| From: | Talofa Pouli |
|--------------|---|
| Sent: | 13/03/2025 2:15:45 PM |
| То: | Council Northernbeaches Mailbox |
| Cc: | Justine Walter |
| Subject: | TRIMMED: DA2025/0132 - Submission on behalf of Owners of Strata Plan 83233, 41 Roseberry Street and 76-80 Kenneth Road Manly Vale (ABN 28727137237) |
| Attachments: | DA2025:0132 - Submission on behalf of Owners of Strata Plan 83233.pdf; |

Dear General Manager Northern Beaches Council

On behalf of the above Owners Corporation – SP83233, we have been instructed to send you the attached (also in below link) submission of objection to the proposed McDonald's as per subject item.

Thank you for your attention to this matter.

Kind Regards

Talofa Pouli Strata Manager



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| _ | | |

13 March 2025 Ref: 25683



General Manager Northern Beaches Council PO Box 82 MANLY NSW 1655

Att: Claire Ryan

Dear Claire,

Submission – DA2025/0132, Proposed McDonalds, 37 Roseberry Street, Balgowlah

We write on behalf of the owners of Strata Plan (SP) 83233, 41 Roseberry Street and 76-80 Kenneth Road Manly Vale (ABN 28727137237). The SP comprises a large three storey residential flat building comprising 45 dwellings. The location of the site and the proximity of the site of the proposed McDonalds' fast food restaurant is illustrated in **Figure 1** on the following page. SP 83233 directly adjoins the land that is subject to the proposed development application No. 2025/0132.

You will note from the image in **Figure 2** below that bedrooms, balconies and living areas face and directly overlook the site and are separated from the site by approximately 23 metres. SP 83233's building carpark exits onto Kenneth Road and must use the Roseberry Street roundabout to access Condamine Street. McDonalds patrons will also be required to use the Roseberry Street roundabout to access Condamine Street

Therefore, the owners of SP 83233 have a direct interest in the outcomes for the land subject to the DA.

Firstly, I must raise the difficulty we had in gaining a full appreciation of the proposed development. The architectural, landscape and, we assume, the lighting plans cannot be accessed on-line as at Friday 7th March. The on line material advises any party that wishes to view the plans to make arrangements to inspect the plans in person during Council's office hours. However, notwithstanding this constraint we have relied on copies of the plans included in other consultant reports to gain an understanding of the development. I will return to this concern later.

Secondly, by making this submission, I confirm that neither I, nor any associate within the period commencing 2 years before the date of this submission, has made any:

- reportable political donations to any local councillor of the Northern Beaches Council
- (b) gifts to any local councillor or employee of the Northern Beaches Council.

In summary, we have reviewed the material on exhibition and write to advise that we object to the proposed development.

The grounds of the objection are listed below with accompanying detail.





>Figure 1: Location of SP 83233 (indicated with red boundary) and the Site of the Proposed Development (indicated with yellow boundary) (Source of Aerial: NSWSIx.Mapping).



>Figure 2: View Showing Balconies and Living Space in SP 83233 Overlooking Site (Source: SP83233).



1. The development application is incomplete, and Council cannot be satisfied that an adequate environmental assessment has been undertaken as required by S.4.15 of the Environmental Planning and Assessment Act 1979.

We note the that:

- a) Section 4.15 of the EP&A Act requires evaluation by Council of 'the likely impacts of that development, including environmental impacts on both the natural and built environments, and social and economic impacts in the locality'.
- b) By virtue of Part 3 Division 1 Clause 24 of the Environmental planning and assessment regulation 2021, a development application is required 'to contain all the information and documents required by— ... (ii) the Act or this Regulation.'
- c) The development application does not satisfy this requirement.
- d) Nowhere in the development application, and specifically in no part of the Statement of Environmental Effects, is the presence of the residential flat building owned by the owners of SP 83233 acknowledged beyond one line on Page 5. Page 5 defers detail to the survey plan that accompanies the development application. However, the survey also ignores the presence of SP 83233. It is not identified in the site analysis.
- e) In only one place in the Statement of Environmental Effects are the impacts of the proposed development upon SP 83233 raised. This takes place in Part 6 on P.23 with regard to noise. However, the assessment is cursory at best and casually dismissed with a simple comment the locality already has a high ambient noise level, and all noise will meet appropriate standards. We will return to noise impact below.
- f) The Statement of Environmental Effects only selectively evaluates the proposed development against the objectives of the E3 'Productivity Zone. It ignores, and fails to evaluate the proposal against, the amenity objectives of the zone. This is deficient and inadequate for Council, or any other party', to gain an appreciation of the proposed development. I will return to this concern below.
- g) No assessment of lighting and luminance impact is undertaken with the exception of a simple comment that it, in effect, 'will comply with the relevant AS'. We will return to lighting impact below.
- h) Nowhere in the development application, and specifically in no part of the Statement of Environmental Effects are the findings of the Traffic Report (Colston Budd, Rogers and Kafes, December 2024) raised or discussed. We will return to traffic impact below.
- The requirement in the EPA Act and the EPA Reg that an adequate and thorough development application be made is a jurisdictional precondition that needs to be satisfied in order for Council (or the Panel) to be able to exercise the function of determining the development application.

2. The proposed development is inconsistent with the Objectives of the 'E3 Productivity Support' zone.

a) The relevant amenity objectives of E3 zone in the Manly LEP 2013 are:

To create employment environments of high visual quality that relate favourably in architectural and landscape treatment to neighbouring land uses and to the natural environment.

To minimise conflict between land uses in the zone and adjoining zones and ensure the amenity of adjoining and nearby residential land uses.

- b) As we note above, the evaluation contained in the development application does not acknowledge the presence of the land owned by SP 83233 and does not acknowledge the presence of the higher density residential environment located in the adjoining R3 Medium Density Zone within which that land is located, notwithstanding the inclusion in the Statement of Environmental Effects of an extract of the zoning map on Page 15.
- c) Furthermore, nowhere in the development application, and specifically in no part of the Statement of Environmental Effects is the proposed development evaluated against the amenity objectives above beyond one line on Page 16 that simply states "[it is] compatible with the objectives of the zone."
- Objective Assessment The evaluation in the development application provides no assessment of the To create emplovment architectural quality of the proposed development and its relationship with neighbouring land uses or the natural environment beyond the statement "The environments of building is of a simple, modern design, with colours and finishes to be consistent high visual quality that McDonald's corporate theme (p.8)." relate favourably in architectural However, we note that: and landscape (i) The architectural design of the building presents a homogeneous highway treatment to oriented drive through fast food business dominated by surface car parking to neighbouring all boundaries, prominent advertising signage, long twin drive-thru lanes and land uses and to excessive building setbacks. the natural environment. (ii) Due to the hidden and obscure location of the site, and the inherent difficulty in advertising its presence to passing traffic, the development seeks to address this with prominent signage addressing Condamine Street and site planning and building character more suited to a main road location. (iii) The design fails to acknowledge or accommodate the adjoining residential character directly adjoining the site. (iv) The large expanse of car parking proposed to all boundaries, the dominance of the drive-thru lanes in the streetscape, large prominent signage and the excessive building setbacks are incongruous and inappropriate for this transition area between the E3 and R3 zone. To minimise The assessment of the proposed development in this submission recognises that conflict between there are a number of conflicts with adjoining and nearby residential uses as land uses in the follows: zone and Acoustic impacts have not been adequately evaluated, and it is evident (i) adjoining zones that such impacts will be unreasonable; and ensure the amenity of Traffic impacts have not been adequately evaluated, and it is evident that (ii) adjoining and such impacts will be unreasonable; nearby (iii) Odour impacts have not been adequately evaluated, and it is evident that residential land such impacts will be unreasonable; and uses. (iv) The building style, site planning and built form character are inconsistent with the desired character sought for the area.
- d) From our review, the proposed development fails to achieve the amenity objectives of the zone for the reasons stated below.



3. The site of the proposed development is a residential transition zone, rather than a highway oriented site, and thus the proposed development is inappropriate located.

We note the that:

- a) The site is hidden and obscured from passing traffic on Condamine Street by the presence of a three storey bulky goods (large format retail) showroom, for which the building car parking, siting and signage is designed. Of note, this development also includes a residential use directly adjoining the site.
- b) The site is located in a part residential area distant from, and not suitable for highway oriented commercial services and uses.
- c) Specifically, the prevailing character of the site is that of a transition area between the E3 zone and the R3 zone to the south.
- d) The proposed development generates unreasonable impacts on the amenity and desired character for the area as described elsewhere in this submission.
- e) Therefore, the proposed development is inappropriately located. A site directly addressing Condamine Street or similar sub-arterial road is a more suitable location. The presence of a similar KFC fast food drive thru fast food restaurant directly addressing Condamine Street located less than 70 metres from the proposed site provides a good example of a more suitable location for such a use.
- 4. No evidence has been provided to confirm that the proposed development will not have unreasonable lighting impact on the adjoining residential use in land owned by SP 83233 and the amenity of the area.

We note the that:

- a) The proposed drive thru- fast food restaurant seeks to operate 24 hours, 7 days a week.
- b) No external lighting impact report has been prepared in support of the Development Application.
- c) The submission of such a report to support a proposal of this nature is common. The purpose of the report would be to review the proposed development and to provide concept external lighting recommendations to ensure a compliant lighting design is developed. It should ensure that lighting design reduces and controls potential spill of obtrusive light onto neighbouring properties, and particularly into windows of bedrooms and other habitable rooms at nighttime.



5. No evidence has been provided to confirm that the proposed development will not have unreasonable acoustic impacts on the adjoining residential use in land owned by SP 83233 and the amenity of the area.

We note the that:

- a) The proposed drive thru fast food restaurant seeks to operate 24 hours, 7 days a week.
- b) While the Acoustic report acknowledges the presence of noise receivers in SP 83233, the assessment only addresses construction, operational noise and waste collection. It fails to assess the following potential noise impacts of night time users of the car park: vehicle noise (engine revving, tyre screeching); amplified music; customer congregation and anti-social behaviour (often induced by excessive alcohol or drug consumption). These noise generating activities are often associated with the operation of a 24 hour drive thru fast food restaurant.
- c) The assessment merely states in one sentence: "sleep disturbance is not anticipated, as emissions from maximum noise events (i.e. door slams and patrons shouting) are predicted to satisfy the NPIs maximum noise trigger levels for the night period" (p.35).
- d) This is inadequate. Residents in SP83233 have confirmed that the existing uses in the site are unobtrusive in terms of noise outside business hours and the area in general enjoys a quite ambience at night. The acoustic assessment is deficient and the concerns regarding noise impact of the proposed development by the residents and owners in SP 83233 are reasonable and appropriate.

6. No evidence has been provided to confirm that the proposed development will not have unreasonable odour impacts on the adjoining residential use in land owned by SP 83233 and the amenity of the area.

We note the that:

- a) The Odour Assessment report acknowledges in Part 6 that the clustering of the kitchen exhaust fans when combined will exceed the combined flow threshold rate required by the relevant Australian Standard and are 'deemed objectionable' (p.17). The report also acknowledges in Part 7 that '*The ventilation design has not yet been finalised for the Project, and thus it is not possible to provide precise details of the discharge velocities or stack heights. McDonald's has extensive experience in managing and mitigating against adverse odour impacts from their operations (p.21)'.*
- b) Thus, the report is incomplete and deficient, and it makes the extraordinary claim that, in the face of these inadequacies and the lack of ability for Council and local residents to understand and assess odour impact that all parties should essentially 'trust McDonalds to do a good job.'
- c) This is clearly inadequate. The odour assessment is deficient and the concerns regarding odour impact of the proposed development by the residents and owners in SP 83233 are reasonable and appropriate.



7. No evidence has been provided to confirm that the proposed development will not generate unreasonable crime and safety impacts on the adjoining residential use in land owned by SP 83233 and the amenity of the area.

We note the that:

- a) Two relevant documents are provided with the development application: a ''Crime Risk Assessment' SLR, 16 December 2024 and a 'Plan of Management' 5th December 2024.
- b) The Crime Risk Assessment is a generic document that fails to consider the site specific circumstances, locality context and characteristics of the proposed development. No site plan or site and locality assessment is undertaken. In fact, the header to the document refers to another site entirely: 90-98 Glenmore Ridge Drive, Glenmore Park.
- c) Similarly, the Plan of Management is also a generic document. It fails to consider the site specific circumstances, locality context and characteristics of the proposed development. No site plan or site and locality assessment is undertaken.
- d) Neither document addresses the proximity of a residential flat building with balconies and windows of habitable rooms overlooking the drivethru lanes and carpark of the proposed development.
- e) Neither document provides actions, strategies and responses to address potential antisocial behaviour that may be generated by users of the car park of the proposed 24 hour operation of the premises.
- f) This is particularly relevant as there are valid concerns by residents adjoining the site of the proposed development with anti-social behaviour gained from experience at other McDonalds fast food restaurant in the Northern Baches Area. Dee Why police are on the public record that certain McDonalds fast food restaurants create a notable increase in incidents of crime. The link below to a news article provides evidence of this. <u>https://www.northernbeachesadvocate.com.au/2024/10/07/mayhem-atbrookie-maccas/.</u>
- g) This situation is clearly unacceptable. The crime risk assessment and plan of management are deficient and the concerns regarding crime and safety impacts of the proposed development by the residents and owners in SP 83233 are reasonable and appropriate.
- 8. No evidence has been provided to confirm that the proposed development will not generate unreasonable traffic impacts on the adjoining residential use in land owned by SP 83233 and the amenity of the area.

We note the that:

- a) The traffic impact assessment concludes that the road network will be able to cater for the traffic generation of the proposed development.
- b) We find that conclusion incongruous and inconsistent with the conclusions of the SIDRA traffic modelling that finds that the level of service of Kenneth Street at certain times is often 'D' and 'F.' Level of service 'F' is the most unacceptable and is defined as 'unsatisfactory and requires additional capacity.'



- c) Of particular importance, SP83233 commissioned McLaren Traffic Engineering to review the Traffic Impact Assessment. This is attached in Appendix A at the rear of this advice. It's review found a number of errors in the assessment, and it concludes "The lodged CBRK report contains an incorrect traffic generation assessment. The key points in this regard are listed on page 2 of this letter, under Section 1 items (a) to (e), inclusive" (p.5). For the sake of brevity, the errors in the report are not reproduced here and the McLaren Report in Appendix A should be consulted for detail.
- d) The traffic impact assessment has been found to be inadequate and deficient by McLaren Traffic Engineering. It also contains a number of errors. Thus, the concerns regarding traffic impacts of the proposed development by the residents and owners in SP 83233 are well founded and appropriate.

9. Insufficient information has been provided to enable a sufficient and appropriate level of assessment of the impacts of the proposed development.

- a) We note in our objections above the failure of the development application to address the requirements of Section 4.15 of the EP&A Act and the Regulations. We also note the numerous deficiencies and gaps in the assessment reports provided with the development application. These deficiencies prevent Council from undertaking a proper assessment of the proposed development and satisfying itself that the proposed development will not have unreasonable impacts.
- b) Furthermore, the exhibition of the development application is flawed. The online material fails to include copies of the architectural and landscape plans to enable thorough assessment.
- c) In particular a one page statement on line refers viewers to contact Council and manually inspect the plans in Council's offices.
- d) The development application should be rewritten and reexhibited with a thorough suite of documents that addresses the requirements of the Act, contain no gaps and do not require viewers to attend Council offices to view plans.

9. Approval would not be in the Public Interest.

a) We note the large number of objections that have been received regarding the proposed development (and have been advised it now amounts to 450 objections and a 3,000 signature petition). Suffice to say that approval of the proposed development in the face of such a large number of objections would be contrary to the public interest as required by the evaluation criteria in Cause 4.15(1e) of the EP&Act and the objects of the Act in Part 1 Clause 1.3.



We trust this information is sufficient for your purposes. I look forward to hearing from you, and should you also require any further details or clarification, please do not hesitate to contact me.

Yours sincerely, INSPIRE URBAN DESIGN + PLANNING PTY LTD

Stephen McMahon Director



APPENDIX A

Review of DA Traffic Impact Assessment, McLaren Traffic Engineering



13 March 2025

Reference: 250154.01FB

General Manager Northern Beaches Council C/o The Owners - Strata Plan No. 83233

SUBMISSION OF OBJECTION – DA2025/0132, PROPOSED M^cDONALDS, 37 ROSEBERRY STREET, BALGOWLAH

Dear The Owners – Strata Plan No. 83233,

M^cLaren Traffic Engineering (**MTE**) has been engaged by The Owners of Strata Plan No. 83233, 41 Roseberry Street & Kenneth Road, Manly Vale (ABN 28728137237) to review the above-described proposal and to make submissions on its behalf.

lssues

The following issues have been identified following a review of the *Traffic Report for Proposed McDonald's, 37 Roseberry Street, Balgowlah*, prepared by *Colston Budd Rogers & Kafes Pty Ltd* (**CBRK**) dated December 2024 lodged as part of the Applicant's development application:

- 1. Inadequate External Traffic Impact Assessment with regard to Average Vehicle Delay experienced, Average Vehicle Queue Lengths and 95th Percentile Vehicle Queue Lengths for the Critical Condamine Street / Kenneth Road Traffic Signal Controlled Intersection.
- 2. Incorrect Traffic Generation Assessment
- 3. Lack of Any Sensitivity Testing on Traffic Assignment Changes
- 4. Loss of On-Street Parking

The first issue outlined above is presented in detail in the attached recent traffic counts (Friday 28 February 2025 [2.00pm to 7.00pm], Saturday 29 February 2025 [9.00am to 2.00pm] and Wednesday 5 March 2025 [6.00am to 10.00am plus 2.00pm to 6.00pm]) and associated SIDRA analysis for the EXISTING conditions in **Technical Memo 1** (96 pages) and FUTURE conditions with the impacts of the proposed McDonald's outlet in **Technical Memo 2** (14 pages).



1. Summary of Issue 1 From Technical Memos 1 & 2

The lodged **CBRK** report contains inadequate external traffic impact assessment with regard to Average Vehicle Delay (AVD) experienced, Average Vehicle Queue Lengths and 95th Percentile Vehicle Queue Lengths for the critical Condamine Street / Kenneth Road Traffic Signal Controlled Intersection. The key points in this regard are as follows:

- a) The estimated traffic generation is based on '*Trip Generation and Parking Demand Surveys* of *Fast Food Outlets Analysis Report*' created by *Bitzios Consulting 2016*. The estimated traffic generation is in the order of **140** vehicles during the afternoon peak hour, and **180** vehicles during the Saturday midday peak hour.
- b) More recent documents, specifically the *TfNSW Guide to Transport Impact Assessment*, suggests that during the weekend site peak hour, McDonald's generates **267** vehicle trips which is an increase of **87** vehicle trips from the **CBRK** report.

| Table 5.46. Fast food sample summary – McDonalds | | | | | | | |
|--|-----------------------|----------|----------|--|--|--|--|
| | Sydney | Regional | Combined | | | | |
| Weekday Vehicle trips | (vehicle trips/outlet |) | | | | | |
| Site AM Peak hour | 137 | 206 | 192 | | | | |
| Network AM Peak | 119 | 188 | 173 | | | | |
| Site PM Peak hour | 188 | 201 | 214 | | | | |
| Network PM Peak | 138 | 183 | 179 | | | | |
| Daily | 1,032 | 1,261 | 1,272 | | | | |
| Weekend Vehicle trips (vehicle trips/outlet) | | | | | | | |
| Site Peak hour | 267 | 225 | 269 | | | | |
| Daily | 1,209 | 1,164 | 1,303 | | | | |

c) The transitional period of the *TfNSW Guide Transport Impact Assessment* ended 4 November 2024 and therefore applies to this traffic report.

Transitional Arrangements:

This Guide does not apply to TIAs commenced and development applications lodged before 4 November 2024.

- d) It is noted that due the eastern approach to Condamine Street / Kenneth Road performing at an LoS "F", any minor increases in traffic volumes are expected to further significantly degrade the performance of this approach.
- e) It is acknowledged that 50% of the traffic to the proposed development can be considered passing trade. In any case, it is expected that the proposed McDonald's will generate destination vehicle trips which will utilise the existing road network. Approximately 44 additional trips are generated during the weekend peak hour period which should be taken into consideration.



Existing Conditions

 a) A comparison between the existing intersection performance of the eastern approach of Condamine Street / Kenneth Road between the CBRK assessment and MTE assessment is provided in Table 1.

TABLE 1: EASTERN APPROACH – LEVEL OF SERVICE MOVEMENT COMPARISON – EXISTING SCENARIO

| Turning Movement | Level of Service | | | | | | |
|---------------------|------------------|------|----------|---|--|--|--|
| | Wee | kday | Weekend | | | | |
| Wovement | CBRK | MTE | CBRK MTE | | | | |
| RT | F | F | F | F | | | |
| Т | С | F | С | F | | | |
| LT | В | D | В | D | | | |

- b) As shown, it is likely that the CBRK model overestimated the efficiency of the signalised intersection due to utilising the optimal cycle time setting which does not reflect the performance of the intersection under existing operation.
- c) A comparison of the LoS of the movements associated with the eastern approach to the signals indicates that the eastern approach exceeds capacity for the RT and T movements and is at capacity for the LT movement. It is noted that based on video footage observations, the right turn queues regularly block the ability for T and LT traffic to exit the approach.
- d) In any case, both models agree that the RT operates with an LoS "F". A LoS "F" performance is indicative of traffic which exceeds the available lane capacity resulting in queueing and excessive delays.

Future Conditions

- a) By comparing the existing performance of the intersections provided in "Memo 1", it is evident that the overall performance of the signalised intersection of Condamine Street / Kenneth Road remains at a LoS "D". Although the overall performance remains the same, the traffic throughput of the eastern approach already exceeds capacity (LoS "F"), and any additional vehicle trips will adversely impact queues and delays. This is evident as the roundabout intersection of Kenneth Road / Roseberry Street quickly degrades, specifically during the Saturday period.
- b) The roundabout of Kenneth Road / Roseberry Street degrades from a Level of Service "B" to "C" during the Saturday period, with degree of saturation exceeding 1.0 and the average delay increasing from 15.7 seconds to 37.6 seconds. The subject development adversely impacts the roundabout performance.
- c) The performance of the eastern approach of Condamine Street / Kenneth Road is summarised in Table 2.



TABLE 2: EASTERN LEG – LEVEL OF SERVICE MOVEMENT COMPARISON – POST DEVELOPMENT

| Turning Movement | Level of Service | | | | | | |
|---------------------|------------------|------|---------|-----|--|--|--|
| | Wee | kday | Weekend | | | | |
| | CBRK | MTE | CBRK | MTE | | | |
| RT | F | F | F | F | | | |
| Т | С | F | С | F | | | |
| LT | В | D | В | D | | | |

d) Persons trip generation rates are not available for McDonald's fast-food outlets, however it is reasonable to assume that a McDonald's would generate additional pedestrian foot traffic from the surrounding area. Although pedestrian crossing facilities are provided at roundabouts, it is not particularly safe as pedestrians strictly do not have right of way at roundabouts. In practice, vehicles tend to stop to allow pedestrians to cross at roundabout which would result in additional delays.

Eastern Approach of Condamine Street / Kenneth Road – Detailed Review

- d) To assess the eastern approach of Condamine Street / Kenneth Road in further detail, the following parameters were extracted from the **CBRK** and **MTE** SIDRA outputs:
- Degree of Saturation;
- Average Delay;
- Average Queue Length;
- 95th Percentile Queue Length (the SIDRA INTERSECTION 9.1 results for 95th percentile queue is presented in **Annexure B**).

The CBRK and MTE performance are summarised in Table 3 and Table 4 respectively.

| MODEL) | | | | | | | | | |
|-----------------------------|---------------------|---------------|---------------|-----------------------------|--|--|--|--|--|
| Peak Period | Degree of | | Average Queue | 95 th Percentile | | | | | |
| reak renou | Saturation | Average Delay | Length | Queue | | | | | |
| | Existing Conditions | | | | | | | | |
| Weekday | 1.011 | 56.7 seconds | 84.3m | (1) | | | | | |
| Saturday | 0.99 | 55.8 seconds | 90.0m | (1) | | | | | |
| Post Development Conditions | | | | | | | | | |
| Friday | 0.99 | 51.9 seconds | 80.6m | (1) | | | | | |
| Saturday | 1.01 | 54.3 seconds | 90.0m | (1) | | | | | |

TABLE 3: EASTERN APPROACH – SPECIFIC SIDRA OUTPUT PARAMETERS (CBRK MODEL)

NOTE:

(1) Cannot be determined from CBRK Report.

TABLE 4: EASTERN APPROACH - SPECIFIC SIDRA OUTPUT PARAMETERS (MTE MODEL)

| Peak Period | Degree of Saturation | Average Delay | Average Queue Length | 95 th Percentile Queue | | | |
|---------------------|-------------------------|---------------|-------------------------|--------------------------------------|--|--|--|
| Existing Conditions | | | | | | | |
| Friday | 0.996 | 75.5 seconds | 81.4m | 132.9m | | | |



| Saturday | 0.940 | 72.4 seconds | 75.6m | 123.4m | | | |
|--|-------|--------------|-------|--------|--|--|--|
| Post Development Conditions (Saturday Worst Case) | | | | | | | |
| Saturday 0.976 78.1 seconds 84.1m 137.2m | | | | | | | |

e) Based on the above, it is evident that the eastern approach is currently at maximum capacity with traffic generated by the proposed McDonalds adversely impacting the eastern approach.

Key Findings

The following findings and conclusions can be made upon assessment of the existing plus post development intersection conditions:

- A. The CBRK model overestimates the efficiency of the signalised intersection of Condamine Street / Kenneth Avenue by utilising the 'Network Optimum Cycle Time'. The model should utilise the existing phase durations to reflect existing conditions. As a result, the movements associated with the eastern approach perform with a lower level of service.
- B. The traffic generation rates contained within *TfNSW Guide to Transport Impact Assessment* apply. The intersections of Condamine Street / Kenneth Road and Kenneth Road / Roseberry Street are effectively at capacity. Any increases to traffic volumes will have significant impact to intersection performance.
- C. The performance of the eastern approach at Condamine Street / Kenneth Road is adversely impacted. Further, the additional traffic has flow on traffic impacts to the roundabout of Kenneth Road / Roseberry Street, with queues extending past the roundabout from the signalised intersection.
- D. Application of post-development traffic to the MTE model indicates that the performance of Kenneth Road / Roseberry Street is adversely impacted. The performance degrades from a LoS "B" to LoS "C" with a 20.9 second increase in average delay. The degree of saturation also exceeds 1.0 under post-development conditions.
- E. Any potential intersection or road upgrades should also consider the eastern approach of the signalised intersection of Condamine Street / Kenneth Road. It is evident that there is no capacity for right turns, resulting in lane blockages for the through and left-turn movements.

2. Incorrect Traffic Generation Assessment

The lodged **CBRK** report contains an incorrect traffic generation assessment. The key points in this regard are listed on page 2 of this letter, under Section 1 items (a) to (e), inclusive.

3. Lack of Any Sensitivity Testing on Traffic Assignment Changes

The lodged **CBRK** report does not include any sensitivity testing of changes in traffic assignment. To this end, the lodged **CBRK** report does not robustly justify at all the adopted traffic assignment, nor has any changes in traffic assignment, as stated in *Section 3.4.3 "Sensitivity Testing"* of the 4 November 2024 "Guide to Transport Impact Assessment" (NSW Government TfNSW). Section 3.4.3 states that "sensitivity testing is important to ensure that technical assumptions do not distort the findings" for Transport Impact Assessments (**TIA**'s).



This is a critically important issue and upon review of the lodged **CBRK** report, it is evident that the adopted and assessed "additional" traffic flows for the two key intersections of Kenneth Road with both Condamine Street and Roseberry Street are extremely confusing. No robust justification of the assignment of approaching and departing traffic has been included in the **CBRK** report at all.

This is a serious matter, and it appears as though traffic has been assigned to lessen the impacts on the critical movements at both intersections, particularly avoiding the impact on the Condamine Street intersection with Kenneth Road.

To this end, the disparity and illogical (or at least not robustly justified) traffic assignment adopted by **CBRK** report for both the Friday PM and Saturday noon peak periods is as follows:

> Arrival of traffic to the McDonald's driveway

- 40% from the south along Roseberry Street.
- 15% from the south via the right turn lane in Condamine Street.
- 25% from the east along Kenneth Road.
- 10% from the north along Roseberry Street.
- 10% from the north along Condamine Street.

> <u>Departure of traffic from the McDonald's driveway</u>

- 22% to the south along Roseberry Street.
- 15% to Condamine Street (south) via Kenneth Road.
- 31% to the east along Kenneth Road.
- 16% to the north along Roseberry Street.
- 16% to Condamine Street 9north) via Kenneth Road.

4. Loss of On-Street Parking

The road carriageway width of Roseberry Street fronting the proposed McDonalds Site is approximately 9 metres or less. This is a narrow width that cannot accommodate two kerbside (parallel) parking lanes with two-way traffic flow in between.

The **CBRK** report acknowledges on page 11 that vehicles currently queue back past the site from the roundabout.

It is important to note that Council "required" that a median be installed across the driveway in its response, as set out on page 17 & 18 of the **CBRK** report (as repeated below), to prohibit right turns entering and leaving the proposed driveway (30m offset from the Kenneth Road roundabout) and presumably to prohibit the loss of any kerbside parking along the eastern side of Roseberry Street, south of Kenneth Road:

"As traffic often queues along the full frontage of the site a median will be required on Roseberry Street across the proposed driveway to physically prevent right turns in and out of the driveway. This will ensure that vehicles attempting to turn right in and out will not be blocked by that queue and create queuing/congestion issues within and external to the site. This may need to be supported by a roundabout at the Roseberry Street/Hayes Street intersection to assist with access for vehicles blocked by the median." (The CBRK report identifies this as Option 1).



In regard to Option 1, the **CBRK** report states on page 12, that "To accommodate the median, parking on the eastern side of Roseberry Street opposite the site (4 spaces would be lost). This option was suggested by Council in the pre-DA advice;"

It is evident from the above (indented) extract of Council's "required" median works did not state that 4 spaces would be lost, which is otherwise suggested by **CBRK**'s sentence above. The **CBRK** report therefore misleads the reader to believe that Council agrees that 4 spaces would be lost, which is not evident from the extracts.

It should further be noted that the undersigned has been involved in other development applications whereby the provision of a median has either been reduced in width to retain kerbside parking or that the kerb and gutter along the site frontage has been relocated (with a localised reduced verge / nature strip width) in order to retain the prevailing kerbside parking.

With retained kerbside parking along the eastern side of Roseberry Street, south of Kenneth Road, right turning traffic entering the site driveway will not be possible across the queue of northbound traffic at peak times (as agreed by **CBRK**) and will create a worsening of traffic conditions with vehicle queues extending back to the Kenneth Road roundabout and effectively block the efficient operation of the roundabout leading to gridlock conditions at times.

This leads to a discussion on Option 2, as raised solely by **CBRK**, which involves the removal of *"parking on the eastern side of Roseberry Street opposite the site (4 spaces would be lost) and provide no queuing line marking on the northbound traffic lane in Roseberry Street across the McDonald's access. This would allow southbound vehicles on Roseberry Street to pass a vehicle turning right into the site."* Refer to page 12 of the **CBRK** report under the Option 2 description.

The **CBRK** report then provides a self-serving recommendation, without any detailed considerations of either a narrow median / narrow verge outcome or a small local road roundabout at the Roseberry Street / Hayes Street "T-junction", which many councils have installed in local streets over many years.

The **CBRK** report recommendation for Option 2 is repeated below for ease of reference:

- "Option 2 is the recommended option as:
- both options result in the loss of parking on the eastern side of Roseberry Street;
- there is insufficient area to accommodate a roundabout at the intersection of Hayes Street/Roseberry Street; and

• Option 2 provides direct right turn access to the site, whereas Option 1 would restrict access to the site from the north and result in additional travel time and distance for these vehicles to access the site."

CBRK's recommended loss of parking along the eastern side of Roseberry Street south of Kenneth Road constitutes a poor outcome for the localised mixed-use precinct that includes industrial, commercial, retail and high density residential land uses.

CBRK's recommended "no queuing line marking on the northbound traffic lane in Roseberry Street across the McDonald's access" is not supported by any detailed (to scale) plans of the proposed works.

The undersigned notes that the expressed words *"no queuing line marking on the northbound traffic lane"* indicates a poorly expressed treatment, which if corrected in traffic engineering terms, would mean "KEEP CLEAR" pavement marking across the northbound traffic lane in Roseberry Street across the proposed McDonald's driveway.



From the undersigned experience dealing with local councils and TfNSW, local traffic committees typically reject "KEEP CLEAR" pavement markings across private car parks and reserve them for public road junctions, hospitals, fire stations, bus only terminals and some public car parks.



5. <u>Concluding Statement</u>

In conclusion, the proposed development application should be refused for the following reasons:

- a) On the basis of our modelling, it is evident that the eastern approach (Kenneth Road) to the Condamine Street / Kenneth Road traffic signals is currently at maximum capacity with traffic generated by the proposed McDonalds adversely impacting the eastern approach
- b) The lodged **CBRK** report contains numerous insufficient, inadequate and unjustified matters as outlined in detail in this objection letter. A complete, thorough and comprehensive review of the vehicular access planning and development potential is required.
- c) The lodged CBRK report does not include any sensitivity testing of changes in traffic assignment. To this end, the lodged CBRK report does not robustly justify at all the adopted traffic assignment, nor has any changes in traffic assignment, as stated in Section 3.4.3 "Sensitivity Testing" of the 4 November 2024 "Guide to Transport Impact Assessment" (NSW Government TfNSW). Section 3.4.3 states that "sensitivity testing is important to ensure that technical assumptions do not distort the findings" for Transport Impact Assessments (TIA's).
- d) **CBRK**'s Option 2 assessment for vehicular access management at the proposed McDonald's driveway on Roseberry Street is largely self-serving in response to Council's "required" Option 1 traffic management treatment that includes a median across the McDonald's driveway, whilst presumably retaining the existing kerbside parking along the eastern side of Roseberry Street, south of Kenneth Road.
- e) **CBRK**'s response to Council's Option 1, specifically relating to the provision of a roundabout at Roseberry Street / Hayes Street "T-junction" is unprofessionally dismissive with no detailed consideration of small localised roundabouts that many local councils have installed in local streets over many years.
- f) From the undersigned experience dealing with local councils and TfNSW, local traffic committees typically reject "KEEP CLEAR" pavement markings across private car parks and reserve them for public road junctions, hospitals, fire stations, bus only terminals and some public car parks.
- g) In view of the foregoing, the proposed McDonald's outlet must be rejected based upon the inadequate external traffic impact assessment submitted by the applicant. Indeed, the Kenneth Road intersections of both Condamine Street and Roseberry Street are currently operating poorly with respect to localised traffic congestion along Kenneth Road over the 90-metre distance between Condamine and Roseberry streets with flow on adverse vehicle queues extending through the Roseberry Street roundabout and other approaches from the south, east and north.
- h) The lodged CBRK report acknowledges that queues regularly extend past the proposed driveway location within Roseberry Street, which is an indicator that the site location is an inappropriate location for a high traffic generating use, such as the proposed fast-food outlet.

Please contact the undersigned on 9521 7199 should you require further information or assistance. Yours faithfully,

M^cLaren Traffic Engineering

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Craig M^cLaren FIEAust Director & Mentor RPEQ 19457 BE Civil. Graduate Diploma (Transport Eng) MAITPM MITE [1985] TfNSW Accredited Level 3 Road Safety Auditor [1998] SafeWork NSW Traffic Control Work Training card, [Authorisation number TCT0015914 : Prepare Work Zone (PWZ)] Expert Traffic Engineering & Road Safety Witness at NSW Land & Environment & NSW Supreme Court





TECHNICAL MEMO 1 (96 SHEETS)



1 EXISITING TRAFFIC ENVIRONMENT

1.1 Turning Movement Count (TMC) Traffic Surveys

TMC traffic surveys were conducted at the intersections of Condamine Street / Kenneth Road and Kenneth Road / Roseberry Street during the following periods:

- Friday, 28 February 2025 between 2:00_{PM} to 7:00_{PM};
- Saturday, 29 February 2025 between 9:00AM to 2:00PM;
- Wednesday, 5 March 2025 between 6:00_{AM} to 10:00_{AM}, and 2:00_{PM} to 6:00_{PM}.

The full survey results are shown in **Annexure A** for reference.

1.1.1 Existing Road Performance

The performance of the surrounding intersections under the existing traffic conditions has been assessed using SIDRA INTERSECTION 9.1, with full SIDRA results reproduced in **Annexure B**.

The following considerations have been undertaken to ensure a realistic calibrated model:

- Consideration to the TCS Plan for signalised intersection of Condamine Street / Kenneth Road;
- A review of the phase length and cycle times based upon video footage;
 - Output cycle and phase duration fall within observed cycle and phase lengths.
- Validation of the model using approach queue lengths with consideration to the following input modifications:
 - Observed queue lengths along the eastern approaches of Kenneth Road to Condamine Street and Roseberry Street (see Section 2.1).

The resulting SIDRA INTERSECTION performance data is summarised in **Table 1**, **Table 2** and **Table 3** for the Friday survey peak, Saturday survey peak and Wednesday AM and PM survey peak, respectively.



TABLE 1: FRIDAY PEAK HOUR PERIOD – INTERSECTION PERFORMANCE SUMMARY (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ⁽¹⁾ | Average Delay ⁽²⁾ (sec/veh) | Level of Service ⁽³⁾⁽⁴⁾ | Control Typ e | Worst Movement | Average Queue | |
|----------------------|---------------------------------------|--|--|---------------------------------------|-----------------------------|---------------------|-------------------|--|
| | FRIDAY PEAK HOUR EXISTING PERFORMANCE | | | | | | | |
| Condamine Street | FRI | 1.00 | 46.2 | D | Signals | RT from Kenneth | 22.7 veh (159.2m) | |
| /Kenneth Road | | FRI 1.00 | 1.00 40.2 | b | Signals | Road | Condamine Street | |
| Kenneth Road | ED! | 0.00 | 15.5 | в | Deve debard | UT from | 5.6 veh (39.9m) | |
| /Roseberry Street | FRI | 0.90 | (Worst: 23.7) | (Worst: 23.7) (Worst: B) | | Roseberry Street | Kenneth Road | |

Notes:

(1) The Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.

(2) The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.

(3) The Level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from A to F, with A representing the best operational condition and level of service F the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.

(4) No overall Level of Service is provided for Give Way and Stop controlled intersections as the low delays associated with the dominant movements skew the average delay of the intersection. The Level of Service of the worst approach is an indicator of the operation of the intersection, with a worse Level of Service corresponding to long delays and reduced safety outcomes for that approach.

As shown above, during the Friday peak period, the intersection of Condamine Street / Kenneth Road performs with a Level of Service (LoS) "D". A LoS "D" indicates that the intersection is operating near capacity and any small increases in traffic flow is likely to cause operational problems. This is further evident by the degree of saturation of **1.0** which indicates that there is a movement within the intersection that is operating at capacity. A detailed review of the SIDRA outputs indicates that this corresponds to the RT from Kenneth Road (E), which performs at an LoS "F" indicating that this movement exceeds the available lane capacity.

During the Friday peak period, the intersection of Kenneth Road / Roseberry Street performs at an LoS "B". A LoS "B" is characterised by acceptable delays and spare capacity. Similarly, a detailed review of the SIDRA outputs indicate that the southern and eastern approaches have a degree of saturation of **0.86** and **0.90**, respectively. These movements are approaching capacity, although it is operating with acceptable performance at this stage.



TABLE 2: SATURDAY PEAK HOUR PERIOD – INTERSECTION PERFORMANCE SUMMARY (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ⁽¹⁾ | Average Delay ⁽²⁾ (sec/veh) | Level of Service ⁽³⁾⁽⁴⁾ | Control Typ e | Worst Movement | Average Queue | |
|----------------------|---|--|--|---------------------------------------|-----------------------------|-------------------|-------------------|------------------|
| | SATURDAY PEAK HOUR EXISTING PERFORMANCE | | | | | | | |
| Condamine Street | SAT | 0.94 | 45.4 | D | Signals | T from Kenneth | 25.7 veh (179.9m) | |
| /Kenneth Road | 0/11 | 0.34 | 0.04 40.4 | -0 D | 2 | Digitals | Road | Condamine Street |
| Kenneth Road | 0.07 | 0.00 | 15.7 | В | | UT from | 4.9 veh (34.4m) | |
| /Roseberry Street | SAT | 0.86 | (Worst: 23.1) | (Worst: B) | Roundabout | Kenneth Road | Kenneth Road | |

Notes: See Table 1.

During the Saturday peak period, the intersection of Condamine Street / Kenneth Road performs with a Level of Service (LoS) "D". Similar to the Friday peak period, Kenneth Road (E) is near capacity with the 'through' and 'right turn' movements performing with a LoS "F".

During the Saturday peak period, the intersection of Kenneth Road / Roseberry Street performs at an LoS "B". A LoS "B" is characterised by acceptable delays and spare capacity. It is acknowledged that the southern, eastern and western approaches are approaching movement saturation, although the intersection is currently performing with good efficiency.

TABLE 3: WEDNESDAY SURVEY PERIOD – INTERSECTION PERFORMANCE SUMMARY (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ⁽¹⁾ | Average Delay ⁽²⁾ (sec/veh) | Level of Service ⁽³⁾⁽⁴⁾ | Control Typ e | Worst Movement | Average Queue | | | | |
|----------------------|--------------|--|--|---------------------------------------|-----------------------------|----------------------|-------------------|---|--|---------|-----------------|
| | | | EXI | STING PERFO | RMANCE | | | | | | |
| | АМ | 0.77 3 | 34.9 | с | | RT from Kenneth | 17.6 veh (123.4m) | | | | |
| Condamine Street | | | 04.0 | | Signals | Road | Condamine Street | | | | |
| /Kenneth Road | РМ | 0.88 | 46.1 | D | | RT from Kenneth | 23.8 veh (166.6m) | | | | |
| | | 0.00 | | | | Road | Condamine Street | | | | |
| | АМ | | | | | 0.63 | 9.6 | Α | | UT from | 2.5 veh (18.1m) |
| Kenneth Road | | 0.03 | (Worst: 17) | (Worst: B) | | Roseberry Street | Kenneth Road | | | | |
| /Roseberry Street | DM | 0.63 | 10.1 | Α | Roundabout | UT from Roseberry | 2.4 veh (16.9m) | | | | |
| | PM | 0.05 | (Worst: 16.4) | (Worst: B) | (Worst: B) | | Roseberry Street | | | | |

Notes: See Table 1.

During the Wednesday survey periods, the intersection of Condamine Street / Kenneth Road performs with a LoS "C" during the AM peak hour period, and LoS "D" during the PM peak hour period. An LoS "C" is characterised by acceptable delays and some spare capacity.

During the AM peak hour period, although the performance of the signalised intersection is at a LoS "C", the RT from Kenneth Road (E) performs with an LoS "F". It is evident that this right turn movement exceeds capacity. During the PM peak hour period, the signalised intersection performs at an LoS "D", similar to the Friday and Saturday peak hour period.

During the Wednesday AM and PM peak hour periods, the intersection of Kenneth Road / Roseberry Street performs with an LoS "A", indicating a high level of efficiency with low approach delays and spare capacity.

2 SIDRA MODEL CALIBRATION

The SIDRA INTERSECTION 9.1 model was calibrated with due consideration to the cycle times, phase duration and queue lengths of the intersection of Condamine Street and Kenneth Avenue. A 30-minute segment of video footage for each of the periods surveyed was reviewed in detail (equivalent to approximately 10 signal phase cycles).

2.1 Signal Phases Review

In accordance with the TCS Plans (presented in **Annexure C**), the signalised intersection of Condamine Street / Kenneth Road operated with the "A", "C", "D", "E" and "E2" phases. From the video footage, it was also evident that new phases, not a part of the initial TCS Plan, were introduced. The "X" phase consists of a RT movement and T movement from Kenneth Road. The "Y" phase consists of RT movements from Kenneth Road (E) and Kenneth Road (W), and LT movements from Condamine Street (N) and Condamine Street (S), which is commonly referred to as a double-diamond phase.

The introduction of these phases is likely a result of excessive traffic demand from Kenneth Road (E) in the past.

In addition, the duration of the phases was reviewed with results presented in **Annexure D**. The phase durations and cycle times were input into the SIDRA Model to ensure a realistic calibrated model. The model was then cross referenced to the observed vehicle queue lengths further detailed **Section 2.2** below.

2.2 Vehicle Queue Observation

Screenshots of the video footage were extracted at the time when the signalised intersection of Condamine Street / Kenneth Road ran a phase which permitted traffic movements out of the eastern leg of Condamine Street / Kenneth Avenue to determine the vehicle queue lengths. A complete compilation of the screenshots is provided in the Annexures, in accordance with **Figure 1**.





FIGURE 1: OBSERVED VEHICLE QUEUE – SNAPSHOT LOCATION

A summary of the observed queue lengths of the eastern approaches to the intersections of Condamine Street / Kenneth Avenue and Kenneth Avenue / Roseberry Street is provided in **Table 4** and **Table 5**, respectively.

| TABLE 4. REINELTI ROAD (E) ATTROACT TO CONDAMINE OTREET | | | | | | | | |
|---|-----------------------------|--------------------------|--|--|--|--|--|--|
| | | Approx | Approximate Observed Queue Lengths (m) | | | | | |
| Approach | Observed Signal Cycle | Friday, 27 March 2025 | Saturday, 28 March 2025 | Wednesday, 5 March 2025 - AM Period | Wednesday, 5 March 2025 - PM Period | | | |
| | 1 | 83m | 70m | 42m | 90m | | | |
| | 2 | 49m | 70m | 35m | 77m | | | |
| | 3 | 42m | 90m | 21m | 49m | | | |
| Kenneth | 4 | 56m | 90m | 35m | 42m | | | |
| Road (E) | 5 | 90m | 90m | 49m | 90m | | | |
| Approach to | 6 | 90m | 90m | 42m | 83m | | | |
| Condamine | 7 | 90m | 56m | 49m | 49m | | | |
| Street | 8 | 90m | 70m | 42m | 63m | | | |
| | 9 | 90m | 56m | - | 35m | | | |
| | 10 | 90m | 49m | 77m | 35m | | | |
| | 11 | - | - | - | - | | | |
| Average Queue | - | 77m | 73.1m | 43.5m | 61.3m | | | |

TABLE 4: KENNETH ROAD (E) APPROACH TO CONDAMINE STREET

NOTE:

(1) A "90m" queue indicates a queue which extends from the signalised intersection at Condamine Street / Kenneth Road to the roundabout at Kenneth Road / Roseberry Street (i.e. the lane approaches are at capacity).



| IABLE | J. KENNEI | | PROACH TO R | USEDERKT S | |
|------------------|-----------------------------|--------------------------|----------------------------|--|--|
| | | Appr | oximate Obser | ved Queue Ler | ngths |
| Approach | Observed Signal Cycle | Friday, 27 March 2025 | Saturday, 28 March 2025 | Wednesday, 5 March 2025 - AM Period | Wednesday, 5 March 2025 - PM Period |
| | 1 | - | 28m | - | - |
| | 2 | 7m | 42m | 21m | - |
| | 3 | 21m | 56m | - | - |
| Kenneth | 4 | 7m | 42m | - | 35m |
| Road (E) | 5 | 35m | 180m | - | 7m |
| Approach to | 6 | 63m | 7m | - | 7m |
| Roseberry | 7 | - | - | - | 14m |
| Street | 8 | 28m | - | - | 7m |
| | 9 | 14m | 21m | - | - |
| | 10 | 7m | 7m | 21m ⁽²⁾ | 7m |
| | 11 | 180m | - | - | - |
| Average Queue | - | 36.2m | 38.3m | 21m | 12.8m |

TABLE 5: KENNETH ROAD (E) APPROACH TO ROSEBERRY STREET

NOTE:

(1) A "180m" queue indicates a queue which extends from the roundabout intersection at Kenneth Road / Roseberry Street to the roundabout at Kenneth Road / Quirk Road (i.e. the lane approach is at capacity).

(2) Bus obstructs view of back of queue.

The queues determined in **Table 4** and **Table 5**, approximately reflect the queues calculated by SIDRA INTERSECTION 9.1, ensuring a realistic calibrated model.

2.3 Notable Observations

The following observations are relevant to note based on the review of the video footage:

- It was observed that the eastern queue at the signalised intersection at times extended
 past the roundabout of Kenneth Road / Roseberry Street. In instances, the queue
 extended even further to the roundabout of Kenneth Avenue / Quirk Road. This does
 not occur over a whole peak hour period and only occurs for a concentrated 10-minute
 period.
 - Although this should impact the performance of the roundabout, particularly Kennth Road / Roseberry Street, the queues do tend to clear outside of the concentrated 10-minute period. SIDRA calculates average delay based on the whole hour which would lower the overall average delay when compared to a 10-minute peak flow.
- The eastern approach to the signalised intersection is evidently at capacity. Lane blockage occurs caused by the RT movement from Kenneth Road (E), limiting traffic throughput from the eastern approach, particularly the T and LT movements from Kenneth Road (E).



ANNEXURE A: TRAFFIC SURVEY DATA (6 SHEETS)

TRANS TRAFFIC SURVEY DNV-GL

Intersection of Kenneth Rd and Condamine St, Sydney GPS -33,786520, 151,266679

| Ti | ime North | Approach Conda | mine St | East Approac | h Kennet | h Rd | Sout | h Approach Condam | ine |
|--------------|----------------------|----------------|---------|--------------|----------|---------|----------|-------------------|-----|
| All Vehicles | 5 | | | | | | | | |
| | | | | | | | | | |
| Customer: | McLaren | West: | Kenneth | Rd | 1 | Peak | PM: | 3:00 PM-4:00 PM | 1 |
| Suburban: | Sydney | South: | Condami | ne St | 1 1 | Traffic | AM: | #REF! | 1 |
| Weather: | Overcast | East: | Kenneth | Rd | | Period | PM: | 2:00 PM-7:00 PM | |
| Date: | Fri 28/02/25 | North: | Condami | |] [| Survey | 2 State. | 2:00 PM-2:00 PM |] |
| 013 | -33.786520, 151.2666 | | | | | | | | |

| | me | North | Approaci | h Condan | nine St | East | t Approac | h Kenne | th Rd | Sout | h Approac | h Condam | ine St | Wes | t Approa | ch Kenne | th Rd | Hourt | y Total |
|------------|--|-------|----------|----------|---------|-----------------------------|-----------|---------|-------|------|----------------------------|----------|--------|-----|----------|----------|-------|---------------|---------|
| eriod Star | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | Hour | Peak |
| 14:00 | 14:15 | 0 | 15 | 260 | 17 | 0 | 61 | 13 | 89 | 0 | 65 | 275 | 15 | 0 | 37 | 16 | 11 | 3509 | |
| 14:15 | 14:30 | 0 | 8 | 290 | 11 | 0 | 53 | 9 | 67 | 0 | 45 | 208 | 10 | 0 | 17 | 24 | 16 | 3598 | |
| 14:30 | 14:45 | 0 | 8 | 238 | 18 | 0 | 55 | 17 | 99 | 0 | 93 | 376 | 17 | 0 | 18 | 7 | 8 | 3871 | |
| 14:45 | 15:00 | 1 | 11 | 218 | 9 | 0 | 62 | 30 | 92 | 0 | 92 | 357 | 17 | 0 | 14 | 12 | 8 | 3871 | |
| 15:00 | 15:15 | 1 | 13 | 285 | 23 | 0 | 44 | 10 | 107 | 0 | 87 | 318 | 16 | 0 | 25 | 17 | 17 | 4044 | Pea |
| 15:15 | 15:30 | 0 | 17 | 296 | 9 | 0 | 55 | 19 | 94 | 1 | 95 | 335 | 22 | 0 | 39 | 33 | 16 | 3957 | |
| 15:30 | 15:45 | 0 | 10 | 258 | 6 | 0 | 63 | 21 | 80 | 0 | 96 | 343 | 16 | 0 | 27 | 15 | 19 | 3946 | |
| 15:45 | 16:00 | 0 | 14 | 290 | 15 | 0 | 53 | 15 | 92 | 0 | 104 | 411 | 30 | 0 | 38 | 21 | 13 | 3901 | |
| 16:00 | 16:15 | 0 | 17 | 224 | 12 | 0 | 59 | 20 | 64 | 0 | 83 | 300 | 17 | 0 | 32 | 22 | 26 | 3778 | |
| 16:15 | 16:30 | 0 | 4 | 288 | 17 | 0 | 65 | 16 | 65 | 1 | 86 | 409 | 19 | 0 | 28 | 14 | 8 | 3769 | |
| 16:30 | 16:45 | 0 | 12 | 232 | 9 | 0 | 46 | 19 | 66 | 0 | 95 | 368 | 19 | 0 | 20 | 17 | 6 | 3730 | |
| 16:45 | 17:00 | 0 | 11 | 270 | 14 | 0 | 56 | 19 | 61 | 0 | 106 | 346 | 17 | 0 | 21 | 30 | 22 | 3698 | |
| 17:00 | 17:15 | 0 | 14 | 257 | 9 | 0 | 57 | 18 | 70 | 0 | 94 | 285 | 16 | 0 | 25 | 11 | 11 | 3617 | |
| 17:15 | 17:30 | 0 | 14 | 294 | 20 | 0 | 56 | 20 | 63 | 0 | 87 | 350 | 14 | 0 | 28 | 17 | 18 | 3557 | |
| 17:30 | 17:45 | 1 | 12 | 257 | 10 | 0 | 46 | 23 | 78 | 0 | 103 | 265 | 15 | 0 | 28 | 20 | 19 | 3409 | |
| 17:45 | 18:00 | 0 | 16 | 303 | 10 | 0 | 42 | 12 | 58 | 0 | 95 | 276 | 20 | 0 | 28 | 19 | 13 | 3299 | |
| 18:00 | 18:15 | 0 | 10 | 220 | 13 | 0 | 56 | 25 | 69 | 0 | 91 | 243 | 18 | 0 | 27 | 21 | 14 | 3128 | |
| 18:15 | 18:30 | 0 | 14 | 235 | 9 | 0 | 45 | 16 | 59 | 0 | 93 | 277 | 15 | 0 | 34 | 15 | 21 | | |
| 18:30 | 18:45 | 1 | 11 | 196 | 12 | 0 | 47 | 15 | 65 | 0 | 92 | 257 | 16 | 0 | 32 | 9 | 14 | | |
| 18:45 | 19:00 | 0 | 10 | 175 | 11 | 0 | 41 | 18 | 79 | 0 | 66 | 246 | 18 | 0 | 23 | 14 | 20 | | |
| Peak | Peak Time North Approach Condamine St East Approach Kenneth Rd | | | | th Rd | South Approach Condamine St | | | | | t West Approach Kenneth Rd | | | | 1 | | | | |
| | Period End | U | R | SB | L | U | R | WB | | U | R | NB | L | U | R | EB | L | Peak total | |
| 15:00 | 16:00 | 1 | 54 | 1129 | 53 | 0 | 215 | 65 | 373 | 1 | 382 | 1407 | 84 | 0 | 129 | 86 | 65 | 4044 | 1 |

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Hausha Tatal

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configu

| Graphic |
|---------|
| Total |
| Light |
| Heavy |



TRANS TRAFFIC SURVEY

Intersection of Kenneth Rd and Roseberry St, Sydney
GPS -33,786730, 151.267944

| Date: | Fri 28/02/25 | North: | Roseberry St | 1 1 | Survey | AM: | 2:00 PM-2:00 PM |
|-----------|--------------|--------|--------------|-----|---------|-----|-----------------|
| Weather: | Overcast | East: | Kenneth Rd | 1 | Period | PM: | 2:00 PM-7:00 PM |
| Suburban: | Sydney | South: | Roseberry St | 1 | Traffic | AM: | #REF! |
| Customer: | McLaren | West: | Kenneth Rd | 1 | Peak | PM: | 3:00 PM-4:00 PM |

| Time North Approach Roseberry Si Period Starl Period End U R SB L | | | erry St | | | | | | | | | | | | | Hourly Total | | | |
|--|------------|-------|---------|----------|---------|------|---------|---------|-------|------|-----------|------------|--------|-----|-----------|--------------|-------|-------|------|
| Period Star | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | Hour | Peak |
| 14:00 | 14:15 | 0 | 12 | 20 | 4 | 0 | 3 | 77 | 34 | 2 | 36 | 18 | 66 | 6 | 23 | 63 | 7 | 1568 | |
| 14:15 | 14:30 | 0 | 9 | 28 | 5 | 2 | 1 | 61 | 36 | 1 | 44 | 19 | 53 | 3 | 22 | 51 | 5 | 1629 | |
| 14:30 | 14:45 | 0 | 11 | 37 | 2 | 0 | 2 | 96 | 33 | 1 | 42 | 12 | 63 | 4 | 14 | 94 | 7 | 1762 | |
| 14:45 | 15:00 | 2 | 24 | 41 | 3 | 0 | 5 | 96 | 39 | 0 | 48 | 10 | 57 | 5 | 21 | 82 | 6 | 1806 | |
| 15:00 | 15:15 | 1 | 9 | 34 | 5 | 3 | 1 | 97 | 39 | 1 | 44 | 19 | 54 | 4 | 22 | 95 | 4 | 1837 | Peak |
| 15:15 | 15:30 | 0 | 21 | 57 | 3 | 2 | 1 | 89 | 41 | 0 | 52 | 16 | 52 | 6 | 13 | 108 | 12 | 1821 | |
| 15:30 | 15:45 | 2 | 16 | 45 | 8 | 2 | 3 | 94 | 46 | 2 | 62 | 16 | 51 | 1 | 19 | 85 | 10 | 1757 | |
| 15:45 | 16:00 | 1 | 12 | 41 | 5 | 1 | 2 | 93 | 35 | 0 | 52 | 30 | 56 | 1 | 14 | 113 | 14 | 1690 | |
| 16:00 | 16:15 | 1 | 10 | 38 | 10 | 1 | 5 | 71 | 35 | 1 | 53 | 17 | 59 | 1 | 22 | 84 | 8 | 1648 | |
| 16:15 | 16:30 | 0 | 9 | 32 | 5 | 2 | 0 | 80 | 36 | 2 | 52 | 17 | 57 | 2 | 17 | 87 | 11 | 1640 | |
| 16:30 | 16:45 | 0 | 12 | 31 | 7 | 1 | 3 | 65 | 29 | 4 | 45 | 21 | 54 | 2 | 17 | 90 | 14 | 1629 | |
| 16:45 | 17:00 | 2 | 6 | 46 | 7 | 2 | 2 | 68 | 32 | 0 | 38 | 16 | 59 | 2 | 19 | 120 | 9 | 1652 | |
| 17:00 | 17:15 | 1 | 12 | 39 | 4 | 2 | 2 | 69 | 38 | 2 | 49 | 20 | 54 | 8 | 18 | 85 | 5 | 1592 | |
| 17:15 | 17:30 | 0 | 16 | 35 | 9 | 2 | 4 | 73 | 40 | 0 | 32 | 19 | 46 | 6 | 11 | 90 | 15 | 1568 | |
| 17:30 | 17:45 | 0 | 14 | 31 | 5 | 0 | 5 | 94 | 34 | 0 | 45 | 20 | 35 | 6 | 17 | 99 | 13 | 1512 | |
| 17:45 | 18:00 | 1 | 9 | 26 | 7 | 0 | 5 | 66 | 41 | 3 | 41 | 14 | 32 | 7 | 18 | 88 | 10 | 1446 | |
| 18:00 | 18:15 | 1 | 10 | 16 | 6 | 2 | 4 | 78 | 40 | 0 | 35 | 11 | 54 | 6 | 19 | 91 | 11 | 1417 | |
| 18:15 | 18:30 | 1 | 10 | 23 | 6 | 1 | 3 | 66 | 26 | 3 | 33 | 11 | 40 | 4 | 15 | 97 | 3 | | |
| 18:30 | 18:45 | 1 | 9 | 22 | 4 | 1 | 3 | 73 | 32 | 1 | 37 | 13 | 41 | 5 | 14 | 89 | 7 | | |
| 18:45 | 19:00 | 1 | 7 | 17 | 3 | 3 | 5 | 80 | 28 | 0 | 39 | 17 | 47 | 6 | 16 | 65 | 5 | | |
| Peak | Time | North | Annroad | h Rosebe | arry St | Fast | Annroad | h Kenne | th Rd | Sout | th Approa | ch Roseber | rrv St | Wes | t Approad | h Kenne | th Rd | Peak | 1 |
| | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | total | |
| 15:00 | 16:00 | 4 | 58 | 177 | 21 | 8 | 7 | 373 | 161 | 3 | 210 | 81 | 213 | 12 | 68 | 401 | 40 | 1837 | 1 |

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration

| Graphic |
|---------|
| Total |
| Light |
| Heavy |



TURNING MOVEMENT SURVEY

Intersection of Kenneth Rd and Condamine St, Sydney

| GPS | -33.786520, 151.2666 | 79 |
|-----------|----------------------|----|
| Date: | Sat 01/03/25 | |
| Weather: | Overcast | |
| Suburban: | Sydney | |
| Customer: | McLaren | |

North: Condamine St East: Kenneth Rd South: Condamine St West: Kenneth Rd

 Survey
 AM:
 9:00 AM-12:00 PM

 Period
 PM:
 12:00 PM-2:00 PM

 Traffic
 AM:
 10:15 AM-11:15 AM

 Peak
 PM:
 12:00 PM-1:00 PM

| All Vehicle | s ime | Marth | Annes | h Condan | nine St | Erret | Annes | h Kennet | h Dd | C | h Annes | h Condami | ine Ct | M | Anner | ch Kenne | ih Da | Hard | v Total |
|-------------|------------------|-------|--------------|----------|---------|-------|---------|----------|-------|------|----------------|-----------|--------|-------|----------|----------|-------|-------|---------|
| | me Period End | U | Approac R | SB | L | U | R | WB | L | U | n Approac R | NB | L | - Wes | R | EB | | Hour | Peak |
| 9:00 | 9:15 | 1 | 4 | 272 | 13 | 0 | 50 | 9 | 69 | 0 | 84 | 234 | 3 | 0 | 17 | 7 | 7 | 3379 | I Cak |
| 9:15 | 9:30 | 0 | 3 | 245 | 12 | 0 | 64 | 9 | 85 | 0 | 71 | 310 | 5 | 0 | 13 | 5 | 5 | 3354 | |
| 9:30 | 9:45 | 0 | 3 | 287 | 16 | 0 | 56 | 5 | 121 | 0 | 84 | 288 | 10 | 0 | 17 | 11 | 5 | 3501 | |
| 9:45 | 10:00 | 1 | 6 | 279 | 12 | 0 | 62 | 14 | 68 | 0 | 64 | 327 | 11 | 0 | 12 | 11 | 12 | 3516 | |
| 10:00 | 10:15 | 1 | 5 | 220 | 13 | 0 | 65 | 12 | 83 | 0 | 48 | 256 | 8 | 0 | 21 | 8 | 5 | 3584 | |
| 10:15 | 10:30 | 0 | 8 | 306 | 19 | 0 | 62 | 9 | 83 | 0 | 71 | 371 | 12 | 0 | 20 | 8 | 5 | 3784 | Peak |
| 10:30 | 10:45 | 0 | 5 | 277 | 13 | 0 | 61 | 14 | 74 | 0 | 85 | 328 | 19 | 0 | 20 | 15 | 7 | 3758 | |
| 10:45 | 11:00 | 0 | 7 | 290 | 11 | 0 | 56 | 18 | 111 | 0 | 84 | 308 | 16 | 0 | 26 | 8 | 12 | 3748 | |
| 11:00 | 11:15 | 1 | 9 | 295 | 14 | 0 | 57 | 18 | 96 | 0 | 62 | 329 | 16 | 0 | 19 | 18 | 11 | 3779 | |
| 11:15 | 11:30 | 0 | 10 | 273 | 10 | 0 | 72 | 14 | 99 | 0 | 100 | 301 | 13 | 0 | 34 | 11 | 11 | | |
| 11:30 | 11:45 | 0 | 9 | 365 | 19 | 0 | 52 | 14 | 112 | 0 | 43 | 251 | 14 | 0 | 10 | 9 | 10 | | |
| 11:45 | 12:00 | 1 | 6 | 287 | 17 | 0 | 68 | 19 | 87 | 0 | 77 | 335 | 19 | 0 | 28 | 16 | 18 | | |
| 12:00 | 12:15 | 0 | 15 | 323 | 13 | 0 | 64 | 9 | 71 | 0 | 90 | 309 | 13 | 0 | 25 | 5 | 21 | 3872 | Peak |
| 12:15 | 12:30 | 0 | 13 | 320 | 17 | 0 | 52 | 8 | 101 | 0 | 84 | 348 | 18 | 0 | 34 | 12 | 13 | 3843 | |
| 12:30 | 12:45 | 0 | 9 | 264 | 16 | 0 | 65 | 11 | 90 | 0 | 93 | 296 | 15 | 0 | 30 | 6 | 11 | 3772 | |
| 12:45 | 13:00 | 0 | 10 | 310 | 18 | 0 | 54 | 20 | 76 | 0 | 103 | 327 | 22 | 0 | 19 | 14 | 15 | 3751 | |
| 13:00 | 13:15 | 0 | 11 | 329 | 14 | 0 | 61 | 19 | 72 | 0 | 77 | 264 | 18 | 0 | 27 | 15 | 22 | 3700 | |
| 13:15 | 13:30 | 0 | 14 | 297 | 24 | 0 | 55 | 17 | 102 | 0 | 76 | 304 | 14 | 0 | 22 | 8 | 16 | | |
| 13:30 | 13:45 | 1 | 10 | 267 | 7 | 0 | 69 | 18 | 73 | 0 | 87 | 298 | 13 | 0 | 22 | 11 | 9 | | |
| 13:45 | 14:00 | 0 | 11 | 311 | 13 | 0 | 55 | 16 | 96 | 0 | 96 | 279 | 12 | 0 | 23 | 18 | 7 | | |
| Peak | Time | North | Approac | h Condan | nine St | East | Approac | h Kennet | th Rd | Sout | h Approac | h Condami | ine St | Wes | t Approa | ch Kenne | th Rd | Peak | 1 |
| | Period End | U | R | SB | | U | R | WB | | U U | R | NB | L | U | R | EB | | total | 4 |

| 10:15 | 11:15 | 1 | 29 | 1168 | 57 | 0 | 236 | 59 | 364 | 0 | 302 | 1336 | 63 | 0 | 85 | 49 | 35 | 3784 |
|---------------|-------------------|-------------|--------------|------------|-------------|-----------|------------|-----------|------------|------------|--------------|-------------|----|---|-----|----|----|------|
| 12:00 | 13:00 | 0 | 47 | 1217 | 64 | 0 | 235 | 48 | 338 | 0 | 370 | 1280 | 68 | 0 | 108 | 37 | 60 | 3872 |
| | | | | | | | | | | | | | | | | | | |
| Note: Site st | ketch is for illu | ustrating t | raffic flow: | s Directio | n is indica | tive only | drawing is | not to sc | ale and no | of an exac | t streets co | nfiguration | | | | | | |





TRANS TRAFFIC SURVEY

Intersection of Kenneth Rd and Roseberry St, Sydney

| | -33.786730, 151.26794 | | | | | |
|--------------|-----------------------|-------|----------------|------------|-----|-------------------|
| Date: | Sat 01/03/25 | North | | Survey | | 9:00 AM-12:00 PM |
| Weather: | Overcast | East: | Kenneth Rd | Period | PM: | 12:00 PM-2:00 PM |
| Suburban: | | South | : Roseberry St | Traffic | AM: | 10:30 AM-11:30 AM |
| Customer: | McLaren | West: | Kenneth Rd | Peak | PM: | 12:00 PM-1:00 PM |
| | | | | | | |
| All Vehicles | 1 | | | | | |

| 7 III FCINOICO | | | | | | | - | | | | | | | | | | | | |
|-----------------------|----------------|--------|----------|-----------|----------|---|---------|-----------|----------|--------|----------|------------|----------|---------|----------|-----------|---------|---------------|---------|
| | ime | | | h Rosebe | erry St | | | h Kennet | | | | ch Roseber | - | | t Approa | | | | y Total |
| Period Star | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | Hour | Peak |
| 9:00 | 9:15 | 0 | 3 | 24 | 2 | 1 | 3 | 75 | 37 | 2 | 49 | 10 | 47 | 5 | 16 | 77 | 5 | 1531 | |
| 9:15 | 9:30 | 0 | 10 | 33 | 3 | 1 | 0 | 86 | 45 | 0 | 54 | 12 | 62 | 2 | 14 | 67 | 4 | 1564 | |
| 9:30 | 9:45 | 0 | 9 | 22 | 4 | 1 | 2 | 102 | 43 | 1 | 53 | 8 | 68 | 4 | 21 | 86 | 2 | 1586 | |
| 9:45 | 10:00 | 0 | 10 | 39 | 5 | 0 | 0 | 75 | 41 | 1 | 37 | 8 | 52 | 5 | 17 | 60 | 6 | 1588 | |
| 10:00 | 10:15 | 0 | 6 | 34 | 5 | 0 | 4 | 93 | 49 | 2 | 51 | 20 | 57 | 2 | 18 | 45 | 3 | 1679 | |
| 10:15 | 10:30 | 0 | 8 | 33 | 4 | 0 | 1 | 84 | 50 | 0 | 55 | 21 | 60 | 4 | 20 | 66 | 9 | 1739 | |
| 10:30 | 10:45 | 1 | 12 | 37 | 5 | 0 | 0 | 75 | 61 | 3 | 46 | 20 | 57 | 3 | 16 | 88 | 4 | 1796 | Peak |
| 10:45 | 11:00 | 0 | 10 | 29 | 8 | 0 | 2 | 108 | 50 | 0 | 49 | 23 | 63 | 6 | 19 | 73 | 7 | 1784 | |
| 11:00 | 11:15 | 1 | 17 | 39 | 0 | 0 | 2 | 94 | 68 | 2 | 50 | 24 | 58 | 4 | 17 | 65 | 8 | 1760 | |
| 11:15 | 11:30 | 2 | 14 | 34 | 6 | 1 | 1 | 105 | 57 | 1 | 50 | 22 | 60 | 5 | 15 | 89 | 10 | | |
| 11:30 | 11:45 | 0 | 13 | 39 | 7 | 1 | 2 | 93 | 57 | 2 | 38 | 21 | 71 | 2 | 17 | 51 | 2 | | |
| 11:45 | 12:00 | 1 | 14 | 31 | 4 | 0 | 2 | 102 | 48 | 0 | 38 | 17 | 56 | 3 | 24 | 70 | 13 | | |
| 12:00 | 12:15 | 0 | 9 | 44 | 6 | 1 | 5 | 84 | 57 | 2 | 36 | 30 | 46 | 2 | 17 | 82 | 8 | 1766 | Peak |
| 12:15 | 12:30 | 0 | 15 | 31 | 5 | 0 | 3 | 80 | 46 | 2 | 59 | 17 | 66 | 2 | 26 | 83 | 3 | 1750 | |
| 12:30 | 12:45 | 1 | 13 | 40 | 6 | 0 | 5 | 90 | 51 | 1 | 44 | 22 | 64 | 2 | 15 | 93 | 3 | 1764 | |
| 12:45 | 13:00 | 1 | 8 | 33 | 4 | 0 | 1 | 66 | 55 | 2 | 52 | 18 | 72 | 5 | 21 | 100 | 11 | 1705 | |
| 13:00 | 13:15 | 2 | 9 | 33 | 9 | 0 | 6 | 82 | 39 | 2 | 44 | 24 | 58 | 2 | 16 | 78 | 9 | 1698 | |
| 13:15 | 13:30 | 1 | 11 | 39 | 4 | 1 | 4 | 89 | 49 | 1 | 57 | 16 | 73 | 3 | 18 | 76 | 10 | | |
| 13:30 | 13:45 | 0 | 11 | 33 | 9 | 1 | 2 | 83 | 31 | 0 | 34 | 21 | 63 | 1 | 22 | 75 | 5 | | |
| 13:45 | 14:00 | 0 | 12 | 35 | 6 | 0 | 4 | 89 | 40 | 3 | 42 | 17 | 65 | 3 | 15 | 100 | 11 | | |
| | - | | | | ~ | - | | | | | | | | | | | | | |
| | Time | | | h Rosebe | | | | h Kennet | | | | h Roseber | | | t Approa | | | Peak | |
| Period Start 10:30 | Period End | U 4 | R 53 | SB 139 | L 19 | U | R 5 | WB 382 | L 236 | U 6 | R 195 | NB 89 | L 238 | U 18 | R 67 | EB 315 | L 29 | total 1796 | |
| 10:30 | 11:30 13:00 | 2 | 53 45 | 139 | 19 21 | 1 | 5 14 | 382 | 236 | 6 | 195 | 89 | 238 | 18 | 67 79 | 315 | 29 | 1796 | |
| 12.00 | 13.00 | - 2 | 45 | 140 | 21 | 1 | 14 | 320 | 209 | | 191 | - 67 | 240 | 0 | 79 | 300 | 25 | 1/00 | |

 WB
 L

 382
 236

 320
 209
 U 4 2
 R
 SB
 L

 53
 139
 19

 45
 148
 21
 R 5 14 NB 89 87 R 195 191 6 1 Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration.







Intersection of Kenneth Rd and Condamine St, Sydney

| GPS | -33.786520, 151.2666 | 579 | | | | | | | | | | | | |
|--------------|----------------------|-----|--------|----|--------|-------|--|---|---------|-----|--------|---------|------|---|
| Date: | Wed 05/03/25 |] | North: | Co | ondami | ne St | |] | Survey | AM: | 6:00 A | M-10:0 | 0 AM | Γ |
| Weather: | Overcast | 1 | East: | Ke | enneth | Rd | | 1 | Period | PM: | 2:00 F | PM-6:00 | PM | |
| Suburban: | Sydney | 1 | South: | Co | ondami | ne St | | 1 | Traffic | AM: | 8:15 / | M-9:15 | AM | ٦ |
| Customer: | McLaren | 1 | West: | Ke | enneth | Rd | | 1 | Peak | PM: | 4:45 F | M-5:45 | PM | |
| | | - | | | | | | - | | | | | | _ |
| All Vehicles | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

| Time Period Starl PA 6:00 6:15 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 8:30 | | U 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | R 0 2 5 2 4 6 8 6 4 6 | h Condan SB 239 312 348 308 276 298 245 282 217 202 | L 11 15 21 16 26 23 17 17 5 | U 0 0 0 0 0 0 | R 12 24 24 39 31 40 44 | Kennet WB 1 2 5 5 16 7 | L 80 105 82 68 69 | U 0 0 1 0 | R 18 50 42 56 | h Condami NB 115 182 160 243 | L 3 5 5 7 | U 0 0 0 | R 11 15 15 15 | Ch Kennet EB 6 8 10 5 | L 3 8 6 3 | Hour 2717 2907 2922 2911 | y Total Peak |
|---|--|--|---|--|--|---------------------------------|---|--|----------------------------------|-----------------------|---------------------------|---|-----------------------|------------------|---------------------------|--------------------------------------|-----------------------|--------------------------------------|-----------------|
| 6:00 6:15 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 | 6:15 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 0 0 0 0 0 0 0 | 0 2 5 2 4 6 8 8 6 4 | 239 312 348 308 276 298 245 282 217 | 11 15 21 16 28 23 17 17 | 0 0 0 0 0 | 12 24 24 39 31 40 | 1 2 5 5 16 | 80 105 82 66 | 0 0 1 | 18 50 42 58 | 115 182 160 | 3 5 5 | 0 | 11 15 15 | 6 8 10 | 3 8 6 | 2717 2907 2922 | |
| 6:15 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 | 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 0 0 0 0 0 0 0 | 2 5 2 4 6 8 6 4 | 312 348 308 276 298 245 282 217 | 15 21 16 26 23 17 17 | 0 0 0 0 0 0 0 | 24 24 39 31 40 | 2 5 5 16 | 105 82 66 | 0 | 50 42 56 | 182 160 | 5 | 0 | 15 15 | 10 | 6 | 2907 2922 | |
| 6:30 6:45 7:00 7:15 7:30 7:45 8:00 8:15 | 6:45 7:00 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 0 0 0 0 0 | 5 2 4 6 8 6 4 | 348 308 276 298 245 282 217 | 21 16 26 23 17 17 | 0 0 0 0 0 0 0 | 24 39 31 40 | 5 5 16 | 82 66 | 0 | 42 56 | 160 | 5 | 0 | 15 | 10 | 6 | 2922 | |
| 6:45 7:00 7:15 7:30 7:45 8:00 8:15 | 7:00 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 0 0 0 0 | 2 4 6 8 6 4 | 308 276 298 245 282 217 | 16 26 23 17 17 | 0 0 0 0 0 | 39 31 40 | 5 | 66 | 1 | 56 | | | | | | | <u> </u> | |
| 7:15 7:30 7:45 8:00 8:15 | 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 0 0 | 4 6 8 6 4 | 298 245 282 217 | 26 23 17 17 | 0 | 31 40 | 16 | | — | | | | | | 1 9 | | | |
| 7:30 7:45 8:00 8:15 | 7:45 8:00 8:15 8:30 8:45 9:00 | 0 0 0 | 8 6 4 | 245 282 217 | 17 17 | 0 | | 7 | | | 27 | 192 | 13 | 0 | 14 | 16 | 6 | 3001 | |
| 7:30 7:45 8:00 8:15 | 8:00 8:15 8:30 8:45 9:00 | 0 | 6 4 | 282 217 | 17 | | 44 | | 70 | 0 | 38 | 224 | 5 | 0 | 12 | 13 | 7 | 3053 | |
| 8:00 | 8:15 8:30 8:45 9:00 | 0 | 4 | 217 | | - | | 11 | 64 | 0 | 45 | 228 | 12 | 0 | 16 | 15 | 7 | 3132 | |
| 8:15 | 8:30 8:45 9:00 | 0 | | | 5 | 0 | 55 | 13 | 62 | 0 | 48 | 308 | 17 | 0 | 19 | 18 | 11 | 3288 | |
| | 8:45 9:00 | _ | 6 | 202 | · · | 0 | 55 | 14 | 50 | 0 | 50 | 289 | 7 | 0 | 22 | 12 | 17 | 3344 | |
| 8:30 | 9:00 | 0 | | 282 | 7 | 0 | 50 | 9 | 49 | 0 | 67 | 316 | 4 | 0 | 17 | 11 | 4 | 3468 | Peak |
| | | | 7 | 298 | 10 | 0 | 57 | 28 | 60 | 0 | 56 | 301 | 9 | 0 | 20 | 11 | 11 | 3446 | |
| 8:45 | 0.15 | 1 | 4 | 290 | 12 | 0 | 67 | 26 | 62 | 0 | 44 | 324 | 17 | 0 | 32 | 29 | 4 | 3334 | |
| 9:00 | 8.10 | 0 | 4 | 268 | 15 | 0 | 54 | 14 | 93 | 1 | 61 | 299 | 9 | 0 | 21 | 23 | 4 | 3205 | |
| 9:15 | 9:30 | 0 | 7 | 282 | 16 | 0 | 53 | 8 | 73 | 0 | 55 | 273 | 7 | 0 | 9 | 9 | 8 | | |
| 9:30 | 9:45 | 0 | 6 | 243 | 9 | 0 | 53 | 11 | 76 | 0 | 49 | 274 | 8 | 0 | 9 | 10 | 8 | | |
| 9:45 | 10:00 | 0 | 4 | 224 | 9 | 0 | 50 | 7 | 65 | 0 | 80 | 277 | 13 | 0 | 26 | 13 | 15 | | |
| 14:00 | 14:15 | 0 | 4 | 252 | 16 | 0 | 51 | 14 | 59 | 0 | 54 | 254 | 16 | 0 | 25 | 4 | 7 | 3301 | |
| 14:15 | 14:30 | 1 | 6 | 266 | 11 | 0 | 57 | 14 | 75 | 0 | 51 | 271 | 12 | 0 | 20 | 15 | 10 | 3407 | |
| 14:30 | 14:45 | 1 | 7 | 243 | 11 | 0 | 44 | 23 | 73 | 0 | 74 | 343 | 12 | 0 | 19 | 9 | 16 | 3617 | |
| 14:45 | 15:00 | 0 | 15 | 257 | 6 | 0 | 59 | 27 | 76 | 0 | 64 | 310 | 7 | 0 | 20 | 9 | 11 | 3658 | |
| 15:00 | 15:15 | 0 | 12 | 240 | 10 | 0 | 47 | 11 | 73 | 0 | 70 | 323 | 13 | 0 | 23 | 28 | 12 | 3763 | |
| 15:15 | 15:30 | 1 | 7 | 307 | 9 | 0 | 59 | 10 | 89 | 0 | 78 | 393 | 16 | 0 | 21 | 17 | 12 | 3857 | |
| 15:30 | 15:45 | 1 | 16 | 209 | 9 | 0 | 58 | 20 | 63 | 0 | 89 | 384 | 13 | 0 | 19 | 19 | 16 | 3815 | |
| 15:45 | 16:00 | 0 | 13 | 246 | 11 | 0 | 51 | 16 | 79 | 0 | 106 | 373 | 21 | 0 | 18 | 15 | 17 | 3798 | |
| 16:00 | 16:15 | 0 | 14 | 246 | 13 | 0 | 61 | 14 | 60 | 0 | 87 | 380 | 26 | 0 | 25 | 16 | 14 | 3817 | |
| 16:15 | 16:30 | 1 | 11 | 299 | 15 | 0 | 49 | 13 | 65 | 0 | 89 | 374 | 20 | 0 | 13 | 13 | 15 | 3863 | |
| 16:30 | 16:45 | 0 | 5 | 241 | 13 | 0 | 56 | 22 | 53 | 0 | 96 | 337 | 15 | 0 | 27 | 13 | 21 | 3874 | |
| 16:45 | 17:00 | 0 | 9 | 281 | 7 | 0 | 47 | 12 | 67 | 0 | 95 | 411 | 17 | 0 | 22 | 10 | 7 | 3949 | Peak |
| 17:00 | 17:15 | 1 | 9 | 295 | 3 | 0 | 55 | 20 | 73 | 0 | 97 | 355 | 21 | 0 | 30 | 25 | 18 | 3897 | |
| 17:15 | 17:30 | 0 | 10 | 300 | 10 | 0 | 58 | 27 | 66 | 0 | 111 | 334 | 17 | 0 | 29 | 20 | 6 | | |
| 17:30 | 17:45 | 0 | 8 | 303 | 12 | 0 | 53 | 20 | 58 | 0 | 85 | 373 | 15 | 0 | 14 | 19 | 14 | | |
| 17:45 | 18:00 | 0 | 12 | 270 | 14 | 0 | 48 | 19 | 64 | 0 | 107 | 334 | 22 | 0 | 18 | 14 | 11 | | |
| Peak Ti | Time | North | | | | East Approach Kenneth Rd | | | | | | | | | | | | | |

 Period Star
 Period End

 8:15
 9:15

 16:45
 17:45

 R
 SB

 21
 1138

 36
 1179
 R 228 213 WB 77 79 R 228 388 NB 1240 1473 L 39 70 R 90 95 EB 74 74 U 0 L total 23 3468 45 3949 U L 44 32 U L 264 264 U 0 1 1 1 0

Kenneth Rd





Intersection of Kenneth Rd and Roseberry St, Sydney

| GPS | -33.786730, 151.26794 | 44 | | | | | | |
|--------------|-----------------------|----|--------|--------------|---|---------|-----|------------------|
| Date: | Wed 05/03/25 | | North: | Roseberry St | | Survey | AM: | 6:00 AM-10:00 AM |
| Weather: | Overcast | | East: | Kenneth Rd | | Period | PM: | 2:00 PM-6:00 PM |
| Suburban: | Sydney | | South: | Roseberry St | | Traffic | AM: | 8:15 AM-9:15 AM |
| Customer: | McLaren | | West: | Kenneth Rd | | Peak | PM: | 5:00 PM-6:00 PM |
| | | | | | • | | | |
| All Vehicles | | | | | | | | |

| Time | | Mart | | - Deeska | | East Approach Kenneth Rd | | | | | | - Deseker | | 14/ | | Unud | Tetal | | |
|-------|------------------|-------|--------|----------|---------|--------------------------|-----------|-----------|----------|-----|-----------|-----------|----------|-----|----------|-----------|-------|----------|-----------------|
| | me Period End | U | R | h Rosebe | L L | U | R | WB | | U | R | h Roseber | L | U | t Approa | EB | | Hour | y Total Peak |
| 6:00 | 6:15 | 0 | 5 | 12 | 4 | 0 | 1 | 77 | 8 | 0 | 10 | 5 | 10 | 1 | 7 | 24 | 0 | 976 | I Can |
| 6:15 | 6:30 | 1 | 8 | 12 | 7 | 1 | 1 | 109 | 16 | 0 | 9 | 5 | 10 | 3 | 10 | 54 | 1 | 1113 | <u> </u> |
| | | | - | | 2 | | 5 | 96 | <u> </u> | - | - | - | <u> </u> | L | 6 | | 3 | <u> </u> | |
| 6:30 | 6:45 | 0 | 6 | 24 | L | 0 | | | 38 | 2 | 15 | 3 | 11 | 5 | | 56 | | 1170 | <u> </u> |
| 6:45 | 7:00 | 1 | 9 | 38 | 4 | 0 | 4 | 75 | 48 | 0 | 15 | 2 | 24 | 2 | 8 | 60 | 2 | 1223 | <u> </u> |
| 7:00 | 7:15 | 1 | 11 | 35 | 5 | 0 | 2 | 74 | 40 | 2 | 26 | 10 | 31 | 2 | 10 | 47 | 5 | 1282 | |
| 7:15 | 7:30 | 3 | 9 | 34 | 9 | 0 | 3 | 71 | 37 | 0 | 31 | 9 | 31 | 2 | 7 | 56 | 3 | 1316 | |
| 7:30 | 7:45 | 2 | 15 | 38 | 2 | 4 | 5 | 70 | 33 | 1 | 30 | 14 | 37 | 2 | 16 | 51 | 5 | 1364 | |
| 7:45 | 8:00 | 0 | 6 | 45 | 9 | 0 | 2 | 74 | 45 | 2 | 30 | 9 | 51 | 1 | 11 | 64 | 2 | 1451 | |
| 8:00 | 8:15 | 0 | 13 | 47 | 7 | 0 | 5 | 56 | 38 | 0 | 49 | 8 | 48 | 1 | 10 | 50 | 3 | 1519 | |
| 8:15 | 8:30 | 0 | 4 | 48 | 7 | 3 | 2 | 74 | 38 | 0 | 43 | 10 | 35 | 1 | 13 | 70 | 5 | 1597 | Peak |
| 8:30 | 8:45 | 0 | 20 | 59 | 6 | 2 | 4 | 80 | 50 | 0 | 56 | 16 | 45 | 4 | 8 | 55 | 7 | 1582 | |
| 8:45 | 9:00 | 0 | 21 | 65 | 6 | 0 | 2 | 73 | 51 | 2 | 46 | 14 | 53 | 2 | 12 | 63 | 9 | 1523 | |
| 9:00 | 9:15 | 0 | 13 | 42 | 10 | 1 | 3 | 102 | 43 | 0 | 42 | 13 | 48 | 6 | 21 | 59 | 10 | 1458 | |
| 9:15 | 9:30 | 2 | 8 | 28 | 5 | 3 | 3 | 79 | 30 | 1 | 40 | 13 | 42 | 0 | 16 | 63 | 5 | | |
| 9:30 | 9:45 | 0 | 7 | 32 | 6 | 1 | 4 | 84 | 40 | 0 | 46 | 14 | 53 | 3 | 15 | 45 | 3 | | |
| 9:45 | 10:00 | 0 | 5 | 29 | 8 | 4 | 2 | 62 | 36 | 1 | 45 | 11 | 50 | 2 | 19 | 77 | 3 | | |
| 14:00 | 14:15 | 1 | 9 | 26 | 4 | 0 | 1 | 65 | 35 | 1 | 37 | 14 | 48 | 2 | 19 | 45 | 8 | 1376 | |
| 14:15 | 14:30 | 0 | 9 | 22 | 2 | 3 | 2 | 71 | 46 | 1 | 40 | 14 | 64 | 1 | 13 | 50 | 10 | 1440 | |
| 14:30 | 14:45 | 0 | 10 | 20 | 7 | 0 | 2 | 67 | 43 | 0 | 31 | 10 | 66 | 4 | 9 | 75 | 9 | 1504 | |
| 14:45 | 15:00 | 0 | 15 | 38 | 3 | 2 | 0 | 84 | 27 | 1 | 38 | 12 | 59 | 2 | 13 | 59 | 7 | 1557 | |
| 15:00 | 15:15 | 0 | 10 | 32 | 2 | 0 | 1 | 73 | 32 | 0 | 60 | 21 | 46 | 0 | 12 | 82 | 8 | 1627 | |
| 15:15 | 15:30 | 0 | 10 | 43 | 4 | 2 | 3 | 97 | 39 | 1 | 41 | 14 | 54 | 1 | 12 | 81 | 10 | 1637 | |
| 15:30 | 15:45 | 0 | 7 | 33 | 7 | 1 | 2 | 66 | 36 | 1 | 56 | 20 | 60 | 2 | 21 | 85 | 9 | 1639 | |
| 15:45 | 16:00 | 0 | 13 | 36 | 8 | 0 | 4 | 74 | 37 | 3 | 42 | 16 | 60 | 6 | 26 | 94 | 11 | 1626 | |
| 16:00 | 16:15 | 1 | 9 | 39 | 3 | 2 | 1 | 58 | 29 | 2 | 50 | 16 | 56 | 5 | 17 | 93 | 8 | 1609 | |
| 16:15 | 16:30 | 0 | 12 | 49 | 5 | 0 | 3 | 70 | 40 | 1 | 48 | 18 | 49 | 2 | 16 | 86 | 15 | 1639 | |
| 16:30 | 16:45 | 1 | 12 | 37 | 5 | 2 | 2 | 57 | 29 | 0 | 54 | 16 | 50 | 6 | 25 | 91 | 6 | 1691 | |
| 16:45 | 17:00 | 0 | 10 | 54 | 5 | 0 | 1 | 71 | 37 | 0 | 59 | 14 | 45 | 5 | 13 | 89 | 10 | 1711 | |
| 17:00 | 17:15 | 0 | 15 | 39 | 9 | 1 | 5 | 78 | 35 | 0 | 47 | 14 | 44 | 6 | 13 | 103 | 10 | 1716 | Peak |
| 17:15 | 17:30 | 0 | 12 | 52 | 8 | 0 | 2 | 78 | 50 | 2 | 52 | 15 | 57 | 3 | 21 | 103 | 11 | | |
| 17:30 | 17:45 | 1 | 13 | 36 | 7 | 1 | 6 | 58 | 36 | 3 | 65 | 19 | 47 | 10 | 18 | 84 | 9 | | |
| 17:45 | 18:00 | 0 | 7 | 30 | 6 | 1 | 3 | 73 | 37 | 1 | 44 | 25 | 51 | 7 | 20 | 107 | 6 | | <u> </u> |
| 11.10 | 10.00 | ~ | | | Ť | | Ŭ | | | | | | | | | | Ň | | L |
| Peak | Time | North | Approa | h Rosebe | erry St | Eas | t Approad | ch Kennet | th Rd | Sou | th Approa | h Roseber | тySt | Wes | t Approa | ch Kennet | th Rd | Peak | 1 |

 Period Star
 Period End

 8:15
 9:15

 17:00
 18:00
 R 58 47 SB 214 157 R 11 16 WB 329 287 R 187 208 NB 53 73 U 13 26
 R
 EB

 54
 247

 72
 397
 L total 31 1597 36 1716 U L 29 30 U L 182 158 L 181 199 U 0 6 3 2 1 6





ANNEXURE B: SIDRA INTERSECTION PERFORMANCE RESULTS (8 SHEETS)

MOVEMENT SUMMARY

Site: 1 [(ExFridayPeakPM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Friday Peak Hour Period (3pm to 4pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 136 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|--------|--------------|-----------|-------------|---------------|---------------------------|---------------------|-----------------------|---------------------|-----------------------------|-------------------------|--------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | Aver. Back [Veh. veh | Of Queue Dist] m | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| South | n: Con | damine S | | | VOIIIII | 70 | 10 | 500 | | Volt | | | | | |
| 1 | L2 | All MCs | 88 | 0.0 | 88 | 0.0 | 0.192 | 30.1 | LOS C | 3.1 | 30.1 | 0.52 | 0.59 | 0.52 | 40.6 |
| 2 | T1 | All MCs | 1481 | 4.8 | 1481 | 4.8 | 0.717 | 29.8 | LOS C | 22.7 | 159.2 | 0.80 | 0.73 | 0.80 | 36.3 |
| 3 | R2 | All MCs | 402 | 1.6 | 402 | 1.6 | *0.690 | 28.8 | LOS C | 7.8 | 55.4 | 0.93 | 0.87 | 0.93 | 19.6 |
| Appro | bach | | 1972 | 4.0 | 1972 | 4.0 | 0.717 | 29.6 | LOS C | 22.7 | 159.2 | 0.81 | 0.75 | 0.81 | 31.4 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 389 | 1.6 | 389 | 1.6 | *0.482 | 43.9 | LOS D | 8.3 | 58.8 | 0.72 | 0.88 | 0.72 | 21.6 |
| 5 | T1 | All MCs | 68 | 0.0 | 68 | 0.0 | 0.191 | 72.2 | LOS F | 2.4 | 16.5 | 0.89 | 0.69 | 0.89 | 25.4 |
| 6 | R2 | All MCs | 226 | 5.6 | 226 | 5.6 | *0.996 | 131.0 | LOS F | 11.1 | 81.4 | 1.00 | 1.23 | 1.57 | 12.7 |
| Appro | bach | | 684 | 2.8 | 684 | 2.8 | 0.996 | 75.5 | LOS F | 11.1 | 81.4 | 0.83 | 0.98 | 1.02 | 14.3 |
| North | : Con | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 56 | 5.7 | 56 | 5.7 | 0.294 | 25.1 | LOS B | 3.6 | 38.7 | 0.76 | 0.68 | 0.76 | 28.0 |
| 8 | T1 | All MCs | 1188 | 7.4 | 1188 | 7.4 | *0.840 | 54.6 | LOS D | 22.3 | 156.1 | 0.97 | 0.92 | 1.03 | 26.5 |
| 9 | R2 | All MCs | 57 | 0.0 | 57 | 0.0 | 0.126 | 42.8 | LOS D | 1.0 | 6.8 | 0.78 | 0.72 | 0.78 | 39.5 |
| Appro | bach | | 1301 | 7.0 | 1301 | 7.0 | 0.840 | 52.8 | LOS D | 22.3 | 156.1 | 0.96 | 0.90 | 1.01 | 24.8 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 68 | 1.5 | 68 | 1.5 | 0.431 | 9.7 | LOS A | 5.7 | 40.1 | 0.93 | 0.78 | 0.93 | 29.4 |
| 11 | T1 | All MCs | 91 | 0.0 | 91 | 0.0 | * 0.431 | 90.0 | LOS F | 5.7 | 40.1 | 0.93 | 0.78 | 0.93 | 22.0 |
| 12 | R2 | All MCs | 136 | 2.3 | 136 | 2.3 | 0.802 | 64.2 | LOS E | 5.0 | 35.4 | 1.00 | 0.93 | 1.19 | 23.8 |
| Appro | bach | | 295 | 1.4 | 295 | 1.4 | 0.802 | 59.4 | LOS E | 5.7 | 40.1 | 0.96 | 0.85 | 1.05 | 24.8 |
| All Ve | hicles | ; | 4252 | 4.5 | 4252 | 4.5 | 0.996 | 46.2 | LOS D | 22.7 | 159.2 | 0.87 | 0.84 | 0.92 | 25.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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V Site: 2 [(ExFridayPeakPM) Kenneth Road / Roseberry Street (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

■ Network: N101 [Exising Friday PM Peak Hour Period (Network Folder: General)]

Existing Friday Peak Hour Period (3pm to 4pm) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Vehi | cle M | ovement | t Perfo | orma | nce | | | | | | | | | | |
|--------|--------|------------|---------------|-------------|-------|-------------|-------|-------|----------|------------|----------|------|--------------|------------------|-------|
| Mov | Turn | Mov | | nand | | rival | Deg. | Aver. | Level of | Aver. Back | Of Queue | | Eff. | Aver. | Aver. |
| ID | | Class | Fi [Total | ows HV 1 | | ows HV 1 | Satn | Delay | Service | [Veh. | Dist] | Que | Stop Rate | No. of Cycles | Speed |
| | | | veh/h | | veh/h | % | v/c | sec | | veh | m | | | _ , | km/h |
| South | : Ros | eberry Str | reet (S) | | | | | | | | | | | | |
| 1 | L2 | All MCs | 216 | 0.0 | 216 | 0.0 | 0.860 | 18.8 | LOS B | 4.6 | 32.2 | 1.00 | 1.11 | 1.62 | 33.3 |
| 2 | T1 | All MCs | 84 | 0.0 | 84 | 0.0 | 0.860 | 18.9 | LOS B | 4.6 | 32.2 | 1.00 | 1.11 | 1.62 | 35.7 |
| 3 | R2 | All MCs | 220 | 0.0 | 220 | 0.0 | 0.860 | 22.1 | LOS B | 4.6 | 32.2 | 1.00 | 1.11 | 1.62 | 36.5 |
| 3u | U | All MCs | 3 | 0.0 | 3 | 0.0 | 0.860 | 23.7 | LOS B | 4.6 | 32.2 | 1.00 | 1.11 | 1.62 | 40.8 |
| Appro | ach | | 523 | 0.0 | 523 | 0.0 | 0.860 | 20.2 | LOS B | 4.6 | 32.2 | 1.00 | 1.11 | 1.62 | 35.3 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 169 | 0.0 | 169 | 0.0 | 0.903 | 18.2 | LOS B | 5.6 | 39.9 | 1.00 | 1.11 | 1.58 | 37.9 |
| 5 | T1 | All MCs | 393 | 2.9 | 393 | 2.9 | 0.903 | 18.4 | LOS B | 5.6 | 39.9 | 1.00 | 1.11 | 1.58 | 23.5 |
| 6 | R2 | All MCs | 7 | 0.0 | 7 | 0.0 | 0.903 | 21.4 | LOS B | 5.6 | 39.9 | 1.00 | 1.11 | 1.58 | 28.5 |
| 6u | U | All MCs | 8 | 0.0 | 8 | 0.0 | 0.903 | 23.0 | LOS B | 5.6 | 39.9 | 1.00 | 1.11 | 1.58 | 30.9 |
| Appro | ach | | 578 | 2.0 | 578 | 2.0 | 0.903 | 18.5 | LOS B | 5.6 | 39.9 | 1.00 | 1.11 | 1.58 | 29.9 |
| North | : Rose | eberry Str | eet (N) | | | | | | | | | | | | |
| 7 | L2 | All MCs | 22 | 9.5 | 22 | 9.5 | 0.466 | 13.3 | LOSA | 1.5 | 10.7 | 0.92 | 0.77 | 1.01 | 32.0 |
| 8 | T1 | All MCs | 186 | 0.6 | 186 | 0.6 | 0.466 | 12.9 | LOSA | 1.5 | 10.7 | 0.92 | 0.77 | 1.01 | 40.6 |
| 9 | R2 | All MCs | 61 | 3.4 | 61 | 3.4 | 0.466 | 16.2 | LOS B | 1.5 | 10.7 | 0.92 | 0.77 | 1.01 | 23.5 |
| 9u | U | All MCs | 4 | 0.0 | 4 | 0.0 | 0.466 | 17.6 | LOS B | 1.5 | 10.7 | 0.92 | 0.77 | 1.01 | 25.6 |
| Appro | ach | | 274 | 1.9 | 274 | 1.9 | 0.466 | 13.7 | LOS A | 1.5 | 10.7 | 0.92 | 0.77 | 1.01 | 37.7 |
| West | Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 42 | 2.5 | 42 | 2.5 | 0.602 | 8.2 | LOS A | 2.0 | 14.3 | 0.55 | 0.71 | 0.60 | 33.4 |
| 11 | T1 | All MCs | 422 | 1.2 | 422 | 1.2 | 0.602 | 8.1 | LOS A | 2.0 | 14.3 | 0.55 | 0.71 | 0.60 | 37.2 |
| 12 | R2 | All MCs | 72 | 4.4 | 72 | 4.4 | 0.602 | 11.5 | LOS A | 2.0 | 14.3 | 0.55 | 0.71 | 0.60 | 43.3 |
| 12u | U | All MCs | 13 | 0.0 | 13 | 0.0 | 0.602 | 13.0 | LOS A | 2.0 | 14.3 | 0.55 | 0.71 | 0.60 | 26.1 |
| Appro | ach | | 548 | 1.7 | 548 | 1.7 | 0.602 | 8.7 | LOS A | 2.0 | 14.3 | 0.55 | 0.71 | 0.60 | 37.9 |
| All Ve | hicles | i. | 1923 | 1.4 | 1923 | 1.4 | 0.903 | 15.5 | LOS B | 5.6 | 39.9 | 0.86 | 0.95 | 1.23 | 34.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Site: 1 [(ExSaturdayPeakPM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Saturday Peak Hour Period (12pm to 1pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 134 seconds (Site User-Given Phase Times)

| Vehi | cle M | ovement | Perfo | orma | nce | | | | | | | | | | |
|-----------|------------|--------------|---------|-------------|---------------|---------------------------|---------------------|-----------------------|---------------------|-----------------------------|-------------------------|----------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | Aver. Back [Veh. veh | Of Queue Dist] m | e Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| Sout | h: Con | damine S | | _ | VGIIIII | 70 | VIC | 300 | | VCIT | | _ | _ | _ | KI1/11 |
| 1 | L2 | All MCs | 72 | 1.5 | 72 | 1.5 | 0.117 | 27.3 | LOS B | 1.9 | 16.9 | 0.48 | 0.60 | 0.48 | 41.0 |
| 2 | T1 | All MCs | 1347 | 2.5 | 1347 | 2.5 | 0.648 | 27.3 | LOS B | 19.1 | 133.4 | 0.75 | 0.69 | 0.75 | 37.3 |
| 3 | R 2 | All MCs | 389 | 0.8 | 389 | 0.8 | *0.715 | 30.1 | LOS C | 8.2 | 57.5 | 0.95 | 0.88 | 0.95 | 19.0 |
| Appr | oach | | 1808 | 2.1 | 1808 | 2.1 | 0.715 | 27.9 | LOS B | 19.1 | 133.4 | 0.79 | 0.73 | 0.79 | 32.1 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 356 | 0.9 | 356 | 0.9 | *0.468 | 46.5 | LOS D | 7.9 | 55.8 | 0.76 | 0.89 | 0.76 | 20.6 |
| 5 | T1 | All MCs | 51 | 2.1 | 51 | 2.1 | 0.176 | 77.7 | LOS F | 1.8 | 12.7 | 0.91 | 0.69 | 0.91 | 24.4 |
| 6 | R2 | All MCs | 247 | 0.9 | 247 | 0.9 | *0.940 | 108.7 | LOS F | 10.7 | 75.6 | 1.00 | 1.15 | 1.39 | 15.3 |
| Appr | oach | | 654 | 1.0 | 654 | 1.0 | 0.940 | 72.4 | LOS F | 10.7 | 75.6 | 0.86 | 0.98 | 1.01 | 14.8 |
| North | : Con | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 67 | 0.0 | 67 | 0.0 | 0.137 | 21.2 | LOS B | 1.9 | 16.0 | 0.65 | 0.67 | 0.65 | 31.1 |
| 8 | T1 | All MCs | 1281 | 1.9 | 1281 | 1.9 | * 0.868 | 56.1 | LOS D | 25.7 | 179.9 | 0.99 | 0.96 | 1.08 | 26.4 |
| 9 | R2 | All MCs | 49 | 0.0 | 49 | 0.0 | 0.095 | 41.8 | LOS C | 0.8 | 5.7 | 0.73 | 0.71 | 0.73 | 40.7 |
| Appr | oach | | 1398 | 1.7 | 1398 | 1.7 | 0.868 | 53.9 | LOS D | 25.7 | 179.9 | 0.96 | 0.94 | 1.04 | 24.4 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 63 | 0.0 | 63 | 0.0 | 0.313 | 10.1 | LOS A | 3.6 | 25.1 | 0.91 | 0.76 | 0.91 | 29.1 |
| 11 | T1 | All MCs | 39 | 0.0 | 39 | 0.0 | *0.313 | 132.5 | LOS F | 3.6 | 25.1 | 0.91 | 0.76 | 0.91 | 21.6 |
| 12 | R2 | All MCs | 114 | 1.9 | 114 | 1.9 | 0.605 | 54.1 | LOS D | 3.9 | 27.9 | 1.00 | 0.79 | 1.01 | 26.2 |
| Appr | oach | | 216 | 1.0 | 216 | 1.0 | 0.605 | 55.4 | LOS D | 3.9 | 27.9 | 0.96 | 0.77 | 0.96 | 26.4 |
| All Ve | hicles | ; | 4076 | 1.7 | 4076 | 1.7 | 0.940 | 45.4 | LOS D | 25.7 | 179.9 | 0.87 | 0.84 | 0.92 | 25.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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V Site: 2 [(ExSaturdayPeakPM) Kenneth Road / Roseberry Street (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Saturday Peak Hour Period (12pm to 1pm) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Vehi | cle M | ovement | Performa | ance | | | | | | | | | |
|--------|--------|-------------|-----------------------|-----------------------|-------|-------|----------|------------|----------|------|--------------|------------------|-------|
| Mov | Turn | Mov | Demand | | Deg. | Aver. | Level of | Aver. Back | Of Queue | | Eff. | Aver. | Aver. |
| ID | | Class | Flows [Total HV] | Flows [Total HV] | Satn | Delay | Service | [Veh. | Dist] | Que | Stop Rate | No. of Cycles | Speed |
| | | | | veh/h % | v/c | sec | | veh | m | | Tuto | Cycles | km/h |
| South | : Rose | eberry Str | eet (S) | | | | | | | | | | |
| 1 | L2 | All MCs | 263 0.8 | 263 0.8 | 0.836 | 16.2 | LOS B | 4.5 | 31.4 | 1.00 | 1.01 | 1.48 | 35.4 |
| 2 | T1 | All MCs | 92 0.0 | 92 0.0 | 0.836 | 16.3 | LOS B | 4.5 | 31.4 | 1.00 | 1.01 | 1.48 | 37.7 |
| 3 | R2 | All MCs | 201 0.5 | 201 0.5 | 0.836 | 19.4 | LOS B | 4.5 | 31.4 | 1.00 | 1.01 | 1.48 | 38.3 |
| 3u | U | All MCs | 7 0.0 | 7 0.0 | 0.836 | 21.0 | LOS B | 4.5 | 31.4 | 1.00 | 1.01 | 1.48 | 42.4 |
| Appro | bach | | 563 0.6 | 563 0.6 | 0.836 | 17.4 | LOS B | 4.5 | 31.4 | 1.00 | 1.01 | 1.48 | 37.1 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | |
| 4 | L2 | All MCs | 220 0.5 | 220 0.5 | 0.859 | 18.2 | LOS B | 4.9 | 34.4 | 1.00 | 1.07 | 1.59 | 37.9 |
| 5 | T1 | All MCs | 337 0.6 | 337 0.6 | 0.859 | 18.4 | LOS B | 4.9 | 34.4 | 1.00 | 1.07 | 1.59 | 23.5 |
| 6 | R2 | All MCs | 15 0.0 | 15 0.0 | 0.859 | 21.4 | LOS B | 4.9 | 34.4 | 1.00 | 1.07 | 1.59 | 28.5 |
| 6u | U | All MCs | 1 0.0 | 1 0.0 | 0.859 | 23.1 | LOS B | 4.9 | 34.4 | 1.00 | 1.07 | 1.59 | 30.9 |
| Appro | ach | | 573 0 .6 | 573 0.6 | 0.859 | 18.4 | LOS B | 4.9 | 34.4 | 1.00 | 1.07 | 1.59 | 31.3 |
| North | : Rose | eberry Stre | eet (N) | | | | | | | | | | |
| 7 | L2 | All MCs | 22 0.0 | 22 0.0 | 0.428 | 13.1 | LOSA | 1.3 | 9.2 | 0.93 | 0.79 | 1.01 | 32.6 |
| 8 | T1 | All MCs | 156 0.0 | 156 0.0 | 0.428 | 13.2 | LOS A | 1.3 | 9.2 | 0.93 | 0.79 | 1.01 | 40.4 |
| 9 | R2 | All MCs | 47 2.2 | 47 2.2 | 0.428 | 16.5 | LOS B | 1.3 | 9.2 | 0.93 | 0.79 | 1.01 | 23.2 |
| 9u | U | All MCs | 2 0.0 | 2 0.0 | 0.428 | 18.0 | LOS B | 1.3 | 9.2 | 0.93 | 0.79 | 1.01 | 25.4 |
| Appro | bach | | 227 0.5 | 227 0.5 | 0.428 | 13.9 | LOSA | 1.3 | 9.2 | 0.93 | 0.79 | 1.01 | 37.7 |
| West | Kenn | eth Road | (W) | | | | | | | | | | |
| 10 | L2 | All MCs | 53 50.0 | 53 50.0 | 0.755 | 12.3 | LOSA | 3.5 | 28.4 | 0.70 | 0.85 | 0.88 | 26.9 |
| 11 | T1 | All MCs | 380 0.8 | 380 0.8 | 0.755 | 10.6 | LOS A | 3.5 | 28.4 | 0.70 | 0.85 | 0.88 | 33.4 |
| 12 | R2 | All MCs | 166 50.0 | 166 50.0 | 0.755 | 15.6 | LOS B | 3.5 | 28.4 | 0.70 | 0.85 | 0.88 | 38.0 |
| 12u | U | All MCs | 23 50.0 | 23 50.0 | 0.755 | 17.2 | LOS B | 3.5 | 28.4 | 0.70 | 0.85 | 0.88 | 21.6 |
| Appro | ach | | 622 20.0 | 622 20.0 | 0.755 | 12.3 | LOSA | 3.5 | 28.4 | 0.70 | 0.85 | 0.88 | 34.4 |
| All Ve | hicles | | 1985 6.6 | 1985 6.6 | 0.859 | 15.7 | LOS B | 4.9 | 34.4 | 0.90 | 0.95 | 1.27 | 34.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Site: 1 [(ExWednesdayPeakAM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Wednesday AM Peak Hour Period (8:15am to 9:15am) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Phase Times)

| Vehi | cle M | ovement | t Perfo | orma | nce | | | | | | | | | | |
|-----------|--------|--------------|----------|-------------|-----------------|---------------------------|---------------------|-----------------------|---------------------|-----------------------------|-------------------------|--------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | | ows HV] | Fl [Total] | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | Aver. Back [Veh. veh | Of Queue Dist] m | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| South | n: Con | damine S | treet (S | ;) | | | | | | | | | | | |
| 1 | L2 | All MCs | 41 | 0.0 | 41 | 0.0 | 0.192 | 21.4 | LOS B | 2.5 | 28.1 | 0.53 | 0.52 | 0.53 | 42.3 |
| 2 | T1 | All MCs | 1305 | 7.7 | 1305 | 7.7 | 0.593 | 21.7 | LOS B | 15.0 | 105.0 | 0.71 | 0.64 | 0.71 | 39.8 |
| 3 | R2 | All MCs | 240 | 2.2 | 240 | 2.2 | *0.454 | 21.9 | LOS B | 3.6 | 25.8 | 0.82 | 0.80 | 0.82 | 23.3 |
| Appro | bach | | 1586 | 6.7 | 1586 | 6.7 | 0.593 | 21.7 | LOS B | 15.0 | 105.0 | 0.72 | 0.66 | 0.72 | 36.6 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 278 | 3.8 | 278 | 3.8 | *0.393 | 40.0 | LOS C | 6.3 | 45.9 | 0.73 | 0.85 | 0.73 | 19.8 |
| 5 | T1 | All MCs | 81 | 1.3 | 81 | 1.3 | 0.240 | 62.4 | LOS E | 2.5 | 17.9 | 0.90 | 0.70 | 0.90 | 26.7 |
| 6 | R2 | All MCs | 240 | 3.9 | 240 | 3.9 | 0.768 | 70.6 | LOS F | 7.7 | 55.4 | 0.99 | 0.99 | 1.10 | 20.7 |
| Appro | bach | | 599 | 3.5 | 599 | 3.5 | 0.768 | 55.3 | LOS D | 7.7 | 55.4 | 0.86 | 0.89 | 0.90 | 18.5 |
| North | : Cond | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 46 | 4.5 | 46 | 4.5 | *0.300 | 22.2 | LOS B | 3.4 | 38.0 | 0.74 | 0.66 | 0.74 | 29.7 |
| 8 | T1 | All MCs | 1198 | 8.6 | 1198 | 8.6 | *0.772 | 40.7 | LOS C | 17.6 | 123.4 | 0.93 | 0.84 | 0.94 | 30.5 |
| 9 | R2 | All MCs | 22 | 0.0 | 22 | 0.0 | 0.039 | 30.9 | LOS C | 0.3 | 2.3 | 0.67 | 0.67 | 0.67 | 42.5 |
| Appro | bach | | 1266 | 8.3 | 1266 | 8.3 | 0.772 | 39.9 | LOS C | 17.6 | 123.4 | 0.92 | 0.83 | 0.93 | 28.8 |
| West | Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 24 | 4.3 | 24 | 4.3 | 0.297 | 9.8 | LOS A | 3.2 | 22.6 | 0.91 | 0.73 | 0.91 | 31.3 |
| 11 | T1 | All MCs | 78 | 0.0 | 78 | 0.0 | *0.297 | 60.0 | LOS E | 3.2 | 22.6 | 0.91 | 0.73 | 0.91 | 24.0 |
| 12 | R2 | All MCs | 95 | 1.1 | 95 | 1.1 | 0.411 | 44.4 | LOS D | 2.7 | 19.3 | 0.95 | 0.76 | 0.95 | 29.0 |
| Appro | bach | | 197 | 1.1 | 197 | 1.1 | 0.411 | 46.3 | LOS D | 3.2 | 22.6 | 0.93 | 0.75 | 0.93 | 27.6 |
| All Ve | hicles | | 3648 | 6.4 | 3648 | 6.4 | 0.772 | 34.9 | LOS C | 17.6 | 123.4 | 0.82 | 0.76 | 0.83 | 29.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

SIDRA INTERSECTION 9.1 | Copyright © 2000-2024 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Monday, 10 March 2025 7:29:48 PM Project: Z:\Jobs\2025\250154\MTE SIDRA\25 03 07 - SI SIDRA.sip9

V Site: 2 [(ExWednesdayPeakAM) Kenneth Road / Roseberry Street (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Network: N101 [Existing Wednesday AM Peak Hour Period (Network Folder: General)]

Existing Wednesday AM Peak Hour Period (8:15am to 9:15am) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Mov ID Turn Mov Class Demand Flows Tedatty I [Total HV] veh/h Sand Aver Delay Service Service Aver. Aver Weh Back Of Queue Weh Prop Delay Eff Service Aver. Service Service Weh Service Tedatty Service Veh Service Weh Aver. Tedatty Service Veh Service Weh Aver. Weh Service Weh Service Wei Service Wei <th>Vehic</th> <th>cle M</th> <th>ovemen</th> <th>t Perfo</th> <th>orma</th> <th>nce</th> <th></th> | Vehic | cle M | ovemen | t Perfo | orma | nce | | | | | | | | | | |
|--|--------|--------|------------|---------|---------------|------|---------------|-------|-------|---------|------------|----------|------|------|--------|-------|
| [Voh. Dist] Rate Cycles km/h South: Roseberry Street (S) 1 L2 All MCs 191 2.8 0.557 9.7 LOSA 1.9 13.9 0.81 0.76 0.92 41.6 2 T1 All MCs 197 3.7 197 3.7 0.557 9.6 LOSA 1.9 13.9 0.81 0.76 0.92 42.9 3 R2 All MCs 197 3.7 197 3.7 0.557 17.0 LOSA 1.9 13.9 0.81 0.76 0.92 42.8 3u U All MCs 145 3.1 0.557 11.2 LOSA 1.9 13.9 0.81 0.76 0.92 42.4 All MCs 164 0 46.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 33.0 6 R2 All MCs 12 0.0 0.629 9.7 <td></td> <td>Turn</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Aver. Back</td> <td>Of Queue</td> <td></td> <td></td> <td></td> <td></td> | | Turn | | | | | | | | | Aver. Back | Of Queue | | | | |
| Veh/n % v/c sec veh m km/h South: Roseberry Street (S) | ID | | Class | | | | | Satn | Delay | Service | [\/ob | Dist 1 | Que | | | Speed |
| South: Roseberry Street (S) 1 L2 All MCs 191 2.8 191 2.8 0.557 9.7 LOS A 1.9 13.9 0.81 0.76 0.92 41.6 2 T1 All MCs 56 0.0 56 0.0 0.557 9.6 LOS A 1.9 13.9 0.81 0.76 0.92 42.9 3u U All MCs 157.0 250.0 250.0 0.557 17.0 LOS B 1.9 13.9 0.81 0.76 0.92 44.6 Approach 445 3.1 0.57 17.0 LOS B 1.9 13.9 0.81 0.76 0.92 44.6 Approach 455.1 453.1 0.57 17.0 LOS A 1.9 13.9 0.81 0.76 0.92 44.7 5 T1 All MCs 346.4.0 0.629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 30.0 6 R2 All MCs 6 0.0 6.029 12.6 LOS A | | | | | | | | v/c | sec | | | | | Rate | Cycles | km/h |
| 2 T1 All MCs 56 0.0 55 9.6 LOSA 1.9 13.9 0.81 0.76 0.92 42.9 3 R2 All MCs 197 3.7 197 3.7 0.557 13.0 LOSA 1.9 13.9 0.81 0.76 0.92 42.8 3u U All MCs 250.0 250.0 0.557 17.0 LOS B 1.9 13.9 0.81 0.76 0.92 42.8 Approach 445 3.1 0.557 11.2 LOS A 1.9 13.9 0.81 0.76 0.92 42.4 East: Kenneth Road (E 192 1.0 0.557 11.2 LOS A 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCs 192 0.1 0.629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 36.5 6u U All MCs 12 0.0 0.629 142 LOS A 2.5 18.1 0.82 0.72 0.93 <td>South</td> <td>: Ros</td> <td>eberry St</td> <td></td> | South | : Ros | eberry St | | | | | | | | | | | | | |
| 3 R2 All MCs 197 3.7 197 3.7 0.557 13.0 LOS A 1.9 13.9 0.81 0.76 0.92 42.8 3u U All MCs 250.0 250.0 0.557 17.0 LOS B 1.9 13.9 0.81 0.76 0.92 42.8 Approach 445 3.1 445 3.1 0.557 11.2 LOS A 1.9 13.9 0.81 0.76 0.92 42.4 East: Kenneth Road (E 4 L2 All MCs 192 1.1 0.629 9.4 LOS A 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCs 346 4.0 0.629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 36.3 6u U All MCs 12 0.0 1629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 38.5 Approach 56 2.8 56 2.8 0.629 9.7 | 1 | L2 | All MCs | 191 | 2.8 | 191 | 2.8 | 0.557 | 9.7 | LOS A | 1.9 | 13.9 | 0.81 | 0.76 | 0.92 | 41.6 |
| 3u U All MCS 2500 2500 0.557 17.0 LOS B 1.9 13.9 0.81 0.76 0.92 44.6 Approach 445 3.1 0.557 11.2 LOS A 1.9 13.9 0.81 0.76 0.92 42.4 East: Kenneth Road (E) 11 192 1.1 0.629 9.4 LOS A 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCS 346 4.0 0.629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 38.5 6u V All MCS 12 0.0 0.629 1.42 LOS A 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 0.629 9.7 LOS A 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 0.629 9.7 LOS A 1.5 18.1 0.82 0.72 0.93 38.5 Approx Noth: | 2 | T1 | All MCs | 56 | 0.0 | 56 | 0.0 | 0.557 | 9.6 | LOS A | 1.9 | 13.9 | 0.81 | 0.76 | 0.92 | 42.9 |
| Approach 445 3.1 445 3.1 0.557 11.2 LOSA 1.9 13.9 0.81 0.76 0.92 42.4 East: Kenneth Road (F) 4 L2 All MCS 192 1.1 192 1.1 0.629 9.4 LOSA 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCS 346 4.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 343.0 6 R2 All MCS 12 0.0 0.629 14.2 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 0.629 9.7 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 | 3 | R2 | All MCs | 197 | 3.7 | 197 | 3.7 | 0.557 | 13.0 | LOS A | 1.9 | 13.9 | 0.81 | 0.76 | 0.92 | 42.8 |
| East: Kenneth Road (E) 4 L2 All MCs 192 1.1 192 1.1 0.629 9.4 LOSA 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCs 346 4.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 33.0 6 R2 All MCs 12 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 566 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 566 2.8 0.629 9.7 LOSA 1.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 0.629 9.7 LOSA 1.2 | 3u | U | All MCs | 2 | 5 0 .0 | 2 | 5 0 .0 | 0.557 | 17.0 | LOS B | 1.9 | 13.9 | 0.81 | 0.76 | 0.92 | 44.6 |
| 4 L2 All MCs 192 1.1 192 1.1 0.629 9.4 LOSA 2.5 18.1 0.82 0.72 0.93 44.7 5 T1 All MCs 346 4.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 33.0 6 R2 All MCs 12 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 36.3 6u U All MCs 6 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Roseberry Street (N) 7 L2 All MCs 3110.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 255 1.4 0.394 9.2 LOSA 1.2 8.3 | Appro | ach | | 445 | 3.1 | 445 | 3.1 | 0.557 | 11.2 | LOS A | 1.9 | 13.9 | 0.81 | 0.76 | 0.92 | 42.4 |
| 5 T1 All MCs 346 4.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 33.0 6 R2 All MCs 12 0.0 12 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 36.3 6u U All MCs 6 0.0 6 0.0 0.629 14.2 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Foresterer Street N 7 L2 All MCs 31 0.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 3.4 61 3.4 0.394 9.2 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 | East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 5 T1 All MCs 346 4.0 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 33.0 6 R2 All MCs 12 0.0 12 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 36.3 6u U All MCs 6 0.0 6.00 0.629 14.2 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approx 556 2.8 566 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Foreverstreets 7 L2 All MCs 31 10.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 3.4 61 3.4 0.394 9.2 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1.94 9.8 | 4 | L2 | All MCs | 192 | 1.1 | 192 | 1.1 | 0.629 | 9.4 | LOSA | 2.5 | 18.1 | 0.82 | 0.72 | 0.93 | 44.7 |
| 6 R2 All MCs 12 0.0 12 0.0 0.629 12.6 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 38.5 Approach 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Roseberry Street (N) 7 L2 All MCs 3110.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 61 3.4 0.394 9.2 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 61 3.4 0.394 12.4 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 <td< td=""><td>5</td><td>T1</td><td>All MCs</td><td>346</td><td>4.0</td><td>346</td><td>4.0</td><td>0.629</td><td>9.7</td><td>LOSA</td><td></td><td>18.1</td><td>0.82</td><td>0.72</td><td>0.93</td><td>33.0</td></td<> | 5 | T1 | All MCs | 346 | 4.0 | 346 | 4.0 | 0.629 | 9.7 | LOSA | | 18.1 | 0.82 | 0.72 | 0.93 | 33.0 |
| Approach 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Roseberry Street (N) 7 L2 All MCs 31 10.3 31 10.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 225 1.4 225 1.4 0.394 9.2 LOSA 1.2 8.3 0.75 0.67 0.75 44.1 9 R2 All MCs 61 3.4 61 3.4 0.394 12.4 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1.39 1.38 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 0.394 9.8 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 0.394 9.8 LOSA 0.9 | 6 | R2 | All MCs | | | 12 | 0.0 | 0.629 | 12.6 | LOSA | 2.5 | 18.1 | 0.82 | 0.72 | 0.93 | 36.3 |
| Approach 556 2.8 556 2.8 0.629 9.7 LOSA 2.5 18.1 0.82 0.72 0.93 39.4 North: Roseberry Street (N) 7 L2 All MCs 31 10.3 31 10.3 0.394 9.5 LOSA 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 225 1.4 225 1.4 0.394 9.2 LOSA 1.2 8.3 0.75 0.67 0.75 44.1 9 R2 All MCs 61 3.4 61 3.4 0.394 12.4 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1.39 1.38 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 0.394 9.8 LOSA 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 0.394 9.8 LOSA 0.9 | 6u | U | All MCs | 6 | 0.0 | 6 | 0.0 | 0.629 | 14.2 | LOSA | 2.5 | 18.1 | 0.82 | 0.72 | 0.93 | 38.5 |
| 7 L2 All MCs 31 10.3 31 10.3 0.394 9.5 LOS A 1.2 8.3 0.75 0.67 0.75 35.7 8 T1 All MCs 225 1.4 225 1.4 0.394 9.2 LOS A 1.2 8.3 0.75 0.67 0.75 44.1 9 R2 All MCs 61 3.4 61 3.4 0.394 12.4 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1.30 0.394 13.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 41.9 West: Kenneth Road (W) 11 11 All MCs 33 0.0 0.375 6.7 LOS A | Appro | ach | | | | 556 | 2.8 | 0.629 | | | | 18.1 | | 0.72 | | |
| 8 T1 All MCs 225 1.4 225 1.4 0.394 9.2 LOS A 1.2 8.3 0.75 0.67 0.75 44.1 9 R2 All MCs 61 3.4 61 3.4 0.394 12.4 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1 0.0 0.394 13.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Most Xerneth Road Xiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii | North | Rose | eberry Str | eet (N) | | | | | | | | | | | | |
| 8 T1 All MCs 225 1.4 225 1.4 0.394 9.2 LOS A 1.2 8.3 0.75 0.67 0.75 24.1 9 R2 All MCs 61 3.4 61 3.4 0.394 12.4 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 9u U All MCs 1 0.0 1 0.0 0.394 13.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 41.9 West: Kenneth Road (W) 10 L2 All MCs 33 0.0 33 0.0 0.375 6.6 LOS A 0.9 6.5 0.43 0.63 0.43 35.3 11 T1 | 7 | L2 | All MCs | 31 | 10.3 | 31 | 10.3 | 0.394 | 9.5 | LOSA | 1.2 | 8.3 | 0.75 | 0.67 | 0.75 | 35.7 |
| 9u U All MCs 1 0.0 1 0.0 0.394 13.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 West: Kenneth Road (W) 10 L2 All MCs 33 0.0 0.375 6.6 LOS A 0.9 6.5 0.43 0.63 0.43 35.3 11 T1 All MCs 260 2.4 0.375 6.7 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12u U All MCs 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.37 | 8 | T1 | All MCs | 225 | 1.4 | 225 | 1.4 | 0.394 | 9.2 | LOSA | | 8.3 | 0.75 | 0.67 | 0.75 | 44.1 |
| 9u U All MCs 1 0.0 1 0.0 0.394 13.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 Approach 318 2.6 318 2.6 0.394 9.8 LOS A 1.2 8.3 0.75 0.67 0.75 28.4 West: Kenneth Road (W) 10 L2 All MCs 33 0.0 0.375 6.6 LOS A 0.9 6.5 0.43 0.63 0.43 35.3 11 T1 All MCs 260 2.4 0.375 6.7 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12u U All MCs 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.37 | 9 | R2 | All MCs | 61 | 3.4 | 61 | 3.4 | 0.394 | 12.4 | LOSA | 1.2 | 8.3 | 0.75 | 0.67 | 0.75 | 28.4 |
| West: Kenneth Road (W) 10 L2 All MCs 33 0.0 33 0.0 0.375 6.6 LOS A 0.9 6.5 0.43 0.63 0.43 35.3 11 T1 All MCs 260 2.4 260 2.4 0.375 6.7 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 44.7 12u U All MCs 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 39.6 | 9u | U | All MCs | 1 | 0.0 | 1 | 0.0 | | 13.8 | LOSA | | 8.3 | 0.75 | 0.67 | | 28.4 |
| 10 L2 All MCs 33 0.0 33 0.0 0.375 6.6 LOS A 0.9 6.5 0.43 0.63 0.43 35.3 11 T1 All MCs 260 2.4 260 2.4 0.375 6.7 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 44.7 12u U All MCs 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 39.6 | Appro | ach | | 318 | 2.6 | 318 | 2.6 | 0.394 | 9.8 | LOS A | 1.2 | 8.3 | 0.75 | 0.67 | 0.75 | 41.9 |
| 11 T1 All MCs 260 2.4 260 2.4 0.375 6.7 LOS A 0.9 6.5 0.43 0.63 0.43 38.7 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 44.7 12u U All MCs 14 0.0 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 | West: | Kenn | eth Road | I (W) | | | | | | | | | | | | |
| 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 44.7 12u U All MCs 14 0.0 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 | 10 | L2 | All MCs | 33 | 0.0 | 33 | 0.0 | 0.375 | 6.6 | LOSA | 0.9 | 6.5 | 0.43 | 0.63 | 0.43 | 35.3 |
| 12 R2 All MCs 57 1.9 57 1.9 0.375 9.9 LOS A 0.9 6.5 0.43 0.63 0.43 44.7 12u U All MCs 14 0.0 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 | 11 | T1 | All MCs | 260 | 2.4 | 260 | 2.4 | 0.375 | 6.7 | LOSA | 0.9 | 6.5 | 0.43 | 0.63 | 0.43 | 38.7 |
| 12u U All MCs 14 0.0 14 0.0 0.375 11.5 LOS A 0.9 6.5 0.43 0.63 0.43 28.4 Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 39.6 | | | | | | | | | | | | | | | | |
| Approach 363 2.0 363 2.0 0.375 7.4 LOS A 0.9 6.5 0.43 0.63 0.43 39.6 | | | | | | | | | | | | | | | | |
| All Vehicles 1682 2.7 1682 2.7 0.629 9.6 LOS A 2.5 18.1 0.72 0.70 0.78 40.9 | | | | | | | | | | | | | | | | |
| | All Ve | hicles | | 1682 | 2.7 | 1682 | 2.7 | 0.629 | 9.6 | LOSA | 2.5 | 18.1 | 0.72 | 0.70 | 0.78 | 40.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Site: 1 [(ExWednesdayPeakPM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Wednesday PM Peak Hour Period (4:45pm to 5:45pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 139 seconds (Site User-Given Phase Times)

| Vehi | cle M | ovement | Perfo | orma | nce | | | | | | | | | | |
|-----------|--------|--------------|---------------------------------|-------------|---------------|-----|---------------------|----------------|---------------------|-----------------------------|--------|----------------|----------------------|---------------------------|----------------|
| Mov ID | Turn | Mov Class | Dem Fl [Total] veh/h | ows HV] | Fl Total | | Deg. Satn v/c | Aver. Delay | Level of Service | Aver. Back [Veh. veh | Dist] | e Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
| South | n: Con | damine St | | | ven/m | % | V/C | Sec | _ | ven | m | _ | _ | _ | km/h |
| 1 | L2 | All MCs | 41 | 0.0 | 41 | 0.0 | 0.199 | 26.6 | LOS B | 3.0 | 33.8 | 0.55 | 0.54 | 0.55 | 40.0 |
| 2 | T1 | All MCs | 1305 | 7.7 | 1305 | 7.7 | 0.623 | 28.4 | LOS B | 18.5 | 129.4 | 0.74 | 0.67 | 0.74 | 36.6 |
| 3 | R2 | All MCs | 240 | 2.2 | 240 | 2.2 | * 0.438 | 25.0 | LOS B | 4.1 | 29.1 | 0.82 | 0.79 | 0.82 | 21.5 |
| Appro | bach | | 1586 | 6.7 | 1586 | 6.7 | 0.623 | 27.8 | LOS B | 18.5 | 129.4 | 0.75 | 0.69 | 0.75 | 32.9 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 278 | 3.8 | 278 | 3.8 | *0.334 | 30.2 | LOS C | 5.6 | 40.7 | 0.68 | 0.80 | 0.68 | 23.9 |
| 5 | T1 | All MCs | 81 | 1.3 | 81 | 1.3 | 0.253 | 77.7 | LOS F | 3.0 | 20.9 | 0.91 | 0.71 | 0.91 | 24.2 |
| 6 | R2 | All MCs | 240 | 3.9 | 240 | 3.9 | 0.801 | 86.4 | LOS F | 8.9 | 64.7 | 1.00 | 1.01 | 1.12 | 18.8 |
| Appro | bach | | 599 | 3.5 | 599 | 3.5 | 0.801 | 59.1 | LOS E | 8.9 | 64.7 | 0.84 | 0.87 | 0.89 | 17.7 |
| North | : Cond | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 46 | 4.5 | 46 | 4.5 | *0.340 | 25.6 | LOS B | 4.2 | 47.2 | 0.80 | 0.71 | 0.80 | 25.3 |
| 8 | T1 | All MCs | 1198 | 8.6 | 1198 | 8.6 | * 0 .877 | 63.3 | LOS E | 23.8 | 166.6 | 0.98 | 0.97 | 1.09 | 24.4 |
| 9 | R2 | All MCs | 22 | 0.0 | 22 | 0.0 | 0.047 | 46.2 | LOS D | 0.4 | 3.0 | 0.74 | 0.68 | 0.74 | 39.4 |
| Appro | bach | | 1266 | 8.3 | 1266 | 8.3 | 0.877 | 61.7 | LOS E | 23.8 | 166.6 | 0.97 | 0.95 | 1.07 | 22.4 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 24 | 4.3 | 24 | 4.3 | 0.315 | 10.6 | LOS A | 3.7 | 26.4 | 0.92 | 0.74 | 0.92 | 29.0 |
| 11 | T1 | All MCs | 78 | 0.0 | 78 | 0.0 | * 0 .315 | 70.9 | LOS F | 3.7 | 26.4 | 0.92 | 0.74 | 0.92 | 21.7 |
| 12 | R2 | All MCs | 95 | 1.1 | 95 | 1.1 | 0.337 | 49.1 | LOS D | 3.1 | 22.2 | 0.89 | 0.76 | 0.89 | 27.6 |
| Appro | bach | | 197 | 1.1 | 197 | 1.1 | 0.337 | 53.0 | LOS D | 3.7 | 26.4 | 0.91 | 0.75 | 0.91 | 25.6 |
| All Ve | hicles | | 3648 | 6.4 | 3648 | 6.4 | 0.877 | 46.1 | LOS D | 23.8 | 166.6 | 0.85 | 0.81 | 0.89 | 25.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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V Site: 2 [(ExWednesdayPeakPM) Kenneth Road / Roseberry Street (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Network: N101 [Existing Wednesday PM Peak Hour Period (Network Folder: General)]

Existing Wednesday PM Peak Hour Period (4:45pm to 5:45pm) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Mov ID Turn Mov Class Demma Flows Total HV [Total HV] vel/h Aver Sah Evel of Sah Aver Sah Level of Sah Aver Sah Level of Sah Aver Sah Evel of Ver Aver Sah Aver Sah </th <th>Vehi</th> <th>cle M</th> <th>ovement</th> <th>t Perfo</th> <th>orma</th> <th>nce</th> <th></th> | Vehi | cle M | ovement | t Perfo | orma | nce | | | | | | | | | | |
|--|--------|--------|------------|---------|------|-------|-------|-------|-------|---------|------------|----------|-------|------|--------|---------|
| Image: Control HV Total HV Total HV Yehn Ye Sec Vehn Dist Yehn Rate Cycles Km/h South: Roseberry Street (S) 1 L2 All MCs 203 2.6 0.634 10.1 LOSA 2.4 16.9 0.84 0.77 0.99 41.1 2 T1 All MCs 235 0.0 0.634 10.1 LOSA 2.4 16.9 0.84 0.77 0.99 42.4 3 R2 All MCs 25 0.0 5 0.0 0.634 11.2 LOSA 2.4 16.9 0.84 0.77 0.99 42.3 3u U All MCs 5 0.0 5 0.0 0.634 11.6 LOSA 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E) U All MCs 15 0.0 1594 8.9 LOSA 2.0 14.2 0.78 0.69 0.87 37.2 | Mov | Turn | Mov | | | Ar | rival | Deg. | Aver. | | Aver. Back | Of Queue | Prop. | Eff. | Aver. | Aver. |
| Veh/h % v/c sec veh m km/h South: Roseberry Street (S) 1 L2 All MCs 203 2.6 0.03 4.0 0.634 10.1 LOS A 2.4 16.9 0.84 0.77 0.99 41.1 2 T1 All MCs 235 0.0 255 0.0 0.634 10.1 LOS A 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 5 0.0 5 0.0 0.634 11.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 166 0.0 0.634 11.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E) 2 0.0 1.66 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6 R2 All MCs | ID | | Class | | | | | Satn | Delay | Service | | | Que | | | Speed |
| South: Roseberry Street view 1 L2 All MCs 203 2.6 0.034 10.1 LOS A 2.4 16.9 0.84 0.77 0.99 42.4 2 T1 All MCs 65 0.0 65 0.0 0.634 10.1 LOS A 2.4 16.9 0.84 0.77 0.99 42.4 3u U All MCs 50 0.0 0.634 13.2 LOS A 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 50 0.0 0.634 14.9 LOS B 2.4 16.9 0.84 0.77 0.99 42.7 Aproact 508 1.0 0.634 14.9 LOS B 2.4 16.9 0.84 0.77 0.99 42.7 Aproact 508 1.0 0.634 1.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.7 41 1.0 0.16 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 | | | | | | | | NIO | 500 | | | | | Rate | Cycles | km/b |
| 1 L2 All MCs 203 2.6 0.634 10.1 LOSA 2.4 16.9 0.84 0.77 0.99 41.1 2 T1 All MCs 65 0.0 65 0.0 0.634 10.1 LOSA 2.4 16.9 0.84 0.77 0.99 42.4 3 R2 All MCs 235 0.0 0.634 13.2 LOSA 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 5 0.0 5 0.0 0.634 11.6 LOSA 2.4 16.9 0.84 0.77 0.99 46.3 Approach 508 1.0 0.634 11.6 LOSA 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E) 10.0 0.634 11.6 LOSA 2.0 14.2 0.78 0.69 0.87 45.5 5 T1 All MCs 10.0 1.1 0.594 19.1 LOSA 2.0 14.2 0.78 0 | South | . Ros | eberry Str | | | ven/m | 70 | V/C | Sec | _ | Ven | | _ | _ | _ | KIII/II |
| 2 T1 All MCs 65 0.0 65 0.0 0.634 10.1 LOSA 2.4 16.9 0.84 0.77 0.99 42.4 3 R2 All MCs 235 0.0 235 0.0 0.634 132 LOSA 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 5 0.0 5 0.0 0.634 14.9 LOSB 2.4 16.9 0.84 0.77 0.99 42.2 Approach 508 1.0 508 1.0 0.634 11.6 LOSA 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E) 0.631 1.1 0.634 8.7 LOSA 2.0 14.2 0.78 0.69 0.87 34.2 6 R2 All MCs 15 0.0 1.5 0.0 0.594 1.6 LOSA 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 31 | | | - | | | 000 | 2.0 | 0.004 | 40.4 | 100.4 | | 40.0 | 0.04 | 0.77 | 0.00 | |
| 3 R2 All MCs 235 0.0 0.634 13.2 LOS A 2.4 16.9 0.84 0.77 0.99 42.7 3u U All MCs 5 0.0 5 0.0 0.634 14.9 LOS B 2.4 16.9 0.84 0.77 0.99 46.3 Approach 508 1.0 508 1.0 0.634 11.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E') 4 L2 All MCs 166 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 45.5 5 T1 All MCs 15 0.0 15 0.0 0.594 1.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 15 0.0 1.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 31 0.0 31. | - | | | | | | | | | | | | | | | |
| 3u U AIMCS 5 0.0 5 0.0 0.634 14.9 LOS B 2.4 16.9 0.84 0.77 0.99 46.3 Approach 508 1.0 508 1.0 0.634 11.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.2 East Kenneth Road (E) 5 0.0 1.66 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 45.5 5 T1 All MCS 300 1.1 300 1.1 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6 R2 All MCS 30 0.1 0.09 1.0 0.594 1.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u J MI MCS 1.0 0.594 1.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u J MI MCS 31 0.0 0.429 1.5 LOS A | | | | | | | | | | | | | | | | |
| Approach 508 1.0 508 1.0 0.634 11.6 LOS A 2.4 16.9 0.84 0.77 0.99 42.2 East: Kenneth Road (E) 4 L2 All MCs 166 0.0 166 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 45.5 5 T1 All MCs 300 1.1 300 1.1 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 45.5 6 R2 All MCs 15 0.0 1.5 0.0 0.594 1.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6u U All MCs 15 0.0 15.4 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6u U All MCs 31 0.0 1.50 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 7 L2 All MCs | | | | | | | | | | | | | | | | |
| East: Kenneth Road (E) 4 L2 All MCs 166 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 45.5 5 T1 All MCs 300 1.1 300 1.1 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6 R2 All MCs 15 0.0 15 0.0 0.594 11.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6u U All MCs 2 0.0 2 0.0 0.594 13.6 LOS A 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 40.4 Vision 10 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 40.4 Vision 10 0.429 11.5 LOS A 1.3 9.1 0.87 | | | All MCs | | | _ | | | | | | | | | | |
| 4 L2 All MCs 166 0.0 166 0.0 0.594 8.7 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 5 T1 All MCs 15 0.0 1.5 0.0 0.594 1.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6 R2 All MCs 15 0.0 15 0.0 0.594 11.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 2 0.0 2.00 0.594 136 LOS A 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 483 0.7 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 483 0.7 0.594 8.9 LOS A 1.0 14.2 0.78 0.69 0.87 40.4 North: Roseberny Street (N) 10.0 0.429 11.6 </td <td>Appro</td> <td>bach</td> <td></td> <td>508</td> <td>1.0</td> <td>508</td> <td>1.0</td> <td>0.634</td> <td>11.6</td> <td>LOSA</td> <td>2.4</td> <td>16.9</td> <td>0.84</td> <td>0.77</td> <td>0.99</td> <td>42.2</td> | Appro | bach | | 508 | 1.0 | 508 | 1.0 | 0.634 | 11.6 | LOSA | 2.4 | 16.9 | 0.84 | 0.77 | 0.99 | 42.2 |
| 5 T1 All MCs 300 1.1 300 1.1 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 34.2 6 R2 All MCs 15 0.0 15 0.0 0.594 11.9 LOS A 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 2 0.0 2.00 0.594 13.6 LOS A 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 483 0.7 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 40.4 North: Foreberny Strete (N) 7 L2 All MCS 31 0.0 0.429 11.5 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCS 191 0.6 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9 R2 All MCS 1 <t< td=""><td>East:</td><td>Kenne</td><td>eth Road</td><td>(E)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 6 R2 All MCs 15 0.0 15 0.0 0.594 11.9 LOSA 2.0 14.2 0.78 0.69 0.87 37.2 6u U All MCs 2 0.0 2 0.0 0.594 13.6 LOSA 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 0.594 8.9 LOSA 2.0 14.2 0.78 0.69 0.87 40.4 North: Roseberry Street (N) 7 L2 All MCs 31 0.0 0.429 11.5 LOSA 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCs 191 0.6 0.429 11.6 LOSA 1.3 9.1 0.87 0.76 0.92 34.2 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1.429 <td>4</td> <td>L2</td> <td>All MCs</td> <td>166</td> <td>0.0</td> <td>166</td> <td>0.0</td> <td>0.594</td> <td>8.7</td> <td>LOSA</td> <td>2.0</td> <td>14.2</td> <td>0.78</td> <td>0.69</td> <td>0.87</td> <td>45.5</td> | 4 | L2 | All MCs | 166 | 0.0 | 166 | 0.0 | 0.594 | 8.7 | LOSA | 2.0 | 14.2 | 0.78 | 0.69 | 0.87 | 45.5 |
| Gu U All MCs 2 0.0 2 0.0 0.594 13.6 LOS A 2.0 14.2 0.78 0.69 0.87 39.4 Approach 483 0.7 483 0.7 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 40.4 North: Roseberry Street (N) 7 L2 All MCs 31 0.0 0.429 11.5 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCs 191 0.6 191 0.6 0.429 11.6 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9 R2 All MCs 1 0.0 1 0.0 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 < | 5 | T1 | All MCs | 300 | 1.1 | 300 | 1.1 | 0.594 | 8.9 | LOSA | 2.0 | 14.2 | 0.78 | 0.69 | 0.87 | 34.2 |
| Approach 483 0.7 483 0.7 0.594 8.9 LOS A 2.0 14.2 0.78 0.69 0.87 40.4 North: Roseberry Street (N) 7 L2 All MCs 31 0.0 31 0.0 0.429 11.5 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCs 191 0.6 0.429 11.6 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 42 0.0 0.57 | 6 | R2 | All MCs | 15 | 0.0 | 15 | 0.0 | 0.594 | 11.9 | LOSA | 2.0 | 14.2 | 0.78 | 0.69 | 0.87 | 37.2 |
| North: Roseberry Street (N) 7 L2 All MCs 31 0.0 0.429 11.5 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCs 191 0.6 191 0.6 0.429 11.6 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 39.4 West: Kenneth Road (W) 10 L2 All MCs 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 | 6u | U | All MCs | 2 | 0.0 | 2 | 0.0 | 0.594 | 13.6 | LOSA | 2.0 | 14.2 | 0.78 | 0.69 | 0.87 | 39.4 |
| 7 L2 All MCs 31 0.0 34 0.0 0.429 11.5 LOS A 1.3 9.1 0.87 0.76 0.92 34.2 8 T1 All MCs 191 0.6 191 0.6 0.429 11.6 LOS A 1.3 9.1 0.87 0.76 0.92 41.8 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 39.4 West: Kenneth Road (W) 10 L2 All MCs 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 | Appro | bach | | 483 | 0.7 | 483 | 0.7 | 0.594 | 8.9 | LOSA | 2.0 | 14.2 | 0.78 | 0.69 | 0.87 | 40.4 |
| 8 T1 All MCs 191 0.6 191 0.6 0.429 11.6 LOS A 1.3 9.1 0.87 0.76 0.92 41.8 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 39.4 West: Kenneth Road (W) 10 L2 All MCs 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 37.3 12 R2 All MCs 6 | North | : Rose | eberry Str | eet (N) | | | | | | | | | | | | |
| 9 R2 All MCs 53 0.0 53 0.0 0.429 14.7 LOS B 1.3 9.1 0.87 0.76 0.92 25.1 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 39.4 West: Kenneth Road (W 10 L2 All MCs 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 All MCs 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 12 R2 All MCs 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12 R2 All MCs 25 0.0 0.574 | 7 | L2 | All MCs | 31 | 0.0 | 31 | 0.0 | 0.429 | 11.5 | LOSA | 1.3 | 9.1 | 0.87 | 0.76 | 0.92 | 34.2 |
| 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 26.5 Mest Kenneth Road (W) Vest Kenneth Road (W) Vest Vest Second All MCs 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 All MCs 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 12 R2 All MCs 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs | 8 | T1 | All MCs | 191 | 0.6 | 191 | 0.6 | 0.429 | 11.6 | LOSA | 1.3 | 9.1 | 0.87 | 0.76 | 0.92 | 41.8 |
| 9u U All MCs 1 0.0 1 0.0 0.429 16.4 LOS B 1.3 9.1 0.87 0.76 0.92 26.5 Approach 275 0.4 275 0.4 0.429 12.2 LOS A 1.3 9.1 0.87 0.76 0.92 26.5 Mest-Kenneth Road (W) West-Kenneth Road (W) V V V V V 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 All MCs 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 12 R2 All MCs 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 37.3 12 R2 All MCs 25 0.0 25 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 0.574 12.7 </td <td>9</td> <td>R2</td> <td>All MCs</td> <td>53</td> <td>0.0</td> <td>53</td> <td>0.0</td> <td>0.429</td> <td>14.7</td> <td>LOS B</td> <td>1.3</td> <td>9.1</td> <td>0.87</td> <td>0.76</td> <td>0.92</td> <td>25.1</td> | 9 | R2 | All MCs | 53 | 0.0 | 53 | 0.0 | 0.429 | 14.7 | LOS B | 1.3 | 9.1 | 0.87 | 0.76 | 0.92 | 25.1 |
| Approach 275 0.4 275 0.4 0.429 12.2 LOSA 1.3 9.1 0.87 0.76 0.92 39.4 West: Kenneth Road (W 10 L2 All MCs 42 0.0 42 0.0 0.574 7.9 LOSA 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 All MCs 399 1.8 399 1.8 0.574 7.9 LOSA 1.8 12.8 0.61 0.72 0.64 33.8 12 R2 All MCs 68 0.0 68 0.0 0.574 11.1 LOSA 1.8 12.8 0.61 0.72 0.64 37.3 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOSA 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.574 12.7 LOSA 1.8 12.8 0.61 0.72 0.64 26.4 Approach | 9u | U | All MCs | | | 1 | 0.0 | 0.429 | 16.4 | LOS B | | 9.1 | 0.87 | 0.76 | | 26.5 |
| 10 L2 All MCs 42 0.0 42 0.0 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 11 T1 All MCs 399 1.8 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 33.8 12 R2 All MCs 68 0.0 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 26.4 Approach 535 1.4 0.574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 37.9 | Appro | ach | | 275 | 0.4 | 275 | 0.4 | 0.429 | 12.2 | LOS A | 1.3 | 9.1 | 0.87 | 0.76 | | 39.4 |
| 11 T1 All MCs 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 37.3 12 R2 All MCs 68 0.0 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 26.4 Approach 535 1.4 535 1.4 0.574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 37.9 | West | Kenn | eth Road | (W) | | | | | | | | | | | | |
| 11 T1 All MCs 399 1.8 0.574 7.9 LOS A 1.8 12.8 0.61 0.72 0.64 37.3 12 R2 All MCs 68 0.0 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 26.4 Approach 535 1.4 535 1.4 0.574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 37.9 | 10 | L2 | All MCs | 42 | 0.0 | 42 | 0.0 | 0.574 | 7.9 | LOSA | 1.8 | 12.8 | 0.61 | 0.72 | 0.64 | 33.8 |
| 12 R2 All MCs 68 0.0 68 0.0 0.574 11.1 LOS A 1.8 12.8 0.61 0.72 0.64 43.7 12u U All MCs 25 0.0 25 0.0 0.574 12.7 LOS A 1.8 12.8 0.61 0.72 0.64 26.4 Approach 535 1.4 535 1.4 0.574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 26.4 | 11 | T1 | All MCs | 399 | 1.8 | | | 0.574 | 7.9 | | 1.8 | 12.8 | 0.61 | 0.72 | 0.64 | 37.3 |
| Approach 535 1.4 574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 37.9 | 12 | R2 | All MCs | 68 | 0.0 | 68 | 0.0 | 0.574 | 11.1 | LOSA | | 12.8 | 0.61 | 0.72 | 0.64 | 43.7 |
| Approach 535 1.4 574 8.5 LOS A 1.8 12.8 0.61 0.72 0.64 37.9 | | | | | | | | | | | | | | | | |
| All Vehicles 1801 0.9 1801 0.9 0.634 10.1 LOS A 2.4 16.9 0.76 0.73 0.84 40.3 | | bach | | | | | | | | | | | | | | |
| | All Ve | hicles | | 1801 | 0.9 | 1801 | 0.9 | 0.634 | 10.1 | LOSA | 2.4 | 16.9 | 0.76 | 0.73 | 0.84 | 40.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2024 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Monday, 10 March 2025 7:29:50 PM Project: Z:\Jobs\2025\250154\MTE SIDRA\25 03 07 - SI SIDRA.sip9



ANNEXURE C: TCS PLANS (1 SHEET)



| RECONSTRU | SERVICE : JCTED : .TOR | 04-03-85 | | |
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| C D E E1 E | Z TABLE | PERMITTED | CONDITIONS | |
| x x | TS-TN-026 | E2/A/C | FILTER OPTION DISABLED ON A-B APPROACH. × P1 NOT RUNNING FILTER OPTION DISABLED ON A-C APPROACH. × P2 NOT RUNNING | |
| X X | TS-TN-026 | CTA ATEZA | × PZ NOT RUNNING | |
| x x z | < TS−TN−026 | | | |
| | 1 | C/D | | |
| X X X | <pre>(100</pre> | ĔŹĔ2 E1/A/B | | |
| + $+$ $+$ $+$ $+$ | (109 | E2/A/C | | |
| X | 1 | | | |

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| | CADD | FILE: | VV089 | 3_13J.dgn | | | |
| | SCALE | 5 | | 0 (1:200) | 5 | 10 | ISSUE |
| H ROAD | FILE | 479 | TS 20 | 6 | SUPERSEDES Sheet/issue | 13/1 | J |
| TCS No 0893 | regn. | 164 | .47 | 79.VV | .089 | 3 | sheet 13 |
| | | | | | C COPYRIGHT | ROADS AND | TRAFFIC AUTHORITY |



ANNEXURE D: PHASE DURATION REVIEW (4 SHEETS)

| Intersection | | | | | | | | | | |
|--------------|--------------------|------|----------|----------|----------|-----|--------------------|----------------|------------|--------------------------|
| | Condamine Street / | | | | | | | | | No. of Cycle Recorded |
| | Kenneth Road | | | | | | | | | - |
| Period Start | Period Finish | | | | | | | | | 11 |
| 3:00:00 PM | 3:30:00 PM | | | | | | | | | |
| | TIME S | TADT | | | TIME END | | | | | |
| Cycle 1 | HR | MIN | SEC | HR | MIN | SEC | Phase Duration (s) | Cycle Time (s) | | |
| Phase | 15 | | 54 | 15 | | 39 | 45 | 111 | 3:00:54 PM | 3:01:39 PM |
| A X | 15 | 1 | 39 | 15 | 1 | 55 | 45 | | 3:01:39 PM | 3:01:55 PM |
| D | 15 | 1 | 55 | 15 | 2 | 24 | 29 | | 3:01:55 PM | 3:02:24 PM |
| E | 15 | 2 | 24 | 15 | 2 | 45 | 29 | | 3:02:24 PM | 3:02:24 PM 3:02:45 PM |
| - | 15 | 2 | 45 | 15 | 4 | 45 | 80 | 162 | 3:02:45 PM | 3:04:05 PM |
| A Y | 15 | 4 | 45 | 15 | 4 | 17 | 12 | 162 | | 3:04:05 PM |
| D | 15 | | | 15 | 4 | | 30 | | 3:04:05 PM | 3:04:17 PM 3:04:47 PM |
| | | 4 | 17 | | | 47 | 30 | | 3:04:17 PM | |
| E E2 | 15 | 4 | 47 9 | 15 15 | 5 | 27 | 18 | | 3:04:47 PM | 3:05:09 PM 3:05:27 PM |
| | | | | | | | | 477 | 3:05:09 PM | |
| A Y | 15 | 5 | 27 29 | 15 | 6 | 29 | 62 | 133 | 3:05:27 PM | 3:06:29 PM |
| - | 15 | 6 | | 15 | 6 | 44 | 15 | | 3:06:29 PM | 3:06:44 PM |
| D | 15 | 6 | 44 | 15 | 7 | 12 | 28 | | 3:06:44 PM | 3:07:12 PM |
| E | 15 | 7 | 12 | 15 | 7 | 33 | 21 | | 3:07:12 PM | 3:07:33 PM |
| E2 | 15 | | 33 | 15 | | 40 | 7 | 154 | 3:07:33 PM | 3:07:40 PM |
| A | 15 | 7 | 40 | 15 | 8 | 44 | 64 | 151 | 3:07:40 PM | 3:08:44 PM |
| с | 15 | 8 | 44 | 15 | 8 | 58 | 14 | | 3:08:44 PM | 3:08:58 PM |
| Y | 15 | 8 | 58 | 15 | 9 | 17 | 19 | | 3:08:58 PM | 3:09:17 PM |
| D | 15 | 9 | 17 | 15 | 9 | 46 | 29 | | 3:09:17 PM | 3:09:46 PM |
| E | 15 | 9 | 46 | 15 | 10 | 11 | 25 | | 3:09:46 PM | 3:10:11 PM |
| A | 15 | 10 | 11 | 15 | 11 | 0 | 49 | 155 | 3:10:11 PM | 3:11:00 PM |
| С | 15 | 11 | 0 | 15 | 11 | 20 | 20 | | 3:11:00 PM | 3:11:20 PM |
| Y | 15 | 11 | 20 | 15 | 11 | 37 | 17 | | 3:11:20 PM | 3:11:37 PM |
| D | 15 | 11 | 37 | 15 | 12 | 6 | 29 | | 3:11:37 PM | 3:12:06 PM |
| E | 15 | 12 | 6 | 15 | 12 | 27 | 21 | | 3:12:06 PM | 3:12:27 PM |
| E2 | 15 | 12 | 27 | 15 | 12 | 46 | 19 | | 3:12:27 PM | 3:12:46 PM |
| A | 15 | 12 | 46 | 15 | 13 | 16 | 30 | 115 | 3:12:46 PM | 3:13:16 PM |
| Y | 15 | 13 | 16 | 15 | 13 | 29 | 13 | | 3:13:16 PM | 3:13:29 PM |
| D | 15 | 13 | 29 | 15 | 13 | 57 | 28 | | 3:13:29 PM | 3:13:57 PM |
| E2 | 15 | 13 | 57 | 15 | 14 | 41 | 44 | | 3:13:57 PM | 3:14:41 PM |
| A | 15 | 14 | 41 | 15 | 15 | 16 | 35 | 107 | 3:14:41 PM | 3:15:16 PM |
| Y | 15 | 15 | 16 | 15 | 15 | 29 | 13 | | 3:15:16 PM | 3:15:29 PM |
| D | 15 | 15 | 29 | 15 | 16 | 2 | 33 | | 3:15:29 PM | 3:16:02 PM |
| E2 | 15 | 16 | 2 | 15 | 16 | 28 | 26 | | 3:16:02 PM | 3:16:28 PM |
| Α | 15 | 16 | 28 | 15 | 17 | 34 | 66 | 158 | 3:16:28 PM | 3:17:34 PM |
| Y | 15 | 17 | 34 | 15 | 17 | 49 | 15 | | 3:17:34 PM | 3:17:49 PM |
| D | 15 | 17 | 49 | 15 | 18 | 17 | 28 | | 3:17:49 PM | 3:18:17 PM |
| E | 15 | 18 | 17 | 15 | 18 | 44 | 27 | | 3:18:17 PM | 3:18:44 PM |
| E2 | 15 | 18 | 44 | 15 | 19 | 6 | 22 | | 3:18:44 PM | 3:19:06 PM |
| Α | 15 | 19 | 6 | 15 | 19 | 58 | 52 | 144 | 3:19:06 PM | 3:19:58 PM |
| С | 15 | 19 | 58 | 15 | 20 | 17 | 19 | | 3:19:58 PM | 3:20:17 PM |
| Y | 15 | 20 | 17 | 15 | 20 | 31 | 14 | | 3:20:17 PM | 3:20:31 PM |
| D | 15 | 20 | 31 | 15 | 21 | 8 | 37 | | 3:20:31 PM | 3:21:08 PM |
| E | 15 | 21 | 8 | 15 | 21 | 30 | 22 | | 3:21:08 PM | 3:21:30 PM |
| Α | 15 | 21 | 30 | 15 | 22 | 28 | 58 | 154 | 3:21:30 PM | 3:22:28 PM |
| С | 15 | 22 | 28 | 15 | 22 | 37 | 9 | | 3:22:28 PM | 3:22:37 PM |
| Y | 15 | 22 | 37 | 15 | 22 | 55 | 18 | | 3:22:37 PM | 3:22:55 PM |
| D | 15 | 22 | 55 | 15 | 23 | 28 | 33 | | 3:22:55 PM | 3:23:28 PM |
| E | 15 | 23 | 28 | 15 | 23 | 55 | 27 | | 3:23:28 PM | 3:23:55 PM |
| E2 | 15 | 23 | 55 | 15 | 24 | 4 | 9 | | 3:23:55 PM | 3:24:04 PM |
| Α | 15 | 24 | 4 | 15 | 24 | 45 | 41 | 126 | 3:24:04 PM | 3:24:45 PM |
| Y | 15 | 24 | 45 | 15 | 24 | 56 | 11 | | 3:24:45 PM | 3:24:56 PM |
| D | 15 | 24 | 56 | 15 | 25 | 33 | 37 | | 3:24:56 PM | 3:25:33 PM |
| | 15 | 25 | 33 | 15 | 25 | 38 | 5 | | 3:25:33 PM | 3:25:38 PM |
| E E2 | 15 | 25 | 38 | 15 | 26 | | 32 | | | |

| le Recorded | Mod | Phase | Min | Max | Average | Occurences |
|-------------|-----|-------|-----|-----|---------|------------|
| 11 | | A | 30 | 80 | 53 | 100% |
| | | x | 16 | 16 | 16 | 9% |
| | | Y | 11 | 19 | 15 | 91% |
| | | С | 9 | 20 | 16 | 36% |
| | | D | 28 | 37 | 31 | 100% |
| :39 PM | | E | 5 | 27 | 21 | 82% |
| :55 PM | | E2 | 7 | 44 | 22 | 73% |

Cycle Time 111 162 138





| Intersection | Condamine Street / | | | | | | | | | No. of Cycle Recorded |
|------------------|--------------------|------|-----|----|----------|-----|--------------------|----------------|----------------------------|----------------------------|
| | Kenneth Road | | | | | | | | | |
| Period Start | Period Finish | | | | | | | | | 10 |
| 12:00:00 PM | 12:30:00 PM | | | | | | | | | |
| Curls 1 | TIMES | TADT | | | TIME END | | | | | |
| Cycle 1 Phase | HR | MIN | SEC | HR | MIN | SEC | Phase Duration (s) | Cycle Time (s) | | |
| | 12 | 1 | 19 | 12 | 2 | 6 | 47 | 133 | 12:01:19 PM | 12:02:06 PM |
| A C | 12 | 2 | 6 | 12 | 2 | 19 | 13 | 133 | 12:01:19 PM | 12:02:08 PM |
| Y | 12 | 2 | 19 | 12 | 2 | 39 | 20 | | 12:02:08 PM | 12:02:19 PM |
| D | 12 | 2 | 39 | 12 | 2 | 59 | 20 | | 12:02:19 PM | 12:02:59 PM |
| E | 12 | 2 | 59 | 12 | 3 | 19 | 20 | | 12:02:59 PM | 12:02:59 PM |
| E2 | 12 | 3 | 19 | 12 | 3 | 32 | 13 | | 12:02:39 PM | 12:03:19 PM |
| A | 12 | 3 | 32 | 12 | 4 | 21 | 49 | 125 | 12:03:13 PM | 12:03:32 PM |
| Y | | | 21 | 12 | 4 | 34 | 13 | 125 | 12:03:32 PM 12:04:21 PM | |
| D | 12 | 4 | 34 | 12 | 5 | 34 | 29 | | 12:04:21 PM | 12:04:34 PM |
| E | 12 | 5 | 3 | 12 | 5 | 22 | 19 | | 12:04:34 PM | 12:05:03 PM 12:05:22 PM |
| E2 | 12 | 5 | 22 | 12 | 5 | 37 | 19 | | 12:05:03 PM | 12:05:22 PM 12:05:37 PM |
| | 12 | 5 | 37 | 12 | 6 | 40 | | 139 | 12:05:22 PM | 12:05:37 PM |
| A | | | | | | | 63 | 139 | | |
| Y | 12 | 6 | 40 | 12 | 6 | 53 | 13 | | 12:06:40 PM | 12:06:53 PM |
| D | 12 | 6 | 53 | 12 | 7 | 14 | 21 | | 12:06:53 PM | 12:07:14 PM |
| E | 12 | 7 | 14 | 12 | 7 | 35 | 21 | | 12:07:14 PM | 12:07:35 PM |
| E2 | 12 | 7 | 35 | 12 | 7 | 56 | 21 | 100 | 12:07:35 PM | 12:07:56 PM |
| <u>A</u> | 12 | | 56 | 12 | 8 | 56 | 60 | 128 | 12:07:56 PM | 12:08:56 PM |
| Y | 12 | 8 | 56 | 12 | 9 | 16 | 20 | | 12:08:56 PM | 12:09:16 PM |
| D | 12 | 9 | 16 | 12 | 9 | 41 | 25 | | 12:09:16 PM | 12:09:41 PM |
| E | 12 | 9 | 41 | 12 | 10 | 4 | 23 | | 12:09:41 PM | 12:10:04 PM |
| A | 12 | 10 | 4 | 12 | 11 | 14 | 70 | 149 | 12:10:04 PM | 12:11:14 PM |
| С | 12 | 11 | 14 | 12 | 11 | 30 | 16 | | 12:11:14 PM | 12:11:30 PM |
| x | 12 | 11 | 30 | 12 | 11 | 45 | 15 | | 12:11:30 PM | 12:11:45 PM |
| D | 12 | 11 | 45 | 12 | 12 | 14 | 29 | | 12:11:45 PM | 12:12:14 PM |
| E | 12 | 12 | 14 | 12 | 12 | 33 | 19 | | 12:12:14 PM | 12:12:33 PM |
| A | 12 | 12 | 33 | 12 | 13 | 27 | 54 | 137 | 12:12:33 PM | 12:13:27 PM |
| с | 12 | 13 | 27 | 12 | 13 | 44 | 17 | | 12:13:27 PM | 12:13:44 PM |
| Y | 12 | 13 | 44 | 12 | 14 | 0 | 16 | | 12:13:44 PM | 12:14:00 PM |
| D | 12 | 14 | 0 | 12 | 14 | 29 | 29 | | 12:14:00 PM | 12:14:29 PM |
| E | 12 | 14 | 29 | 12 | 14 | 48 | 19 | | 12:14:29 PM | 12:14:48 PM |
| E2 | 12 | 14 | 48 | 12 | 14 | 50 | 2 | | 12:14:48 PM | 12:14:50 PM |
| A | 12 | 14 | 50 | 12 | 15 | 46 | 56 | 148 | 12:14:50 PM | 12:15:46 PM |
| С | 12 | 15 | 46 | 12 | 16 | 3 | 17 | | 12:15:46 PM | 12:16:03 PM |
| Y | 12 | 16 | 3 | 12 | 16 | 25 | 22 | | 12:16:03 PM | 12:16:25 PM |
| D | 12 | 16 | 25 | 12 | 16 | 42 | 17 | | 12:16:25 PM | 12:16:42 PM |
| E | 12 | 16 | 42 | 12 | 16 | 58 | 16 | | 12:16:42 PM | 12:16:58 PM |
| E2 | 12 | 16 | 58 | 12 | 17 | 18 | 20 | | 12:16:58 PM | 12:17:18 PM |
| Α | 12 | 17 | 18 | 12 | 18 | 11 | 53 | 134 | 12:17:18 PM | 12:18:11 PM |
| Y | 12 | 18 | 11 | 12 | 18 | 26 | 15 | | 12:18:11 PM | 12:18:26 PM |
| D | 12 | 18 | 26 | 12 | 18 | 52 | 26 | | 12:18:26 PM | 12:18:52 PM |
| E | 12 | 18 | 52 | 12 | 19 | 17 | 25 | | 12:18:52 PM | 12:19:17 PM |
| E2 | 12 | 19 | 17 | 12 | 19 | 32 | 15 | | 12:19:17 PM | 12:19:32 PM |
| Α | 12 | 19 | 32 | 12 | 20 | 34 | 62 | 141 | 12:19:32 PM | 12:20:34 PM |
| Y | 12 | 20 | 34 | 12 | 20 | 49 | 15 | | 12:20:34 PM | 12:20:49 PM |
| D | 12 | 20 | 49 | 12 | 21 | 17 | 28 | | 12:20:49 PM | 12:21:17 PM |
| E | 12 | 21 | 17 | 12 | 21 | 37 | 20 | | 12:21:17 PM | 12:21:37 PM |
| E2 | 12 | 21 | 37 | 12 | 21 | 53 | 16 | | 12:21:37 PM | 12:21:53 PM |
| Α | 12 | 21 | 53 | 12 | 22 | 48 | 55 | 119 | 12:21:53 PM | 12:22:48 PM |
| Y | 12 | 22 | 48 | 12 | 23 | 2 | 14 | | 12:22:48 PM | 12:23:02 PM |
| D | 12 | 23 | 2 | 12 | 23 | 33 | 31 | | 12:23:02 PM | 12:23:33 PM |
| - | 12 | 23 | 33 | 12 | 23 | 52 | 19 | | 12:23:33 PM | 12:23:52 PM |
| E | | | | | | | | | | |
| E | 1 | | | | | | | | | |
| E | | | | | | | | | | |
| E | | | | | | | | | | |

| . of Cycle Recorded | Mod | Phase | Min | Max | Average | Occurences |
|---------------------|-----|-------|-----|-----|---------|------------|
| 10 | | Α | 47 | 70 | 57 | 100% |
| | | С | 13 | 17 | 16 | 40% |
| | | Y | 13 | 22 | 16 | 90% |
| | | D | 17 | 31 | 26 | 100% |
| | | E | 16 | 25 | 20 | 100% |
| 12:02:06 PM | | E2 | 2 | 21 | 15 | 70% |
| 12:02:19 PM | | X | 15 | 15 | 15 | 10% |
| | | | | | | |

Cycle Time 125 149 135



Vm



| | | | | | | | | | | | _ |
|--------------|--------------------|----------|-----|----------|----------|----------|--------------------|----------------|--------------|-----------------------|---|
| Intersection | Condamine Street / | | | | | | | | | No. of Cycle Recorded | Γ |
| Intersection | Kenneth Road | | | | | | | | | No. or cycle necorded | |
| Period Start | Period Finish | | | | | | | | | 10 | |
| 8:15:00 AM | 8:45:00 AM | 1 | | | | | | | | | _ |
| | | • | | | | | | | | | |
| Cycle 1 | TIME S | TART | | 1 | | | | | | | |
| Phase | HR | MIN | SEC | HR | TIME END | SEC | Phase Duration (s) | Cycle Time (s) | | | 1 |
| A | 8 | 16 | 57 | 8 | 17 | 55 | 58 | 124 | 8:16:57 AM | 8:17:55 AM | 1 |
| Y | 8 | 17 | 55 | 8 | 18 | 7 | 12 | 121 | 8:17:55 AM | 8:18:07 AM | 1 |
| D | 8 | 17 | 7 | 8 | 18 | 35 | 28 | | 8:18:07 AM | 8:18:35 AM | + |
| E2 | 8 | 18 | 35 | 8 | 10 | 1 | 26 | | 8:18:35 AM | 8:19:01 AM | + |
| L | | | | | | | | | | | + |
| A | 8 | 19 | 1 | 8 | 19 | 49 | 48 | 111 | 8:19:01 AM | 8:19:49 AM | + |
| Y | 8 | 19 | 49 | 8 | 20 | 3 | 14 | | 8:19:49 AM | 8:20:03 AM | + |
| D | 8 | 20 | 3 | 8 | 20 | 30 | 27 | | 8:20:03 AM | 8:20:30 AM | 4 |
| E2 | 8 | 20 | 30 | 8 | 20 | 52 | 22 | | 8:20:30 AM | 8:20:52 AM | 4 |
| A | 8 | 20 | 52 | 8 | 21 | 50 | 58 | 133 | 8:20:52 AM | 8:21:50 AM | 1 |
| С | 8 | 21 | 50 | 8 | 22 | 3 | 13 | | 8:21:50 AM | 8:22:03 AM | 1 |
| Y | 8 | 22 | 3 | 8 | 22 | 19 | 16 | | 8:22:03 AM | 8:22:19 AM | 1 |
| D | 8 | 22 | 19 | 8 | 22 | 47 | 28 | | 8:22:19 AM | 8:22:47 AM | 1 |
| E2 | 8 | 22 | 47 | 8 | 23 | 5 | 18 | | 8:22:47 AM | 8:23:05 AM | 1 |
| A | 8 | 23 | 5 | 8 | 23 | 41 | 36 | 109 | 8:23:05 AM | 8:23:41 AM | 1 |
| Y | 8 | 23 | 41 | 8 | 23 | 53 | 12 | | 8:23:41 AM | 8:23:53 AM | 1 |
| D | 8 | 23 | 53 | 8 | 24 | 22 | 29 | | 8:23:53 AM | 8:24:22 AM | 1 |
| E | 8 | 24 | 22 | 8 | 24 | 47 | 25 | | 8:24:22 AM | 8:24:47 AM | 1 |
| E2 | 8 | 24 | 47 | 8 | 24 | 54 | 7 | | 8:24:47 AM | 8:24:54 AM | 1 |
| A | 8 | 24 | 54 | 8 | 25 | 37 | 43 | 116 | 8:24:54 AM | 8:25:37 AM | 1 |
| Y | 8 | 25 | 37 | 8 | 25 | 53 | 16 | | 8:25:37 AM | 8:25:53 AM | 1 |
| D | 8 | 25 | 53 | 8 | 26 | 17 | 24 | | 8:25:53 AM | 8:26:17 AM | + |
| E | 8 | 26 | 17 | 8 | | 39 | 24 | | 8:26:17 AM | 8:26:39 AM | + |
| E E2 | | | | | 26 | 50 | | | | | + |
| | 8 | 26 | 39 | 8 | 26 | | 11 | 107 | 8:26:39 AM | 8:26:50 AM | + |
| A | 8 | 26 | 50 | 8 | 27 | 29 | 39 | 107 | 8:26:50 AM | 8:27:29 AM | 4 |
| x | 8 | 27 | 29 | 8 | 27 | 40 | 11 | | 8:27:29 AM | 8:27:40 AM | 4 |
| D | 8 | 27 | 40 | 8 | 28 | 9 | 29 | | 8:27:40 AM | 8:28:09 AM | 4 |
| E | 8 | 28 | 9 | 8 | 28 | 31 | 22 | | 8:28:09 AM | 8:28:31 AM | 4 |
| E2 | 8 | 28 | 31 | 8 | 28 | 37 | 6 | | 8:28:31 AM | 8:28:37 AM | 4 |
| A | 8 | 28 | 37 | 8 | 29 | 43 | 66 | 146 | 8:28:37 AM | 8:29:43 AM | 1 |
| Y | 8 | 29 | 43 | 8 | 29 | 57 | 14 | | 8:29:43 AM | 8:29:57 AM | 1 |
| D | 8 | 29 | 57 | 8 | 30 | 25 | 28 | | 8:29:57 AM | 8:30:25 AM | 1 |
| E | 8 | 30 | 25 | 8 | 30 | 45 | 20 | | 8:30:25 AM | 8:30:45 AM | |
| E2 | 8 | 30 | 45 | 8 | 31 | 3 | 18 | | 8:30:45 AM | 8:31:03 AM | 1 |
| A | 8 | 31 | 3 | 8 | 32 | 11 | 68 | 134 | 8:31:03 AM | 8:32:11 AM | 1 |
| Y | 8 | 32 | 11 | 8 | 32 | 27 | 16 | | 8:32:11 AM | 8:32:27 AM | 1 |
| D | 8 | 32 | 27 | 8 | 32 | 55 | 28 | | 8:32:27 AM | 8:32:55 AM | 1 |
| E | 8 | 32 | 55 | 8 | 33 | 17 | 22 | | 8:32:55 AM | 8:33:17 AM | 1 |
| A | 8 | 33 | 17 | 8 | 34 | 3 | 46 | 113 | 8:33:17 AM | 8:34:03 AM | 1 |
| Y | 8 | 34 | 3 | 8 | 34 | 15 | 12 | | 8:34:03 AM | 8:34:15 AM | 1 |
| D | 8 | 34 | 15 | 8 | 34 | 44 | 29 | | 8:34:15 AM | 8:34:44 AM | 1 |
| E | 8 | 34 | 44 | 8 | 35 | 3 | 19 | | 8:34:44 AM | 8:35:03 AM | 1 |
| E2 | 8 | 35 | 3 | 8 | 35 | 10 | 7 | | 8:35:03 AM | 8:35:10 AM | 1 |
| A | 8 | 35 | 10 | 8 | 35 | 49 | 39 | 82 | 8:35:10 AM | 8:35:49 AM | 1 |
| Ŷ | 8 | 35 | 49 | 8 | 36 | 2 | 13 | | 8:35:49 AM | 8:36:02 AM | 1 |
| E2 | 8 | 36 | 2 | 8 | 36 | 32 | 30 | | 8:36:02 AM | 8:36:32 AM | 1 |
| | • | | - | - | | 32 | <u> </u> | | 0.30.02 AIVI | 0.30.32 Pim | 1 |
| L | | | | | <u> </u> | | | | | | Ł |
| L | | | | | <u> </u> | | | | | | Ł |
| | | — | | <u> </u> | — | <u> </u> | | | | | Ł |
| | | | | | | | | | | | Ł |
| | | | | | | | | | | | Ł |
| | | | | | | | | | | | 1 |
| | | | | | | | | | | | 1 |
| | | | | | | | | | | | 1 |
| | | | | | | | | | | | 1 |
| | | | | | | | | | | | |
| | | | | | | | | | | | |

| cle Recorded | Mod | Phase | Min Max | | Average | Occurences |
|--------------|-----|-------|---------|----|---------|------------|
| 10 | | Α | 36 | 68 | 50 | 100% |
| | | С | 13 | 13 | 13 | 10% |
| | | Y | 12 | 16 | 14 | 90% |
| | | D | 24 | 29 | 28 | 90% |
| | | E | 19 | 25 | 22 | 60% |
| 7:55 AM | | E2 | 6 | 30 | 16 | 90% |
| 3:07 AM | | X | 11 | 11 | 11 | 10% |

Cycle Time 107 133 117





| | Kenneth Road | | | | | | | | | No. of Cycle Recorded |
|------------------|---------------|------|----------|----|----------|-----|--------------------|----------------|-------------|--------------------------|
| Period Start | Period Finish | | | | | | | | | 10 |
| 4:45:00 PM | 5:15:00 PM | | | | | | | | | 10 |
| 1.15.00110 | 5.15.00110 | | | | | | | | | |
| Orde 1 | TIMES | TART | | | TIME END | | | | | |
| Cycle 1 Phase | HR | MIN | SEC | HR | MIN | SEC | Phase Duration (s) | Cycle Time (s) | | |
| A | 16 | 45 | 32 | 16 | 46 | 15 | 43 | 133 | 4:45:32 PM | 4:46:15 PM |
| c | 16 | 46 | 15 | 16 | 46 | 38 | 23 | 133 | 4:46:15 PM | 4:46:38 PM |
| Y | 16 | 46 | 38 | 16 | 40 | 53 | 15 | | 4:46:38 PM | 4:46:53 PM |
| - | | | | | | | | | | |
| D | 16 | 46 | 53 | 16 | 47 | 21 | 28 | | 4:46:53 PM | 4:47:21 PM |
| E2 | 16 | 47 | 21 | 16 | 47 | 45 | 24 | | 4:47:21 PM | 4:47:45 PM |
| A | 16 | 47 | 45 | 16 | 48 | 18 | 33 | 123 | 4:47:45 PM | 4:48:18 PM |
| С | 16 | 48 | 18 | 16 | 48 | 35 | 17 | | 4:48:18 PM | 4:48:35 PM |
| Y | 16 | 48 | 35 | 16 | 48 | 51 | 16 | | 4:48:35 PM | 4:48:51 PM |
| D | 16 | 48 | 51 | 16 | 49 | 20 | 29 | | 4:48:51 PM | 4:49:20 PM |
| E | 16 | 49 | 20 | 16 | 49 | 48 | 28 | | 4:49:20 PM | 4:49:48 PM |
| A | 16 | 49 | 48 | 16 | 50 | 33 | 45 | 140 | 4:49:48 PM | 4:50:33 PM |
| С | 16 | 50 | 33 | 16 | 50 | 50 | 17 | | 4:50:33 PM | 4:50:50 PM |
| Y | 16 | 50 | 50 | 16 | 51 | 7 | 17 | | 4:50:50 PM | 4:51:07 PM |
| D | 16 | 51 | 7 | 16 | 51 | 35 | 28 | | 4:51:07 PM | 4:51:35 PM |
| E2 | 16 | 51 | 35 | 16 | 52 | 8 | 33 | | 4:51:35 PM | 4:52:08 PM |
| A | 16 | 52 | 8 | 16 | 52 | 52 | 44 | 106 | 4:52:08 PM | 4:52:52 PM |
| Y | 16 | 52 | 52 | 16 | 53 | 9 | 17 | | 4:52:52 PM | 4:53:09 PM |
| D | 16 | 53 | 9 | 16 | 53 | 37 | 28 | | 4:53:09 PM | 4:53:37 PM |
| E | 16 | 53 | 37 | 16 | 53 | 54 | 17 | | 4:53:37 PM | 4:53:54 PM |
| Α | 16 | 53 | 54 | 16 | 55 | 16 | 82 | 166 | 4:53:54 PM | 4:55:16 PM |
| Y | 16 | 55 | 16 | 16 | 55 | 31 | 15 | | 4:55:16 PM | 4:55:31 PM |
| D | 16 | 55 | 31 | 16 | 56 | 0 | 29 | | 4:55:31 PM | 4:56:00 PM |
| E | 16 | 56 | 0 | 16 | 56 | 18 | 18 | | 4:56:00 PM | 4:56:18 PM |
| E2 | 16 | 56 | 18 | 16 | 56 | 40 | 22 | | 4:56:18 PM | 4:56:40 PM |
| Α | 16 | 56 | 40 | 16 | 57 | 41 | 61 | 132 | 4:56:40 PM | 4:57:41 PM |
| Y | 16 | 57 | 41 | 16 | 57 | 54 | 13 | | 4:57:41 PM | 4:57:54 PM |
| D | 16 | 57 | 54 | 16 | 58 | 24 | 30 | | 4:57:54 PM | 4:58:24 PM |
| E2 | 16 | 58 | 24 | 16 | 58 | 52 | 28 | | 4:58:24 PM | 4:58:52 PM |
| Α | 16 | 58 | 52 | 16 | 59 | 57 | 65 | 153 | 4:58:52 PM | 4:59:57 PM |
| С | 16 | 59 | 57 | 17 | 0 | 9 | 12 | | 4:59:57 PM | 5:00:09 PM |
| Y | 17 | 0 | 9 | 17 | 0 | 27 | 18 | | 5:00:09 PM | 5:00:27 PM |
| D | 17 | 0 | 27 | 17 | 0 | 56 | 29 | | 5:00:27 PM | 5:00:56 PM |
| E | 17 | 0 | 56 | 17 | 1 | 16 | 20 | | 5:00:56 PM | 5:01:16 PM |
| E2 | 17 | 1 | 16 | 17 | 1 | 25 | 9 | | 5:01:16 PM | 5:01:25 PM |
| A | 17 | 1 | 25 | 17 | 2 | 16 | 51 | 138 | 5:01:25 PM | 5:02:16 PM |
| c | 17 | 2 | 16 | 17 | 2 | 29 | 13 | | 5:02:16 PM | 5:02:29 PM |
| Y | 17 | 2 | 29 | 17 | 2 | 48 | 19 | | 5:02:29 PM | 5:02:48 PM |
| D | 17 | 2 | 48 | 17 | 3 | 16 | 28 | | 5:02:48 PM | 5:03:16 PM |
| E | 17 | 3 | 16 | 17 | 3 | 43 | 20 | | 5:03:16 PM | 5:03:43 PM |
| A | 17 | 3 | 43 | 17 | 4 | 32 | 49 | 155 | 5:03:43 PM | 5:04:32 PM |
| c | 17 | 4 | 32 | 17 | 4 | 52 | 20 | | 5:04:32 PM | 5:04:52 PM |
| Y | 17 | 4 | 52 | 17 | 5 | 10 | 18 | | 5:04:52 PM | 5:05:10 PM |
| D | 17 | 5 | 10 | 17 | 5 | 40 | 30 | | 5:05:10 PM | 5:05:40 PM |
| E | 17 | 5 | 40 | 17 | 6 | 0 | 20 | | 5:05:40 PM | 5:06:00 PM |
| E2 | 17 | 6 | 40 | 17 | 6 | 18 | 18 | | 5:06:00 PM | 5:06:00 PM |
| A 4 | 17 | 6 | 18 | 17 | 6 | 54 | 36 | 123 | 5:06:18 PM | 5:06:54 PM |
| A Y | 17 | 6 | 18 54 | 17 | 7 | 54 | 36 | 123 | 5:06:18 PM | 5:06:54 PM 5:07:07 PM |
| | | | | | | | | | | |
| D | 17 | 7 | 7 | 17 | 7 | 39 | 32 | | 5:07:07 PM | 5:07:39 PM |
| E | 17 | 7 | 39 | 17 | 8 | 3 | 24 | | 5:07:39 PM | 5:08:03 PM |
| E2 | 17 | 8 | 3 | 17 | 8 | 21 | 18 | | 5:08:03 PM | 5:08:21 PM |
| | | | | | <u> </u> | | | | 12:00:00 AM | 12:00:00 AM |
| | | | | | | | | | | |
| | 1 | I | | | | | | | | |
| | | | | | | | | | | |

| ycle Recorded | Mod | Phase | Min | Max | Average | Occurences | |
|---------------|-----|-------|-----|-----|---------|------------|--|
| 10 | | Α | 33 | 82 | 51 | 100% | |
| | | С | 12 | 23 | 17 | 60% | |
| | | Y | 13 | 19 | 16 | 100% | |
| | | D | 28 | 32 | 29 | 100% | |
| | | E | 17 | 28 | 22 | 70% | |
| 6:15 PM | | E2 | 9 | 33 | 22 | 70% | |
| C-39 DM | | | | | | | |

Cycle Time 106 166 133







ANNEXURE E: EAST APPROACH OF CONDAMINE STREET / KENNETH ROAD – QUEUEING OBSERVATIONS (15 SHEETS)

FRIDAY SURVEY PERIOD

















SATURDAY SURVEY PERIOD





















WEDNESDAY AM SURVEY PERIOD



















WEDNESDAY PM SURVEY PERIOD























ANNEXURE F: NORTH APPROACH OF KENNETH ROAD / ROSEBERRY STREET - QUEUEING OBSERVATIONS (15 SHEETS)

FRIDAY SURVEY PERIOD























SATURDAY SURVEY PERIOD




















WEDNESDAY AM SURVEY PERIOD





















WEDNESDAY PM SURVEY PERIOD























ANNEXURE G: EAST APPROACH OF KENNETH ROAD / ROSEBERRY STREET - QUEUEING OBSERVATIONS (15 SHEETS)

FRIDAY SURVEY PERIOD























SATURDAY SURVEY PERIOD





















WEDNESDAY AM SURVEY PERIOD





















WEDNESDAY PM SURVEY PERIOD























ANNEXURE H: SOUTH APPROACH OF KENNETH ROAD / ROSEBERRY STREET - QUEUEING OBSERVATIONS (15 SHEETS)

FRIDAY PEAK PERIOD SURVEYS























SATURDAY PEAK PERIOD SURVEYS




















WEDNESDAY AM SURVEYS





















WEDNESDAY PM SURVEYS























TECHNICAL MEMO 2 (14 SHEETS)



REVIEW OF EXISTING TRAFFIC REPORT

A review of the *Traffic Report for Proposed McDonald's* dated December 2024 created by *Colston Budd Rogers & Kafes Pty Ltd*, hereafter referred to as the **CBRK** report. The findings are outlined in the sections below.

1 TRAFFIC GENERATION

- a) The estimated traffic generation is based on '*Trip Generation and Parking Demand* Surveys of Fast Food Outlets – Analysis Report' created by Bitzios Consulting 2016. The estimated traffic generation is in the order of **140** vehicles during the afternoon peak hour, and **180** vehicles during the Saturday midday peak hour.
- b) More recent documents, specifically the *TfNSW Guide to Transport Impact Assessment*, suggests that during the weekend site peak hour, McDonald's generates
 267 vehicle trips which is an increase of 87 vehicle trips from the CBRK report.

| | Sydney | Regional | Combined |
|-----------------------|-----------------------|----------|----------|
| Weekday Vehicle trips | (vehicle trips/outlet |) | |
| Site AM Peak hour | 137 | 206 | 192 |
| Network AM Peak | 119 | 188 | 173 |
| Site PM Peak hour | 188 | 201 | 214 |
| Network PM Peak | 138 | 183 | 179 |
| Daily | 1,032 | 1,261 | 1,272 |
| Weekend Vehicle trips | (vehicle trips/outlet | ;) | |
| Site Peak hour | 267 | 225 | 269 |
| Daily | 1,209 | 1,164 | 1,303 |

c) The transitional period of the *TfNSW Guide Transport Impact Assessment* ended 4 November 2024 and therefore applies to this traffic report.

Transitional Arrangements:

This Guide does not apply to TIAs commenced and development applications lodged before 4 November 2024.

- d) It is noted that due the eastern approach to Condamine Street / Kenneth Road performing at an LoS "F", any minor increases in traffic volumes are expected to further significantly degrade the performance of this approach.
- e) It is acknowledged that 50% of the traffic to the proposed development can be considered passing trade. In any case, it is expected that the proposed McDonald's will generate destination vehicle trips which will utilise the existing road network. Approximately 44 additional trips are generated during the weekend peak hour period which should be taken into consideration.



2 SIDRA INTERSECTION 9.1 MODEL

a) Based 'Attachment A – SIDRA Movement Summaries' within the CBRK report, the Condamine Street / Kenneth Road models were run utilising 'Network Optimum Cycle Time'. This does not reflect how the intersection operates under existing conditions.

3 TRAFFIC IMPACT

3.1 Existing Conditions

 a) A comparison between the existing intersection performance of the eastern approach of Condamine Street / Kenneth Road between the CBRK assessment and MTE assessment is provided in Table 1.

TABLE 1: EASTERN APPROACH – LEVEL OF SERVICE MOVEMENT COMPARISON – EXISTING SCENARIO

| Turning | | Level of | Service | | | | |
|---------------------|------|----------|---------|-----|--|--|--|
| Turning Movement | Wee | kday | Weekend | | | | |
| wovement | CBRK | MTE | CBRK | MTE | | | |
| RT | F | F | F | F | | | |
| Т | С | F | С | F | | | |
| LT | В | D | В | D | | | |

- b) As shown, it is likely that the CBRK model underestimated the efficiency of the signalised intersection due to utilising the optimal cycle time setting which does not reflect the performance of the intersection under existing operation.
- c) A comparison of the LoS of the movements associated with the eastern approach to the signals indicates that the eastern approach exceeds capacity for the RT and T movements and is at capacity for the LT movement. It is noted that based on video footage observations, the right turn queues regularly block the ability for T and LT traffic to exit the approach.
- d) In any case, both models agree that the RT operates with an LoS "F".

3.2 Future Conditions

a) The future McDonald's traffic (based on TfNSW Guide traffic generation) has been applied to the MTE SIDRA model, with consideration to 50% passing traffic. The passing traffic has been removed from the 'T' movements at the modelled intersections and redirected to the site. The MTE model assumes a similar traffic distribution based on Figure 2 and Figure 3 of the CBRK report. The performance of the intersections is provided in Table 2 and Table 3 with the complete results presented in Annexure AThe existing SIDRA INTERSECTION 9.1 performance is provided in "Memo 1".



TABLE 2: FRIDAY POST DEVELOPMENT PERFORMANCE (SIDRA INTERSECTION

| | | | | 9.1) | | | |
|----------------------|--------------|--|--|---------------------------------------|-----------------|---------------------|-------------------|
| Intersection | Peak Hour | Degree of Saturation ⁽¹⁾ | Average Delay ⁽²⁾ (sec/veh) | Level of Service ⁽³⁾⁽⁴⁾ | Control Type | Worst Movement | Average Queue |
| | | | POST DE | VELOPMENT | PERFORMANC | E | |
| Condamine Street | AM | 1.02 | 45.1 | D | Signals | RT from Kenneth | 22.6 veh (158.2m) |
| /Kenneth Road | | 1.02 | 13.1 | 5 | Signais | Road | Condamine Street |
| Kenneth Road | | 0.01 | 17 | в | Devendelsevet | UT from | 6.4 veh (44.6m) |
| /Roseberry Street | AM | 0.91 | (Worst: 28.6) | (Worst: C) | Roundabout | Roseberry Street | Roseberry Street |

TABLE 3: SATURDAY POST DEVELOPMENT PERFORMANCE (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ⁽¹⁾ | Average Delay ⁽²⁾ (sec/veh) | Level of Service ⁽³⁾⁽⁴⁾ | Control Typ e | Worst Movement | Average Queue |
|-----------------------|--------------|--|--|---------------------------------------|-----------------------------|---------------------|-------------------|
| | | | POST DE | VELOPMENT | PERFORMANC | E | |
| Condamine Street / | AM | 0.98 | 46.7 | D | Signals | T from Kenneth | 25.3 veh (177.4m) |
| Kenneth Road | | | | _ | g | Road | Condamine Street |
| Kenneth Road / | | 1.02 | 37.6 | с | Devendebend | UT from | 13.1 veh (92.4m) |
| Roseberry Street | AM | 1.02 | (Worst: 59.4) | (Worst: E) | | Roseberry Street | Roseberry Street |

- a) By comparing the existing performance of the intersections provided in "Memo 1", it is evident that the overall performance of the signalised intersection of Condamine Street / Kenneth Road remains at a LoS "D". Although the overall performance remains the same, the traffic throughput of the eastern approach already exceeds capacity (LoS "F"), and any additional vehicle trips will adversely impact queues and delays. This is evident as the roundabout intersection of Kenneth Road / Roseberry Street quickly degrades, specifically during the Saturday period.
- b) The roundabout of Kenneth Road / Roseberry Street degrades from a Level of Service "B" to "C" during the Saturday period, with degree of saturation exceeding 1.0 and the average delay increasing from 15.7 seconds to 37.6 seconds. The subject development adversely impacts the roundabout performance.
- c) The performance of the eastern approach of Condamine Street / Kenneth Road is summarised in **Table 4**.

TABLE 4: EASTERN LEG – LEVEL OF SERVICE MOVEMENT COMPARISON – POST DEVELOPMENT

| | | | - | | | | |
|---------------------|------|----------|---------|-----|--|--|--|
| Turning | | Level of | Service | | | | |
| Turning Movement | Wee | kday | Weekend | | | | |
| Movement | CBRK | MTE | CBRK | MTE | | | |
| RT | F | F | F | F | | | |
| Т | С | F | С | F | | | |
| LT | В | D | В | D | | | |

d) Persons trip generation rates are not available for McDonald's fast-food outlets, however it is reasonable to assume that a McDonald's would generate additional pedestrian foot traffic from the surrounding area. Although pedestrian crossing facilities are provided at roundabouts, it is not particularly safe as pedestrians strictly do not have right of way at roundabouts. In practice, vehicles tend to stop to allow pedestrians to cross at roundabout which would result in additional delays.

3.3 Eastern Approach of Condamine Street / Kenneth Road – Detailed Review

To assess the eastern approach of Condamine Street / Kenneth Road in further detail, the following parameters were extracted from the **CBRK** and **MTE** SIDRA outputs:

- Degree of Saturation;
- Average Delay;
- Average Queue Length;
- 95th Percentile Queue Length (the SIDRA INTERSECTION 9.1 results for 95th percentile queue is presented in Annexure B).

The CBRK and MTE performance are summarised in Table 5 and Table 6 respectively.

TABLE 5: EASTERN APPROACH – SPECIFIC SIDRA OUTPUT PARAMETERS (CBRK MODEL)

| Peak Period | Degree of Saturation | Average Delay | Average Queue Length | 95 th Percentile Queue |
|---------------|-------------------------|-------------------|-------------------------|--------------------------------------|
| | E | xisting Condition | S | |
| Weekday | 1.011 | 56.7 seconds | 84.3m | (1) |
| Saturday | 0.99 | 55.8 seconds | 90.0m | (1) |
| | Post D | evelopment Cond | ditions | |
| Friday | 0.99 | 51.9 seconds | 80.6m | (1) |
| Saturday 1.01 | | 54.3 seconds | 90.0m | (1) |

NOTE:

(1) Cannot be determined from CBRK Report.



TABLE 6: EASTERN APPROACH – SPECIFIC SIDRA OUTPUT PARAMETERS (MTE MODEL)

| Peak Period | Degree of Saturation | Average Delay | Average Queue Length | 95 th Percentile Queue |
|-------------|-------------------------|----------------------------|-------------------------|--------------------------------------|
| | | Existing Conditions | | |
| Friday | 0.996 | 75.5 seconds | 81.4m | 132.9m |
| Saturday | 0.940 | 72.4 seconds | 75.6m | 123.4m |
| | Post Developme | nt Conditions (Satur | day Worst Case) | |
| Saturday | 0.976 | 78.1 seconds | 84.1m | 137.2m |

Based on the above, it is evident that the eastern approach is currently at maximum capacity with traffic generated by the proposed McDonalds adversely impacting the eastern approach.

4 KEY FINDINGS

The following findings and conclusions can be made upon assessment of the existing plus post development intersection conditions:

- A. The CBRK model overestimates the efficiency of the signalised intersection of Condamine Street / Kenneth Avenue by utilising the 'Network Optimum Cycle Time'. The model should utilise the existing phase durations to reflect existing conditions. As a result, the movements associated with the eastern approach perform with a lower level of service.
- B. The traffic generation rates contained within *TfNSW Guide to Transport Impact Assessment* apply. The eastern approach of Condamine Street / Kenneth Road exceeds capacity, and the roundabout of Kenneth Road / Roseberry is near capacity. Any additional traffic generated by the proposed McDonald's will result in the Kenneth Road / Roseberry Street exceeding capacity due to excessive queuing from the signalised intersection, resulting in adverse impacts to the intersection performance.
- C. The performance of the eastern approach at Condamine Street / Kenneth Road is adversely impacted. Further, the additional traffic has flow on traffic impacts to the roundabout of Kenneth Road / Roseberry Street, with queues extending past the roundabout from the signalised intersection.
- D. Application of post-development traffic to the **MTE** model indicates that the performance of Kenneth Road / Roseberry Street is adversely impacted. The performance degrades from a LoS "B" to LoS "C" with a **20.9** second increase in average delay. The degree of saturation also exceeds **1.0** under post-development conditions.
- E. Any potential intersection or road upgrades should also consider the eastern approach of the signalised intersection of Condamine Street / Kenneth Road. It is evident that there is no capacity for right turns, resulting in lane blockages for the through and left-turn movements.



ANNEXURE A: SIDRA INTERSECTION 9.1 RESULTS (4 SHEETS)

V Site: 2 [(PostDevFridayPeakPM) Kenneth Road / Roseberry Street (Site Folder: Post Development)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

■ Network: N101 [Post Development Friday PM Peak Hour Period (Network Folder: General)]

Post Development Friday Peak Hour Period (3pm to 4pm) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Vehi | cle M | ovement | t Perfo | orma | nce | | | | | | | | | | |
|---------|--------|------------|------------------|------|--------------------|-------|-------|-------|----------|---------------|------------|---------|------|--------|---------|
| Mov | Turn | Mov | Dem | | | rival | Deg. | Aver. | Level of | Aver. Back | Of Queue | e Prop. | Eff. | Aver. | Aver. |
| ID | | Class | | ows | | ows | Satn | Delay | Service | | D: (1 | Que | Stop | No. of | Speed |
| | | | [lotal veh/h | | [Total veh/h | | v/c | sec | | [Veh. veh | Dist] m | | Rate | Cycles | km/h |
| South | : Ros | eberry Str | | | Ven/m | 70 | V/C | 366 | | Ven | | _ | _ | | NIII/II |
| 1 | L2 | All MCs | 243 | 0.9 | 243 | 0.9 | 0.910 | 23.8 | LOS B | 6.4 | 44.6 | 1.00 | 1.27 | 1.90 | 30.0 |
| 2 | T1 | All MCs | 99 | 0.0 | 99 | 0.0 | 0.910 | 23.8 | LOS B | 6.4 | 44.6 | 1.00 | 1.27 | 1.90 | 32.8 |
| 3 | R2 | All MCs | 245 | 0.0 | 245 | 0.0 | 0.910 | 26.9 | LOS B | 6.4 | 44.6 | 1.00 | 1.27 | 1.90 | 33.7 |
| 3u | U | All MCs | 3 | 0.0 | 3 | 0.0 | 0.910 | 28.6 | LOS C | 6.4 | 44.6 | 1.00 | 1.27 | 1.90 | 38.2 |
| Appro | bach | | 591 | | 591 | | 0.910 | 25.1 | LOS B | 6.4 | 44.6 | 1.00 | 1.27 | 1.90 | 32.3 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 195 | 0.0 | 195 | 0.0 | 0.868 | 16.5 | LOS B | 5.1 | 36.1 | 1.00 | 1.03 | 1.49 | 39.0 |
| 5 | T1 | All MCs | 380 | | 380 | | 0.868 | 16.8 | LOS B | 5.1 | 36.1 | 1.00 | 1.03 | 1.49 | 24.9 |
| 6 | R2 | All MCs | | 0.0 | | 0.0 | 0.868 | 19.7 | LOS B | 5.1 | 36.1 | 1.00 | 1.03 | 1.49 | 29.8 |
| - 6u | U | All MCs | | 0.0 | | 0.0 | 0.868 | 21.3 | LOS B | 5.1 | 36.1 | 1.00 | 1.03 | 1.49 | 32.1 |
| Appro | bach | | 591 | | 591 | | 0.868 | 16.8 | LOS B | 5.1 | 36.1 | 1.00 | 1.03 | 1.49 | 31.9 |
| North | : Rose | eberry Str | eet (N) | | | | | | | | | | | | |
| 7 | L2 | All MCs | 22 | 9.5 | 22 | 9.5 | 0.483 | 14.3 | LOSA | 1.6 | 11.6 | 0.94 | 0.80 | 1.07 | 31.2 |
| 8 | T1 | All MCs | 192 | 0.5 | 192 | 0.5 | 0.483 | 13.8 | LOSA | 1.6 | 11.6 | 0.94 | 0.80 | 1.07 | 39.9 |
| 9 | R2 | All MCs | 61 | 3.4 | | 3.4 | 0.483 | 17.1 | LOS B | 1.6 | 11.6 | 0.94 | 0.80 | 1.07 | 22.6 |
| 9u | U | All MCs | 4 | 0.0 | 4 | 0.0 | 0.483 | 18.5 | LOS B | 1.6 | 11.6 | 0.94 | 0.80 | 1.07 | 25.0 |
| Appro | bach | | 279 | 1.9 | 279 | 1.9 | 0.483 | 14.6 | LOS B | 1.6 | 11.6 | 0.94 | 0.80 | 1.07 | 37.0 |
| West | Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 42 | 2.5 | 42 | 2.5 | 0.642 | 9.1 | LOS A | 2.3 | 16.4 | 0.61 | 0.77 | 0.70 | 32.0 |
| 11 | T1 | All MCs | 412 | 1.3 | 412 | 1.3 | 0.642 | 9.1 | LOSA | 2.3 | 16.4 | 0.61 | 0.77 | 0.70 | 35.8 |
| 12 | R2 | All MCs | 93 | 3.4 | 93 | 3.4 | 0.642 | 12.4 | LOSA | 2.3 | 16.4 | 0.61 | 0.77 | 0.70 | 42.3 |
| 12u | U | All MCs | 13 | 0.0 | 13 | 0.0 | 0.642 | 13.9 | LOS A | 2.3 | 16.4 | 0.61 | 0.77 | 0.70 | 24.4 |
| Appro | bach | | 559 | 1.7 | 559 | 1.7 | 0.642 | 9.8 | LOSA | 2.3 | 16.4 | 0.61 | 0.77 | 0.70 | 36.9 |
| All Ve | hicles | | 2019 | 1.4 | 2019 | 1.4 | 0.910 | 17.0 | LOS B | 6.4 | 44.6 | 0.88 | 1.00 | 1.33 | 33.8 |
| | | | | | | | | | | | | | | | |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Site: 1 [(PostDevSaturdayPeakPM) Condmine Street / Kenneth Road (Site Folder: Post Development)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

■ Network: N101 [Post Development Saturday Peak Hour Period (Network Folder: General)]

Post Development Saturday Peak Hour Period (12pm to 1pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 134 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|--|--------------|---------|-------------|-------------------|------------|--------------|----------------|---------------------|------------|--------|----------------|----------------------|---------------------------|----------------|
| Mov ID | Turn | Mov Class | [Total | ows HV] | Fl Total | | Deg. Satn | Aver. Delay | Level of Service | Aver. Back | Dist] | e Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
| South | veh/h % veh/h % v/c sec veh m South: Condamine Street (S) | | | | | | | | | | | | | | km/h |
| | 1 L2 All MCs 72 1.5 72 1.5 0.117 27.1 LOS B 1.9 16.9 0.48 0.60 0.48 41 | | | | | | | | | | | | | | 41.0 |
| 2 | T1 | All MCs | | | 1337 | | 0.642 | 27.1 | LOSB | 1.9 | 131.7 | 0.46 | 0.60 | 0.40 | 41.0 37.3 |
| 2 | | All MCs | 411 | | 411 | | * 0.793 | 36.9 | LOS D | 9.4 | 66.1 | 0.75 | 0.00 | 1.04 | 37.3 16.4 |
| Appro | | | | | 1819 | | 0.793 | 29.4 | LOSIC | 18.8 | 131.7 | 0.30 | 0.54 | 0.80 | 31.3 |
| Арри | Jach | | 1019 | 2.1 | 1019 | 2.1 | 0.795 | 29.4 | 1030 | 10.0 | 131.7 | 0.19 | 0.74 | 0.00 | 31.5 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 365 | 0.9 | <mark>362</mark> | 0.9 | *0.477 | 47.1 | LOS D | 8.1 | 56.8 | 0.76 | 0.90 | 0.76 | 20.6 |
| 5 | T1 | All MCs | 51 | 2.1 | <mark>50</mark> | 2.1 | 0.175 | 78.6 | LOS F | 1.8 | 12.6 | 0.91 | 0.69 | 0.91 | 24.4 |
| 6 | R2 | All MCs | 257 | 0.8 | <mark>255</mark> | 0.8 | *0.976 | 122.2 | LOS F | 11.9 | 84.1 | 1.00 | 1.20 | 1.49 | 13.8 |
| Appro | bach | | 673 | 0.9 | <mark>667</mark> | 0.9 | 0.976 | 78.1 | LOS F | 11.9 | 84.1 | 0.86 | 1.00 | 1.05 | 14.0 |
| North | : Cond | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 82 | 0.0 | 82 | 0.0 | 0.161 | 21.7 | LOS B | 2.2 | 18.3 | 0.66 | 0.69 | 0.66 | 30.8 |
| 8 | T1 | All MCs | 1274 | 1.9 | 1274 | 1.9 | *0.863 | 55.4 | LOS D | 25.3 | 177.4 | 0.99 | 0.95 | 1.07 | 26.6 |
| 9 | R2 | All MCs | 49 | 0.0 | 49 | 0.0 | 0.095 | 41.2 | LOS C | 0.8 | 5.7 | 0.72 | 0.71 | 0.72 | 40.9 |
| Appro | bach | | 1405 | 1.7 | 1405 | 1.7 | 0.863 | 52.9 | LOS D | 25.3 | 177.4 | 0.96 | 0.93 | 1.03 | 24.6 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 63 | 0.0 | 63 | 0.0 | 0.320 | 10.0 | LOS A | 3.6 | 25.2 | 0.91 | 0.76 | 0.91 | 29.1 |
| 11 | T1 | All MCs | 39 | 0.0 | 39 | 0.0 | *0.320 | 132.8 | LOS F | 3.6 | 25.2 | 0.91 | 0.76 | 0.91 | 21.6 |
| 12 | R2 | All MCs | 114 | 1.9 | 114 | 1.9 | 0.616 | 54.2 | LOS D | 3.9 | 27.9 | 1.00 | 0.79 | 1.02 | 26.2 |
| Appro | bach | | 216 | 1.0 | 216 | 1.0 | 0.616 | 55.5 | LOS D | 3.9 | 27.9 | 0.96 | 0.78 | 0.97 | 26.4 |
| All Ve | hicles | ; | 4113 | 1.7 | <mark>4107</mark> | 1.7 | 0.976 | 46.7 | LOS D | 25.3 | 177.4 | 0.87 | 0.85 | 0.93 | 24.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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V Site: 2 [(PostDevSaturdayPeakPM) Kenneth Road / Roseberry Street (Site Folder: Post Development)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Network: N101 [Post Development Saturday Peak Hour Period (Network Folder: General)]

Post Development Saturday Peak Hour Period (12pm to 1pm) Kenneth Road / Roseberry Street Job No. 250154 Site Category: (None) Roundabout

| Vehi | cle M | ovement | t Performa | nce | | | | | | | | | |
|--------|--------|------------|-----------------------|-------------------------|-------|-------|----------|---------------|----------------|-------|------|--------|---------|
| Mov | Turn | Mov | Demand | Arrival | Deg. | Aver. | Level of | Aver. Back | Of Queue | Prop. | Eff. | Aver. | Aver. |
| ID | | Class | Flows | Flows | Satn | Delay | Service | | D : (1) | Que | Stop | No. of | Speed |
| | | | [Total HV] veh/h % | [lotal HV] veh/h % | v/c | sec | | [Veh. veh | Dist] m | | Rate | Cycles | km/h |
| South | : Ros | eberry Str | | | VIC | 366 | _ | Ven | | _ | _ | _ | KITI/TT |
| 1 | | All MCs | 299 0.7 | 299 0.7 | 1.021 | 54.6 | LOS D | 13.1 | 92.4 | 1.00 | 2.00 | 3.39 | 18.6 |
| 2 | T1 | All MCs | 106 0.0 | 106 0.0 | 1.021 | 54.7 | LOS D | 13.1 | 92.4 | 1.00 | 2.00 | 3.39 | 21.6 |
| 3 | R2 | All MCs | 237 0.4 | 237 0.4 | 1.021 | 57.9 | LOSE | 13.1 | 92.4 | 1.00 | 2.00 | 3.39 | 22.7 |
| 3u | U | All MCs | 7 0.0 | 7 0.0 | 1.021 | 59.4 | LOSE | 13.1 | 92.4 | 1.00 | 2.00 | 3.39 | 27.3 |
| Appro | | 7411005 | 649 0.5 | 649 0.5 | 1.021 | 55.9 | LOS D | 13.1 | 92.4 | 1.00 | 2.00 | 3.39 | 20.9 |
| | | | | 010 0.0 | 1.021 | 00.0 | LOOD | 10.1 | 02.1 | 1.00 | 2.00 | 0.00 | 20.0 |
| East: | Kenn | eth Road | (E) | | | | | | | | | | |
| 4 | L2 | All MCs | 256 0.4 | 256 0.4 | 1.005 | 49.6 | LOS D | 11.0 | 77.2 | 1.00 | 1.97 | 3.23 | 24.4 |
| 5 | T1 | All MCs | 319 0.7 | 319 0.7 | 1.005 | 49.7 | LOS D | 11.0 | 77.2 | 1.00 | 1.97 | 3.23 | 11.5 |
| 6 | R2 | All MCs | 15 0.0 | 15 0.0 | 1.005 | 52.8 | LOS D | 11.0 | 77.2 | 1.00 | 1.97 | 3.23 | 16.1 |
| 6u | U | All MCs | 1 0.0 | 1 0.0 | 1.005 | 54.4 | LOS D | 11.0 | 77.2 | 1.00 | 1.97 | 3.23 | 18.0 |
| Appro | ach | | 591 0.5 | 591 0.5 | 1.005 | 49.7 | LOS D | 11.0 | 77.2 | 1.00 | 1.97 | 3.23 | 18.3 |
| North | : Rose | eberry Str | eet (N) | | | | | | | | | | |
| 7 | L2 | All MCs | 22 0.0 | 22 0.0 | 0.500 | 15.8 | LOS B | 1.6 | 11.3 | 0.98 | 0.86 | 1.17 | 30.4 |
| 8 | T1 | All MCs | 163 0.0 | 163 0.0 | 0.500 | 15.9 | LOS B | 1.6 | 11.3 | 0.98 | 0.86 | 1.17 | 38.4 |
| 9 | R2 | All MCs | 47 2.2 | 47 2.2 | 0.500 | 19.1 | LOS B | 1.6 | 11.3 | 0.98 | 0.86 | 1.17 | 20.8 |
| 9u | U | All MCs | 2 0.0 | 2 0.0 | 0.500 | 20.6 | LOS B | 1.6 | 11.3 | 0.98 | 0.86 | 1.17 | 23.8 |
| Appro | ach | | 235 0.4 | 235 0.4 | 0.500 | 16.6 | LOS B | 1.6 | 11.3 | 0.98 | 0.86 | 1.17 | 35.6 |
| West | Kenn | eth Road | (W) | | | | | | | | | | |
| 10 | L2 | All MCs | 53 50.0 | 53 50.0 | 0.827 | 15.6 | LOS B | 4.4 | 36.2 | 0.77 | 0.97 | 1.10 | 24.4 |
| 11 | T1 | All MCs | 362 0.9 | 362 0.9 | 0.827 | 13.5 | LOS A | 4.4 | 36.2 | 0.77 | 0.97 | 1.10 | 30.3 |
| 12 | R2 | All MCs | 202 41.1 | 202 41.1 | 0.827 | 18.5 | LOS B | 4.4 | 36.2 | 0.77 | 0.97 | 1.10 | 36.0 |
| 12u | U | All MCs | 23 50.0 | 23 50.0 | 0.827 | 20.5 | LOS B | 4.4 | 36.2 | 0.77 | 0.97 | 1.10 | 18.5 |
| Appro | ach | | 640 19.4 | 640 19.4 | 0.827 | 15.5 | LOS B | 4.4 | 36.2 | 0.77 | 0.97 | 1.10 | 32.0 |
| All Ve | hicles | | 2115 6.2 | 2115 6.2 | 1.021 | 37.6 | LOS C | 13.1 | 92.4 | 0.93 | 1.56 | 2.41 | 23.3 |
| | | | | | | | | | | | | | |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Site: 1 [(PostDevFridayPeakPM) Condmine Street / Kenneth Road (Site Folder: Post Development)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Post Development Friday Peak Hour Period (3pm to 4pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 136 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|---|--------------|---------------------------------|-------------|---------------|---------------------------|---------------------|-----------------------|---------------------|-----------------------------|-------------------------|----------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | Dem Fl [Total] veh/h | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | Aver. Back [Veh. veh | Of Queue Dist] m | e Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| South | South: Condamine Street (S) | | | | | | | | | | | | | | |
| 1 | L2 All MCs 88 0.0 88 0.0 0.192 30.0 LOS C 3.1 30.1 0.52 0.59 0.52 4 | | | | | | | | | | | | | | |
| 2 | T1 | All MCs | 1476 | 4.9 | 1476 | 4.9 | 0.715 | 29.7 | LOS C | 22.6 | 158.2 | 0.79 | 0.73 | 0.79 | 36.3 |
| 3 | R2 | All MCs | 413 | 1.5 | 413 | 1.5 | *0.707 | 29.6 | LOS C | 8.2 | 57.8 | 0.94 | 0.88 | 0.94 | 19.2 |
| Appro | bach | | 1977 | 3.9 | 1977 | 3.9 | 0.715 | 29.7 | LOS C | 22.6 | 158.2 | 0.81 | 0.75 | 0.81 | 31.3 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 396 | 1.6 | 396 | 1.6 | *0.490 | 44.3 | LOS D | 8.5 | 60.3 | 0.72 | 0.88 | 0.72 | 21.6 |
| 5 | T1 | All MCs | 68 | 0.0 | 68 | 0.0 | 0.191 | 73.0 | LOS F | 2.4 | 16.5 | 0.89 | 0.69 | 0.89 | 25.4 |
| 6 | R2 | All MCs | 233 | 5.4 | 233 | 5.4 | * 1.022 | 111.0 | LOS F | 10.4 | 76.4 | 1.00 | 1.27 | 1.66 | 11.1 |
| Appro | bach | | 697 | 2.7 | 697 | 2.7 | 1.022 | 69.4 | LOS E | 10.4 | 76.4 | 0.83 | 0.99 | 1.05 | 13.3 |
| North | : Cond | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 66 | 4.8 | 66 | 4.8 | 0.309 | 25.5 | LOS B | 3.9 | 40.8 | 0.76 | 0.69 | 0.76 | 27.8 |
| 8 | T1 | All MCs | 1183 | 7.4 | 1183 | 7.4 | *0.836 | 54.1 | LOS D | 22.0 | 154.3 | 0.97 | 0.91 | 1.03 | 26.6 |
| 9 | R2 | All MCs | 57 | 0.0 | 57 | 0.0 | 0.125 | 42.6 | LOS D | 1.0 | 6.8 | 0.78 | 0.72 | 0.78 | 39.5 |
| Appro | bach | | 1306 | 6.9 | 1306 | 6.9 | 0.836 | 52.2 | LOS D | 22.0 | 154.3 | 0.95 | 0.89 | 1.00 | 24.9 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 68 | 1.5 | 68 | 1.5 | 0.431 | 9.7 | LOS A | 5.7 | 40.1 | 0.93 | 0.78 | 0.93 | 29.4 |
| 11 | T1 | All MCs | 91 | 0.0 | 91 | 0.0 | *0.431 | 90.0 | LOS F | 5.7 | 40.1 | 0.93 | 0.78 | 0.93 | 22.0 |
| 12 | R2 | All MCs | 136 | 2.3 | 136 | 2.3 | 0.816 | 64.9 | LOS E | 5.0 | 35.7 | 1.00 | 0.94 | 1.22 | 23.6 |
| Appro | bach | | 295 | 1.4 | 295 | 1.4 | 0.816 | 59.8 | LOS E | 5.7 | 40.1 | 0.96 | 0.85 | 1.06 | 24.7 |
| All Ve | hicles | | 4275 | 4.5 | 4275 | 4.5 | 1.022 | 45.1 | LOS D | 22.6 | 158.2 | 0.87 | 0.84 | 0.93 | 24.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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ANNEXURE B: SIDRA INTERSECTION 9.1 RESULTS – WITH 95^{TH} PERCENTILE QUEUE OUTPUT (3 SHEETS)

Site: 1 [(ExFridayPeakPM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Friday Peak Hour Period (3pm to 4pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 136 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|--|--------------|-----------|-------------|---------------|---------------------------|---------------------|-----------------------|---------------------|---------------------------|-------------------------|--------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Back [Veh. veh | Of Queue Dist] m | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| South | South: Condamine Street (S) | | | | | | | | | | | | | | |
| 1 | 1 L2 All MCs 88 0.0 88 0.0 0.192 30.1 LOS C 5.1 49.1 0.52 0.59 0.52 40 | | | | | | | | | | | | | | 40.6 |
| 2 | T1 | All MCs | 1481 | 4.8 | 1481 | 4.8 | 0.717 | 29.8 | LOS C | 37.1 | 259.8 | 0.80 | 0.73 | 0.80 | 36.3 |
| 3 | R2 | All MCs | 402 | 1.6 | 402 | 1.6 | *0.690 | 28.8 | LOS C | 12.7 | 90.4 | 0.93 | 0.87 | 0.93 | 19.6 |
| Appro | oach | | 1972 | 4.0 | 1972 | 4.0 | 0.717 | 29.6 | LOS C | 37.1 | 259.8 | 0.81 | 0.75 | 0.81 | 31.4 |
| East: | Kenne | eth Road | (E) | | | | | | | | | | | | |
| 4 | L2 | All MCs | 389 | 1.6 | 389 | 1.6 | *0.482 | 43.9 | LOS D | 13.5 | 95.9 | 0.72 | 0.88 | 0.72 | 21.6 |
| 5 | T1 | All MCs | 68 | 0.0 | 68 | 0.0 | 0.191 | 72.2 | LOS F | 3.8 | 26.9 | 0.89 | 0.69 | 0.89 | 25.4 |
| 6 | R2 | All MCs | 226 | 5.6 | 226 | 5.6 | *0.996 | 131.0 | LOS F | 18.1 | 132.9 | 1.00 | 1.23 | 1.57 | 12.7 |
| Appro | oach | | 684 | 2.8 | 684 | 2.8 | 0.996 | 75.5 | LOS F | 18.1 | 132.9 | 0.83 | 0.98 | 1.02 | 14.3 |
| North | : Con | damine St | treet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 56 | 5.7 | 56 | 5.7 | 0.294 | 25.1 | LOS B | 5.9 | 63.2 | 0.76 | 0.68 | 0.76 | 28.0 |
| 8 | T1 | All MCs | 1188 | 7.4 | 1188 | 7.4 | * 0.840 | 54.6 | LOS D | 36.4 | 254.7 | 0.97 | 0.92 | 1.03 | 26.5 |
| 9 | R2 | All MCs | 57 | 0.0 | 57 | 0.0 | 0.126 | 42.8 | LOS D | 1.6 | 11.1 | 0.78 | 0.72 | 0.78 | 39.5 |
| Appro | oach | | 1301 | 7.0 | 1301 | 7.0 | 0.840 | 52.8 | LOS D | 36.4 | 254.7 | 0.96 | 0.90 | 1.01 | 24.8 |
| West | : Kenn | eth Road | (W) | | | | | | | | | | | | |
| 10 | L2 | All MCs | 68 | 1.5 | 68 | 1.5 | 0.431 | 9.7 | LOS A | 9.3 | 65.5 | 0.93 | 0.78 | 0.93 | 29.4 |
| 11 | T1 | All MCs | 91 | 0.0 | 91 | 0.0 | *0.431 | 90.0 | LOS F | 9.3 | 65.5 | 0.93 | 0.78 | 0.93 | 22.0 |
| 12 | R2 | All MCs | 136 | 2.3 | 136 | 2.3 | 0.802 | 64.2 | LOS E | 8.1 | 57.8 | 1.00 | 0.93 | 1.19 | 23.8 |
| Appro | oach | | 295 | 1.4 | 295 | 1.4 | 0.802 | 59.4 | LOS E | 9.3 | 65.5 | 0.96 | 0.85 | 1.05 | 24.8 |
| All Ve | ehicles | | 4252 | 4.5 | 4252 | 4.5 | 0.996 | 46.2 | LOS D | 37.1 | 259.8 | 0.87 | 0.84 | 0.92 | 25.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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Site: 1 [(ExSaturdayPeakPM) Condmine Street / Kenneth Road (Site Folder: Existing)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Existing Saturday Peak Hour Period (12pm to 1pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 134 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|---|----------------------|--------------|---------|-------------|---------------|---------------------------|---------------------|-----------------------|---------------------|---------------------------|-------------------------|--------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | [Total | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Back [Veh. veh | Of Queue Dist] m | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| veh/h % veh/h % v/c sec veh m km South: Condamine Street (S) | | | | | | | | | | | | | | KI 11/11 | |
| 1 | L2 | All MCs | 72 | 1.5 | 72 | 1.5 | 0.117 | 27.3 | LOS B | 3.1 | 27.6 | 0.48 | 0.60 | 0.48 | 41.0 |
| 2 | T1 | All MCs | 1347 | 2.5 | 1347 | 2.5 | 0.648 | 27.3 | LOS B | 31.1 | 217.7 | 0.75 | 0.69 | 0.75 | 37.3 |
| 3 | R2 | All MCs | 389 | 0.8 | 389 | 0.8 | *0.715 | 30.1 | LOS C | 13.3 | 93.9 | 0.95 | 0.88 | 0.95 | 19.0 |
| Appr | oach | | 1808 | 2.1 | 1808 | 2.1 | 0.715 | 27.9 | LOS B | 31.1 | 217.7 | 0.79 | 0.73 | 0.79 | 32.1 |
| East: Kenneth Road (E) | | | | | | | | | | | | | | | |
| 4 | L2 | All MCs | 356 | 0.9 | 356 | 0.9 | *0.468 | 46.5 | LOS D | 12.9 | 91.0 | 0.76 | 0.89 | 0.76 | 20.6 |
| 5 | T1 | All MCs | 51 | 2.1 | 51 | 2.1 | 0.176 | 77.7 | LOS F | 2.9 | 20.7 | 0.91 | 0.69 | 0.91 | 24.4 |
| 6 | R2 | All MCs | 247 | 0.9 | 247 | 0.9 | *0.940 | 108.7 | LOS F | 17.5 | 123.4 | 1.00 | 1.15 | 1.39 | 15.3 |
| Appr | oach | | 654 | 1.0 | 654 | 1.0 | 0.940 | 72.4 | LOS F | 17.5 | 123.4 | 0.86 | 0.98 | 1.01 | 14.8 |
| North | n: Con | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 67 | 0.0 | 67 | 0.0 | 0.137 | 21.2 | LOS B | 3.0 | 26.1 | 0.65 | 0.67 | 0.65 | 31.1 |
| 8 | T1 | All MCs | 1281 | 1.9 | 1281 | 1.9 | * 0 .868 | 56.1 | LOS D | 41.9 | 293.6 | 0.99 | 0.96 | 1.08 | 26.4 |
| 9 | R2 | All MCs | 49 | 0.0 | 49 | 0.0 | 0.095 | 41.8 | LOS C | 1.3 | 9.3 | 0.73 | 0.71 | 0.73 | 40.7 |
| Appr | oach | | 1398 | 1.7 | 1398 | 1.7 | 0.868 | 53.9 | LOS D | 41.9 | 293.6 | 0.96 | 0.94 | 1.04 | 24.4 |
| West: Kenneth Road (W) | | | | | | | | | | | | | | | |
| 10 | L2 | All MCs | 63 | 0.0 | 63 | 0.0 | 0.313 | 10.1 | LOS A | 5.9 | 41.0 | 0.91 | 0.76 | 0.91 | 29.1 |
| 11 | T1 | All MCs | 39 | 0.0 | 39 | 0.0 | *0.313 | 132.5 | LOS F | 5.9 | 41.0 | 0.91 | 0.76 | 0.91 | 21.6 |
| 12 | R2 | All MCs | 114 | 1.9 | 114 | 1.9 | 0.605 | 54.1 | LOS D | 6.4 | 45.5 | 1.00 | 0.79 | 1.01 | 26.2 |
| Appr | Approach 216 1.0 216 | | | | | 1.0 | 0.605 | 55.4 | LOS D | 6.4 | 45.5 | 0.96 | 0.77 | 0.96 | 26.4 |
| All Ve | ehicles | | 4076 | 1.7 | 4076 | 1.7 | 0.940 | 45.4 | LOS D | 41.9 | 293.6 | 0.87 | 0.84 | 0.92 | 25.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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Site: 1 [(PostDevSaturdayPeakPM) Condmine Street / Kenneth Road (Site Folder: Post Development)] Output produced by SIDRA INTERSECTION Version: 9.1.6.228

■ Network: N101 [Post Development Saturday Peak Hour Period (Network Folder: General)]

Post Development Saturday Peak Hour Period (12pm to 1pm) Condamine Street / Kenneth Road Job No. 250127 Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 134 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|--------------------------|--------------|---------------------------------|------------|-------------------|---------------------------|---------------------|-----------------------|---------------------|---------------------------|-------------------------|--------------|----------------------|---------------------------|------------------------|
| Mov ID | Turn | Mov Class | Dem Fl [Total] veh/h | ows HV] | Fl Total | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Back [Veh. veh | Of Queue Dist] m | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed km/h |
| South: Condamine Street (S) | | | | | | | | | | | | | | | |
| 1 | L2 | All MCs | 72 | 1.5 | 72 | 1.5 | 0.117 | 27.1 | LOS B | 3.1 | 27.6 | 0.48 | 0.60 | 0.48 | 41.0 |
| 2 | T1 | All MCs | 1337 | 2.5 | 1337 | 2.5 | 0.642 | 27.1 | LOS B | 30.7 | 214.9 | 0.75 | 0.68 | 0.75 | 37.3 |
| 3 | R2 | All MCs | 411 | 0.8 | 411 | 0.8 | *0.793 | 36.9 | LOS C | 15.3 | 107.9 | 0.98 | 0.94 | 1.04 | 16.4 |
| Appro | bach | | 1819 | 2.1 | 1819 | 2.1 | 0.793 | 29.4 | LOS C | 30.7 | 214.9 | 0.79 | 0.74 | 0.80 | 31.3 |
| East: Kenneth Road (E) | | | | | | | | | | | | | | | |
| 4 | L2 | All MCs | 365 | 0.9 | <mark>362</mark> | 0.9 | *0.477 | 47.1 | LOS D | 13.1 | 92.7 | 0.76 | 0.90 | 0.76 | 20.6 |
| 5 | T1 | All MCs | 51 | 2.1 | <mark>50</mark> | 2.1 | 0.175 | 78.6 | LOS F | 2.9 | 20.6 | 0.91 | 0.69 | 0.91 | 24.4 |
| 6 | R2 | All MCs | 257 | 0.8 | <mark>255</mark> | 0.8 | *0.976 | 122.2 | LOS F | 19.5 | 137.2 | 1.00 | 1.20 | 1.49 | 13.8 |
| Appro | bach | | 673 | 0.9 | <mark>667</mark> | 0.9 | 0.976 | 78.1 | LOS F | 19.5 | 137.2 | 0.86 | 1.00 | 1.05 | 14.0 |
| North | : Cond | damine St | reet (N |) | | | | | | | | | | | |
| 7 | L2 | All MCs | 82 | 0.0 | 82 | 0.0 | 0.161 | 21.7 | LOS B | 3.6 | 29.9 | 0.66 | 0.69 | 0.66 | 30.8 |
| 8 | T1 | All MCs | 1274 | 1.9 | 1274 | 1.9 | *0.863 | 55.4 | LOS D | 41.4 | 289.6 | 0.99 | 0.95 | 1.07 | 26.6 |
| 9 | R2 | All MCs | 49 | 0.0 | 49 | 0.0 | 0.095 | 41.2 | LOS C | 1.3 | 9.3 | 0.72 | 0.71 | 0.72 | 40.9 |
| Appro | bach | | 1405 | 1.7 | 1405 | 1.7 | 0.863 | 52.9 | LOS D | 41.4 | 289.6 | 0.96 | 0.93 | 1.03 | 24.6 |
| West: Kenneth Road (W) | | | | | | | | | | | | | | | |
| 10 | L2 | All MCs | 63 | 0.0 | 63 | 0.0 | 0.320 | 10.0 | LOS A | 5.9 | 41.1 | 0.91 | 0.76 | 0.91 | 29.1 |
| 11 | T1 | All MCs | 39 | 0.0 | 39 | 0.0 | *0.320 | 132.8 | LOS F | 5.9 | 41.1 | 0.91 | 0.76 | 0.91 | 21.6 |
| 12 | R2 | All MCs | 114 | 1.9 | 114 | 1.9 | 0.616 | 54.2 | LOS D | 6.4 | 45.5 | 1.00 | 0.79 | 1.02 | 26.2 |
| Appro | Approach 216 1.0 216 1.0 | | | | | 0.616 | 55.5 | LOS D | 6.4 | 45.5 | 0.96 | 0.78 | 0.97 | 26.4 | |
| All Ve | hicles | | 4113 | 1.7 | <mark>4107</mark> | 1.7 | 0.976 | 46.7 | LOS D | 41.4 | 289.6 | 0.87 | 0 .85 | 0.93 | 24.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Override Site Data tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

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