIES

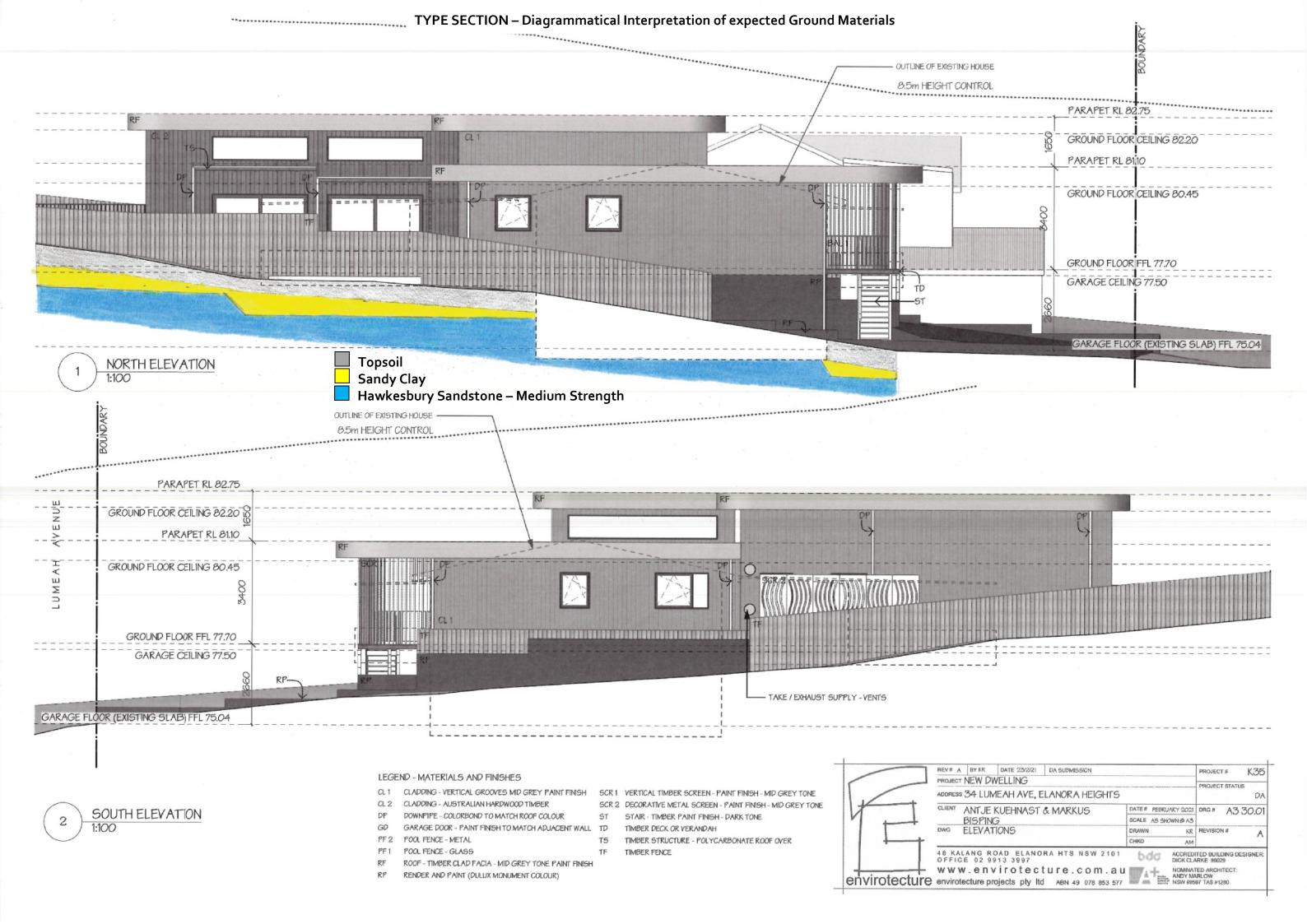


SITE PLAN 1:200

DRAWING NOTES:

- REFER TO ROOF PLAN ON "A3 21.03" FOR FURTHER DETAIL AND INFORMATION
- REFER TO ATTACHED LANDSCAPE PLAN FOR FURTHER DETAILS ON LANDSCAPING
- REFER TO STORMWATER PLANS PROVIDED WITH THIS APPLICATION FOR FURTHER INFORMATION ON STORMWATER INFRASTRUCTURE





EXAMPLES OF GOOD HILLSIDE PRACTICE



EXAMPLES OF POOR HILLSIDE PRACTICE

