## GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Devel	Popment Application forName of Applicant
	Name от Аррисанс
Addre	ss of site 94 Whale Beach Road, Whale Beach
	owing checklist covers the minimum requirements to be addressed in a Geotechnical Risk <b>Declaration made by</b> Innical engineer or engineering geologist or coastal engineer (where applicable) as part of a geotechnical report
I,	Ben White on behalf of White Geotechnical Group Pty Ltd (Insert Name) (Trading or Company Name)
coastal organisa	the certify that I am a geotechnical engineer or engineering geologist or engineer as defined by the Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the above ation/company to issue this document and to certify that the organisation/company has a current professional indemnity at least \$10million.
l: Please	mark appropriate box
	have prepared the detailed Geotechnical Report referenced below in accordance with the Australia Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
	am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
	have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.
	have examined the site and the proposed development/alteration in detail and I am of the opinion that the Development Application only involves Minor Development/Alteration that does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
	have examined the site and the proposed development/alteration is separate from and is not affected by a Geotechnical Hazard and does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
	have provided the coastal process and coastal forces analysis for inclusion in the Geotechnical Report
Geotec	Report Title: Geotechnical Report 94 Whale Beach Road, Whale Beach
	Report Date: 21/12/21
	Author: BEN WHITE
	Author's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD
Docum	entation which relate to or are relied upon in report preparation:
	Australian Geomechanics Society Landslide Risk Management March 2007.
	White Geotechnical Group company archives.
Develop Risk Ma Manage	vare that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a ment Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnica magement aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk ment" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and sonable and practical measures have been identified to remove foreseeable risk.

Signature

Name

Ben White

Chartered Professional Status

MScGEOLAusIMM CP GEOL

Membership No. 222757

Company White Geotechnical Group Pty Ltd

# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Develo	pment Application f		lame of Applicant	
Addres	s of site		• •	
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Report	Title: Geotechnical R	eport 94 Whale Beach R	oad. Whale Beach	
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Report I	Date: 21/12/21			
Author:	BEN WHITE			
Author	's Company/Organi	sation: WHITE GEOTECHI	NICAL GROUP PTY LTD	
Please m	nark appropriate bo	K		
	Comprehensive site r			
	Subsurface investiga	tion required  Justification	with geomorphic mapping to a minimum so	cale of 1:200 (as appropriate)
	Geotechnical hazards  ☐ Above  ☐ On the ☐ Below t	developed and reported as an s identified the site site he site	inferred subsurface type-section	
	Geotechnical hazards Risk assessment con ⊠ Consec	s described and reported ducted in accordance with the quence analysis	e Geotechnical Risk Management Policy fo	or Pittwater - 2009
$\boxtimes$	Risk calculation	noy analysis		
	Risk assessment for Risk assessment for Assessed risks have Management Policy f	oss of life conducted in accor been compared to "Acceptab or Pittwater - 2009	dance with the Geotechnical Risk Manage e Risk Management" criteria as defined in	ement Policy for Pittwater - 2009 the Geotechnical Risk
	specified conditions a	re achieved.	•	•
	Design Life Adopted:  ⊠ 100 yea  □ Other _	ars		
	Pittwater - 2009 have Additional action to re	ons to be applied to all four pl been specified move risk where reasonable	and practical have been identified and inc	
that the g Managen	eotechnical risk mana nent" level for the life reasonable and pract	Name of Applicant  94 Whale Beach Road, Whale Beach  Pers the minimum requirements to be addressed in a Geotechnical Risk Management Geotechnical accompany the Geotechnical Report and its certification (Form No. 1).  Ills:  Report 94 Whale Beach Road, Whale Beach  Inisation: WHITE GEOTECHNICAL GROUP PTY LTD  DOX  The mapping conducted 23/11/21 (date)  The essented on contoured site plan with geomorphic mapping to a minimum scale of 1:200 (as appropriate) gation required  Justification  Date conducted 23/11/21  El developed and reported as an inferred subsurface type-section risk identified we the site with the site de the site with the Geotechnical Risk Management Policy for Pittwater - 2009 sequence analysis uency analysis  The property conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 or loss of life conducted in accordance wi		
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Company White Geotechnical Group Pty Ltd



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#### **GEOTECHNICAL INVESTIGATION:**

New Deck and Gym at 94 Whale Beach Road, Whale Beach

#### 1. Proposed Development

- **1.1** Construct a new deck off the S and E side of the house.
- 1.2 Construct a gym on the downhill side of the property by excavating to a maximum depth of ~2.9m.
- **1.3** Various other minor external alterations and additions.
- Details of the proposed development are shown on 30 drawings prepared by MM+J Architects, project number 2142, drawings numbered EX01 to EX09, and SK01 to SK21, dated 7/12/2021.

#### 2. Site Description

- **2.1** The site was inspected on the 23<sup>rd</sup> November, 2021.
- 2.2 This residential property is on the low side of the road and has a S aspect. It is located on the moderately graded upper reaches of a hillslope. The natural slope falls across the property at an average angle of ~12°. The slope above the property eases to the crest of the hill and the slope below the property continues at similar angles.
- 2.3 At the road frontage, a concrete driveway runs down the slope to a garage underneath the E side of the house (Photo 1). In between the road frontage and the house is a level lawn area (Photo 2). The part-two storey rendered brick house is supported on rendered brick walls and brick piers (Photo 3). The brick walls show no significant signs of movement and the brick piers stand vertical. A cut to create the level platform for the house is supported by a stable ~1.3m high concrete retaining wall (Photo 4). A pool has been cut into the slope on the downhill side of the property (Photo 5). No significant signs of movement were observed in the concrete shell of the



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pool. Immediately below the pool deck, a series of timber log retaining walls reaching

up to ~1.5m in height terrace the slope to the lower common boundary (Photos 6 &

7). Several of these retaining walls are tilting to a maximum angle of ~15°. These

timber log retaining walls are to be demolished and rebuilt as part of the proposed

works. A moderately sloping lawn extends to the lower common boundary (Photo 8).

3. Geology

The Sydney 1:100 000 Geological sheet indicates the contact of the Hawkesbury Sandstone

and the Newport Formation of the Narrabeen Group cuts the property. Given the ground test

results, the Newport Formation of the Narrabeen Group is expected to underlie the proposed

works. This is described as interbedded laminite, shale and quartz to lithic quartz sandstone.

4. Subsurface Investigation

One hand Auger Hole (AH) was put down to identify soil materials. Four Dynamic Cone

Penetrometer (DCP) tests were put down to determine the relative density of the overlying

soil and the depth to weathered rock. The locations of the tests are shown on the site plan

attached. It should be noted that a level of caution should be applied when interpreting DCP

test results. The test will not pass through hard buried objects so in some instances it can be

difficult to determine whether refusal has occurred on an obstruction in the profile or on the

natural rock surface. This is not expected to be an issue for the testing on this site. However,

excavation and foundation budgets should always allow for the possibility that the

interpreted ground conditions in this report vary from those encountered during excavations.

See the appended "Important information about your report" for a more comprehensive

explanation. The results are as follows:

**AUGER HOLE 1** (~RL41.5) – AH1 (Photo 9)

Depth (m) Material Encountered

0.0 to 0.1 FILL, dark brown clayey soil, fine to medium grained, loose, fine trace

of organic matter, dry.



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0.1 to 0.3 **FILL**, orange and brown clay, fine grained, firm, pebbles present throughout, dry.

0.3 to 0.5 **CLAY**, orange, fine grained, firm to stiff, dry.

0.5 to 0.7 **CLAY**, sandy, orange, fine to coarse grained, stiff, dry.

End of test @ 0.7m. No water table encountered.

DCP TEST RESULTS – Dynamic Cone Penetrometer								
Equipment: 9kg har	nmer, 510mm drop, cor	nical tip.	Standard: AS1289.6.3.2 - 1997					
Depth(m) Blows/0.3m	DCP 1 (~RL41.2)	<b>DCP 2</b> (~RL41.5)	DCP 3 (~RL39.5)	<b>DCP 4</b> (~RL44.3)				
0.0 to 0.3	4	4	4	4				
0.3 to 0.6	6	9	9	8				
0.6 to 0.9	9	21	16	11				
0.9 to 1.2	30	29	31	21				
1.2 to 1.5	#	35	38	32				
1.5 to 1.8		#	#	32				
1.8 to 2.1				#				
	Refusal on Rock @ 1.2m	End of Test @ 1.5m	End of Test @ 1.5m	End of Test @ 1.8m				

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

#### **DCP Notes:**

DCP1 – Refusal on rock @ 1.2m, DCP thudding, orange and brown clay on wet tip.

DCP2 – End of test @ 1.5m, DCP still going down slowly, orange clay on dry tip.

DCP3 – End of test @ 1.5m, DCP still going down slowly, orange clay on dry tip.

DCP4 – End of test @ 1.8m, DCP still going down slowly, orange clay on dry tip.

#### 5. Geological Observations/Interpretation

The slope materials are colluvial at the near surface and residual at depth. In the test locations, the ground materials consist of soil and clays. The clays merge into the underlying weathered rock at depths of between ~0.9m to ~1.5m below the current surface. The



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weathered zone is interpreted to be Extremely Low Strength Shale. See Type Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and through the cracks. Due to the slope and elevation of the block, the water table is expected to be many metres below the base of the proposed works.

7. Surface Water

No evidence of significant surface flows were observed on the property during the inspection. Normal sheet wash from the slope above will be intercepted by the street drainage system for Whale Beach Road above.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed above or beside the property. The moderately graded slope that falls across the property and continues below is a potential hazard (Hazard One). The proposed excavation is a potential hazard until retaining walls are in place (Hazard Two). The proposed excavation undercutting the footings for the pool is a potential hazard (Hazard Three).

**RISK ANALYSIS ON THE NEXT PAGE** 



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#### **Risk Analysis Summary**

HAZARDS	Hazard One	Hazard Two	Hazard Three		
TYPE	The moderate slope that falls across the property and continues below failing and impacting on the proposed works.	The excavation for the gym (up to a maximum depth of ~2.9m) collapsing onto the work site before retaining walls are in place.	The proposed excavation for the gym undercutting the foundations of the pool shell causing failure.		
LIKELIHOOD	'Unlikely' (10 <sup>-4</sup> )	'Possible' (10 <sup>-3</sup> )	'Possible' (10 <sup>-3</sup> )		
CONSEQUENCES TO PROPERTY	'Medium' (15%)	'Medium' (20%)	'Medium' (35%)		
RISK TO PROPERTY	'Low' (2 x 10 <sup>-5</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )	'High' (2 x 10 <sup>-3</sup> )		
RISK TO LIFE	9.1 x 10 <sup>-7</sup> /annum	5.9 x 10 <sup>-5</sup> /annum	5.3 x 10 <sup>-5</sup> /annum		
COMMENTS	This level of risk is 'ACCEPTABLE'.	This level of risk to life and property is 'UNACCEPTABLE'. To move risk to 'ACCEPTABLE' levels, the recommendations in <b>Section 13</b> are to be followed.	This level of risk to life and property is 'UNACCEPTABLE'. To move risk to 'ACCEPTABLE' levels, the recommendations in <b>Section 13</b> are to be followed.		

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

#### 9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.

#### 10. Stormwater

The fall is away from the street. The stormwater engineer is to refer to council stormwater policy for suitable options.



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11. Excavations

An excavation to a maximum depth of ~2.9m will be required to create the level platform for

the gym on the downhill side of the property. The excavation is expected to be through soil

and clay with Extremely Low Strength Shale encountered at depths of between 0.9m and

1.5m below the current surface in the area of the proposed works. It is envisaged that

excavations through soil, clay, and Extremely Low Strength Shale can be carried out with an

excavator and bucket.

12. Vibrations

No excessive vibrations will be generated by excavation through soil, sandy clay, and

Extremely Low Strength Shale. Any vibrations generated by a domestic machine and bucket

up to 16 ton carrying out excavation works will be below the threshold limit for infrastructure

or building damage.

13. Excavation Support Advice

The excavation for the proposed gym on the downhill side of the property will reach a

maximum depth of ~2.9m. Allowing for 0.5m of back wall drainage, the setbacks are as

follows:

• Flush with the shell of the existing swimming pool.

• Flush with the SE common boundary.

• ~5.0m from the NW common boundary.

As such, the SE boundary and the shell of the existing swimming pool will lie within the zone

of influence of the proposed excavation. In this instance, the zone of influence is the area

above a theoretical 45° line from the base of the excavation towards the surrounding

structures and boundaries. This line reduces to 30° through the fill and soil.



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To ensure the integrity of the pool structure and the property boundary, ground support will

need to be installed along the SE and uphill sides of the excavation with the support installed

before the excavation commences or in a staged construction.

For ease of construction, it might be desirable to continue the spaced pile wall along the NW

side of the excavation to provide shoring support. Alternatively, the cut face on the NW side

will require the installation of temporary or other permanent shoring installed as the

excavation is progressed so the cut face is not left unsupported.

See the site plan attached for the minimum required extent of the shoring shown in blue.

A spaced piled retaining wall is a suitable method of support. Pier spacing for the wall is

typically ~2.0m but can vary between 1.6 to 2.4m depending on the design. All piers can be

supported by embedment and/or bracing installed as the excavation is lowered. To drill the

pier holes for the wall, a mini piling rig or similar that can excavate through Medium to High

Strength Rock will be required. If a machine of this type is not available, we recommend

carrying out core drilling before the construction commences to confirm the strength of the

rock and to ensure the excavation equipment is capable of reaching the required depths. As

the excavation is lowered in 1.5m lifts, infill sprayed concrete panels or similar are added

between the piers to form the spaced wall. Drainage is installed behind the panels. Upon

completion of the excavation, the piled walls are to be tied into the concrete floor and ceiling

slabs of the gym to provide permanent bracing.

The geotechnical consultant is to inspect the drilling process of the entire first pile and the

ground materials at the base of all pier holes/excavations for ground support purposes.

All excavation spoil is to be removed from site following the current Environmental Protection

Agency (EPA) waste classification guidelines.

14. Retaining Walls

For cantilever or singly-propped retaining walls, it is suggested the design be based on a

triangular pressure distribution of lateral pressures using the parameters shown in Table 1.



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Table 1 – Likely Earth Pressures for Retaining Walls

	Earth Pressure Coefficients						
Unit	Unit weight (kN/m³)		'At Rest' K₀	Passive Pressure 'Ultimate'			
Soil and Residual Clays	20	0.40	0.55	N/A			
Extremely Low Strength Shale	22	0.25	0.35	Kp 2.5 ultimate			

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure, do not account for any surcharge loads, such as that from the pool, and assume retaining walls are fully drained. It should be noted that passive pressure is an ultimate value and should have an appropriate safety factor applied. No passive resistance should be assumed for the top 0.4m to account for any disturbance from the excavation. Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining walls are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e., Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining walls, the likely hydrostatic pressures are to be accounted for in the structural design.

#### 15. Foundations

The proposed gym on the downhill side of the property can be supported on a thickened edge / raft slab with piers taken to Extremely Low Strength Shale where necessary. This ground material is expected to be exposed across the uphill side of the excavation. Where it is not exposed, and where the ground falls away with the slope, piers will be required to maintain



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a uniform bearing material across the structure. The piers will need to be embedded at least

0.5m into the Extremely Low Strength Shale measured from the downhill side of each pier

hole. This ground material is expected at depths of between 0.9m to 1.5m below the current

surface in the area of the proposed works. As such, the required depths of the piered

foundations are expected to be between 1.4m and 2.0m below the current surface measured

from the downhill side of the pier hole.

A maximum allowable bearing pressure of 600kPa can be assumed for footings on Extremely

Low Strength Shale. It should be noted that this material is a soft rock and a rock auger will

cut through it so the builders should not be looking for refusal to end the footings.

As the bearing capacity of clay and shale reduces when it is wet, we recommend the footings

be dug, inspected, and poured in quick succession (ideally the same day if possible). If the

footings get wet, they will have to be drained and the soft layer of wet clay or shale on the

footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible, a sealing

layer of concrete may be added to the footing surface after it has been cleaned.

The proposed deck along the S and E sides of the house is proposed to be supported directly

off the existing concrete slab. The structural adequacy of the existing concrete slab is to be

assessed by the structural engineer.

**NOTE**: If the contractor is unsure of the footing material required, it is more cost-effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over-excavation in clay-like

shaly-rock but can be valuable in all types of geology.

16. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical engineer as being in

accordance with the geotechnical recommendations. On completion, a Form 2B will be

issued. This form is required for the Construction Certificate to proceed.



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17. Inspections

The client and builder are to familiarise themselves with the following required inspections

as well as council geotechnical policy. We cannot provide geotechnical certification for the

owners and Occupation Certificate if the following inspection has not been carried out during

the construction process.

• The geotechnical consultant is to inspect the ground materials while the first pier for

the ground support is being dug to assess the ground strength and to ensure it is in

line with our expectations.

• All finished pier holes for piled wall/excavations for ground support are to be

inspected and measured before concrete is placed.

• All footings are to be inspected and approved by the geotechnical consultant while

the excavation equipment and contractors are still onsite and before steel reinforcing

is placed or concrete is poured.

White Geotechnical Group Pty Ltd.

Ben White M.Sc. Geol., AusIMM., CP GEOL.

Bulut

No. 222757

Engineering Geologist.



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Photo 2



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Photo 3



Photo 4



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Photo 6



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Photo 7



Photo 8



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Photo 9 (Top to Bottom)



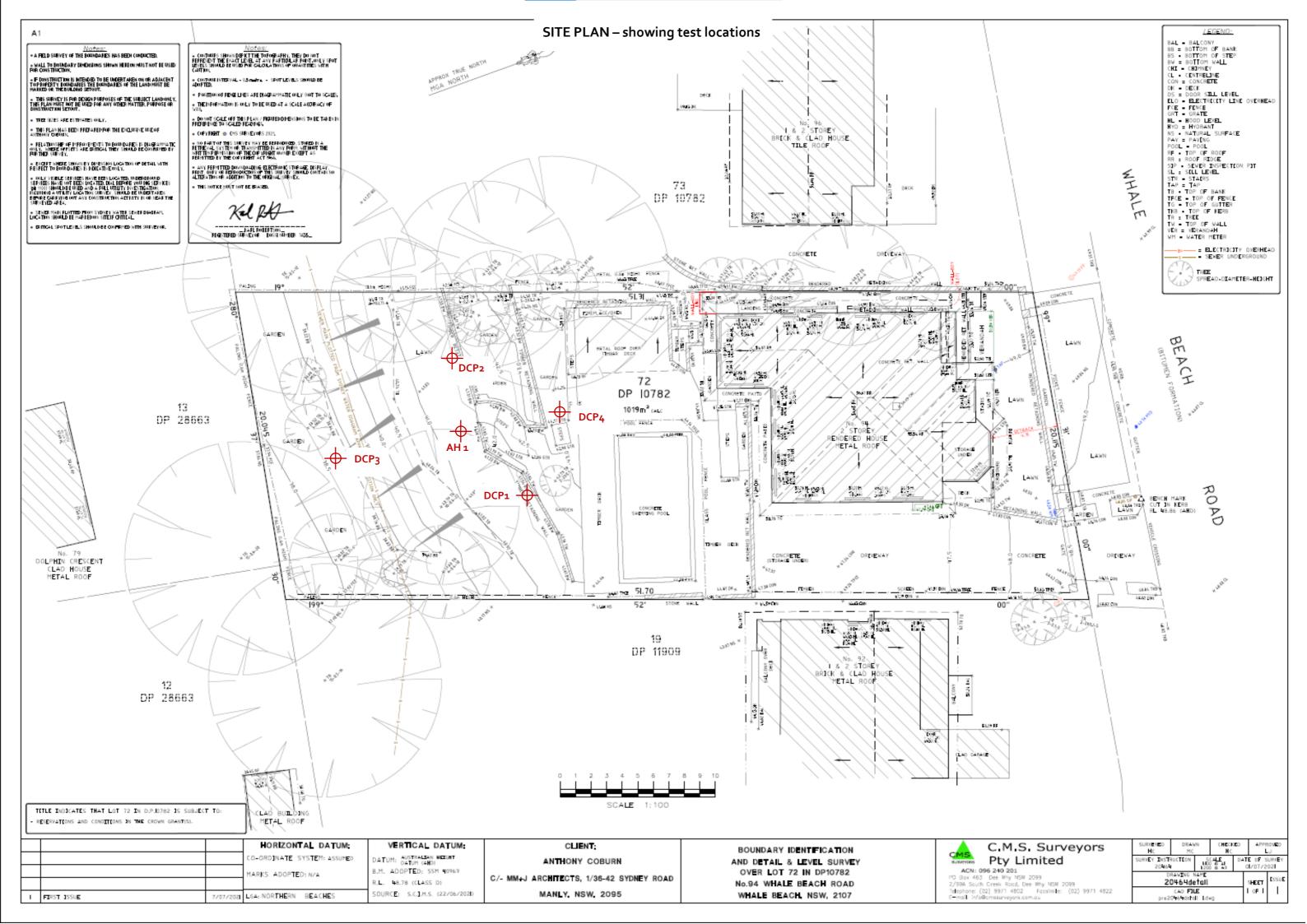
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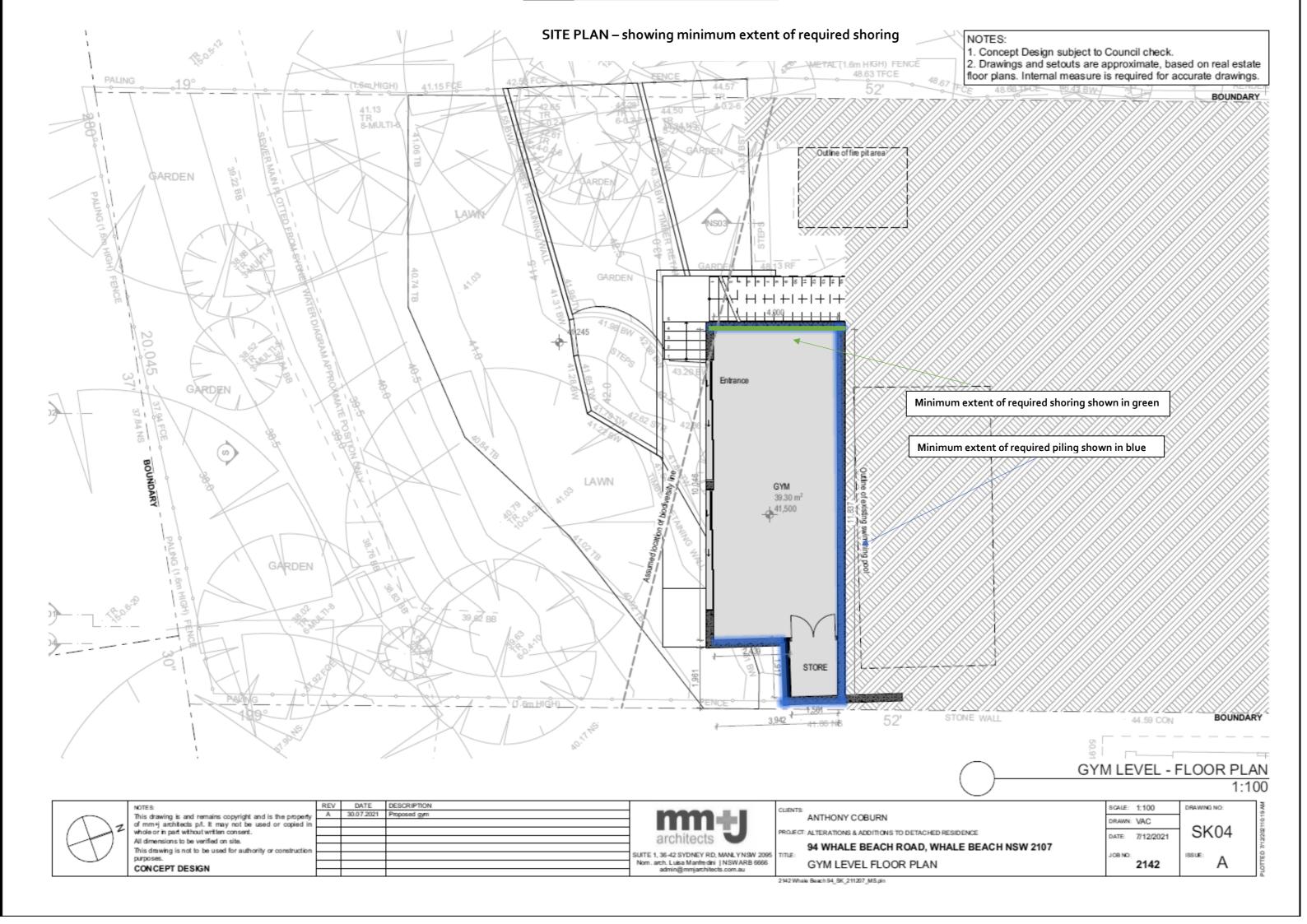
#### Important Information about Your Report

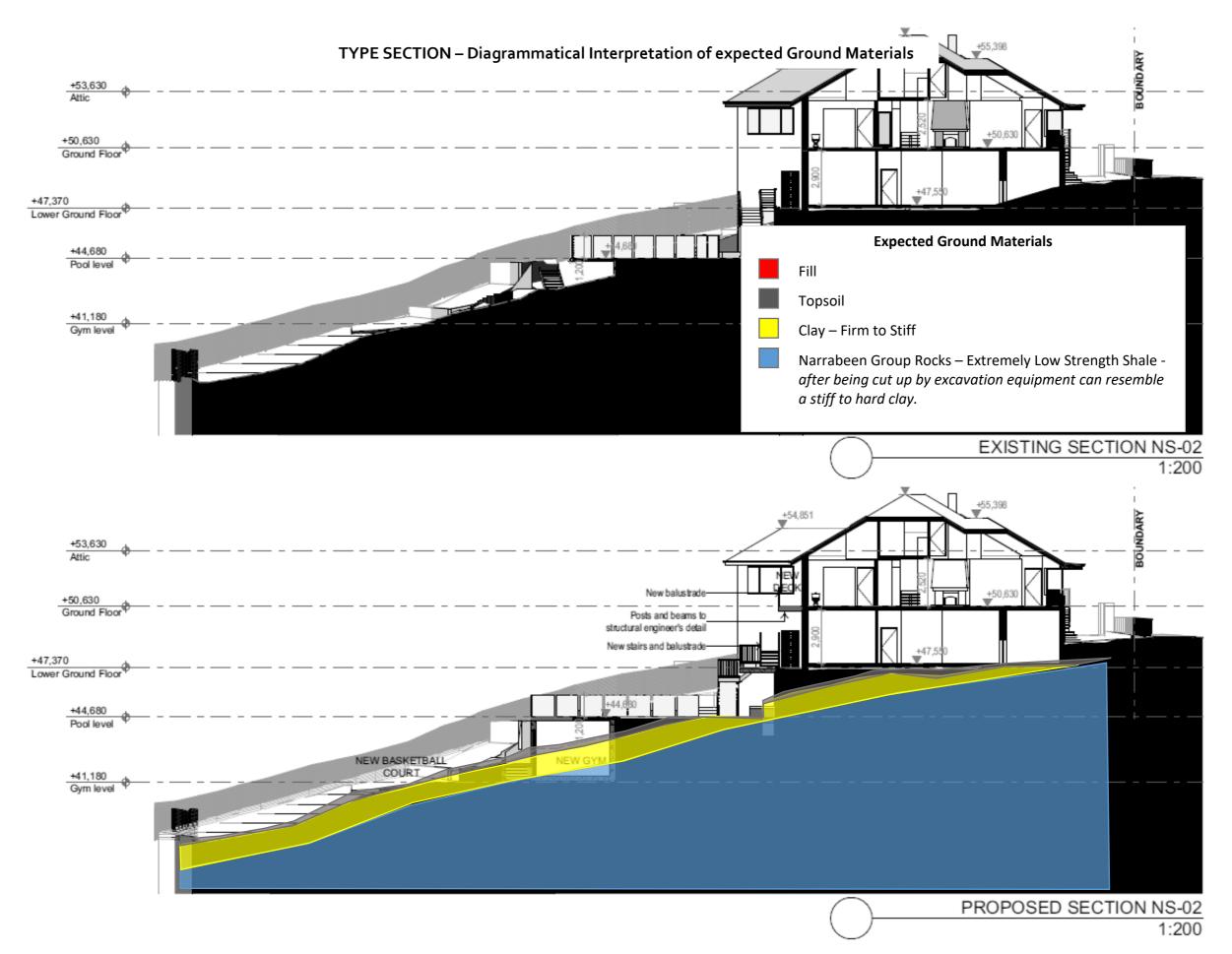
It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.

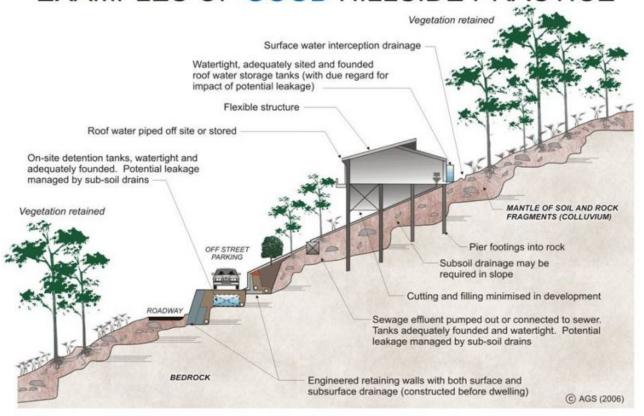






NOTES:	REV	DATE	DESCRIPTION		CLIE	ENTS:	SCALE:	1:200	DRAWING NO:
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of mm+j architects p.fl. It may not be used or copied in whole or in part without written consent.	$\vdash$	<del>                                     </del>			PRO	DJECT: ALTERATIONS & ADDITIONS TO DETACHED RESIDENCE			SK11
All dimensions to be verified on site.				architects	1		DATE:	7/12/2021	SIXTI
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purposes.	$\vdash$	-		Nom. arch. Luisa Manfredini   NSWARB 6666		SECTIONS 03		2142	ISSUE:
CONCEPT DESIGN				admin@mmjarchitects.com.au		3EC110143 03		2142	
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## EXAMPLES OF GOOD HILLSIDE PRACTICE



### EXAMPLES OF POOR HILLSIDE PRACTICE

