GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Development Application for						
			Name of Applica	II		
Address	of site	62 & 64 Powd	erworks Road, North	Narrabeen_		
			uirements to be addresse gist or coastal engineer			
l,	Ben White (Insert Name)	on behalf of	White Geotechni (Trading or Comp	cal Group Pty Ltd any Name)		
organisatio	gineer as defined		certify that I a Il Risk Management Policy nd to certify that the organ		I am authorised by t	he above
: Please ma	ark appropriate b	ох				
			nical Report referenced b nt Guidelines (AGS 2007			
	am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009					
	have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.					
	have examined the Application only	e site and the propo involves Minor De	sed development/alteration velopment/Alteration that in accordance with the German accordance with the	n in detail and I am of the does not require a C	opinion that the Dev Seotechnical Report	or Risk
□ .	have examined the Hazard and does the Geotechnical	not require a Geote Risk Management F	sed development/alteratio chnical Report or Risk As Policy for Pittwater - 2009	sessment and hence my requirements.	Report is in accorda	
	have provided the	coastal process an	d coastal forces analysis	or inclusion in the Geote	chnical Report	
	ical Report Detai					
	Report Title: Geote Report Date: 30/7	•	& 64 Powderworks Ro	oad, North Narrabeer	1	
A	Author: BEN WHI	TE				
A	Author's Company	/Organisation: WHI	TE GEOTECHNICAL GR	OUP PTY LTD		
Documen	tation which rela	te to or are relied	upon in report preparati	on:		
			ociety Landslide Ris		arch 2007	

I am aware that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a Development Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature

Name Ben White

Chartered Professional Status MScGEOL AIG., RPGeo

Membership No. 10306

Company White Geotechnical Group Pty Ltd

White Geotechnical Group company archives.



GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Deve	lopment Application	n for	Niews	- of Annilland	
			Nam	e of Applicant	
	ess of site			Road, North Narral	
Report	t. This checklist is to a	accompany the		be addressed in a Ge ort and its certification	otechnical Risk Management Geotechnical n (Form No. 1).
	chnical Report Detainment Title: Geotechnical		4 Powderwork	s Road, North Nar	raheen
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Repo	ort Date: 30/7/24				
Autho	or: BEN WHITE				
Auth	or's Company/Orga	nisation: WHIT	E GEOTECHNIC	AL GROUP PTY LTD)
Please	e mark appropriate b	юх			
\boxtimes	Comprehensive sit	e mapping condu	ucted 23/7/24 (date)		
\boxtimes	Mapping details pre	esented on conto	oured site plan with	geomorphic mapping t	to a minimum scale of 1:200 (as appropriate)
\boxtimes	Subsurface investig	gation required			
	□ No	Justification_			
_	⊠ Yes	Date conduct			
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	Risk assessment w	ithin Bushfire As	set Protection Zon	e.	
that the	e geotechnical risk ma pement" level for the l	anagement aspetife of the structi	ects of the proposure, taken as at le	al have been adequat	nis checklist applies, as the basis for ensuring lely addressed to achieve an "Acceptable Risk s otherwise stated, and justified in the Report eable risk.
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	Name			Ben White	GEOSCIENTISTS BENJAMIN WHITE
	Chartered Profession	nal Status	MScGEOL	. AIG., RPGeo	世:

222757

White Geotechnical Group Pty Ltd

Membership No.

Company



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GEOTECHNICAL INVESTIGATION:

New House and Driveway at 62 & 64 Powderworks Road, North Narrabeen

1. Proposed Development

- **1.1** Subdivide the lower portion of the existing lots to create a 3rd lot (Proposed lot 2).
- 1.2 Construct a new house on Lot 2 by excavating to a maximum depth of ~5.2m.
- 1.3 Construct a shared driveway from Bellara Avenue to the proposed house by excavating to a maximum depth of ~3.2m.
- 1.4 Details of the proposed development are shown on 11 drawings prepared by Inlet Design Studio, project number BEL001, drawings numbered A001, and A01 to A10, dated 27.5.24.

2. Site Description

- **2.1** The site was inspected on the 23rd July, 2024.
- 2.2 These residential properties are on the high side of the road and have a S aspect. They encompass the moderately graded upper reaches and crest of a NW-SE trending ridgeline. The natural slope rises shortly to the crest of the slope before falling across the properties at an average angle of ~16°. The slopes below the properties increase in grade.
- **2.3** At the road frontages to Powderworks Road, the driveways for 62 & 64 Powderworks Road run up the slopes to their respective houses situated at the crest of the ridgeline (Photos 1 & 2).

The house on 62 Powderworks Road is of timber frame construction and is supported on sandstone block walls (Photo 3). The house on 64 Powderworks Road is dilapidated



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and is to be demolished as part of a separate DA (Photo 4). Some of the walls of both houses were observed to be supported directly on outcropping Medium Strength Sandstone. There are several stack rock / sandstone blocks retaining walls across the two sites that are in various stages of dilapidation (Photo 5, 6, & 7). These will be addressed during the redevelopment of the site. A moderately sloping vegetated bushland area extends from the two houses to their respective lower common boundaries (Photo 8). Medium Strength Sandstone outcrops and steps down the upper portion of the slope immediately below the two existing houses (Photo 9, 10, & 11). The focus of this report is the moderately sloping vegetated bushland area as this is the location of the proposed subdivision and house.

3. Geology

The Sydney 1:100 000 Geological Sheet indicates the contact of the Hawkesbury Sandstone and the Newport Formation of the Narrabeen Group cuts through the site. Given the ground test results, the Newport Formation of the Narrabeen Group is expected to underlie the proposed works. This is described as interbedded laminite, shale and quartz to lithic quartz sandstone.

4. Subsurface Investigation

One hand Auger Hole (AH) was put down to identify soil materials. Four Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil and the depth to weathered rock. The locations of the tests are shown on the site plan attached. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural rock surface. This is not expected to be an issue for the testing on this site. However, excavation and foundation budgets should always allow for the possibility that the interpreted ground conditions in this report vary from those encountered during excavations.



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See the appended "Important information about your report" for a more comprehensive explanation. The results are as follows:

AUGER HOLE 1 (~RL34.0) – AH1 (Photo 12)

Depth (m)	Material Encountered
0.0 to 0.2	TOPSOIL , dark brown clayey soil, medium grained, loose, fine trace of organic matter, dry.
0.2 to 0.7	SAND, clayey, coarse grained, medium dense, dry.
0.7 to 1.6	CLAY, grey, fine grained, stiff, dry.

End of test @ 1.6m. No water table encountered.

DCP TEST RESULTS – Dynamic Cone Penetrometer					
Equipment: 9kg ham	nmer, 510mm drop, cor	Standard: /	Standard: AS1289.6.3.2 - 1997		
Depth(m) Blows/0.3m	DCP 1 (~RL30.0)	DCP 2 (~RL37.5)	DCP 3 (~RL34.0)	DCP 4 (~RL34.5)	
0.0 to 0.3	5	3	3	3	
0.3 to 0.6	4	7	2	8	
0.6 to 0.9	10	16	8	10	
0.9 to 1.2	31	40	13	10	
1.2 to 1.5	#	#	10	12	
1.5 to 1.8			15	31	
1.8 to 2.1			22	#	
2.1 to 2.4			30		
2.4 to 2.7			#		
	End of Test @ 1.2m	End of Test @ 1.2m	End of Test @ 2.4m	End of Test @ 1.8m	

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

DCP Notes:



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DCP1 – End of test @ 1.2m, DCP still going down slowly, red and white shale on dry tip.

DCP2 – End of test @ 1.2m, DCP still going down slowly, red and white shale on dry tip.

DCP3 – End of test @ 2.4m, DCP still going down slowly, white shale on dry tip.

DCP4 – End of test @ 1.8m, DCP still going down slowly, white shale on dry tip.

5. Geological Observations/Interpretation

The slope materials are colluvial at the near surface and residual at depth. In the test locations, the ground materials consist of shallow soils and sands over clays. The clay merges into the underlying weathered rock at depths of between ~1.2m to ~2.1m below the current surface. The weathered zone is interpreted to be Extremely Low Strength Rock. See Type Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and through the cracks. Due to the slope and elevation of the block, the water table is expected to be many metres below the base of the proposed works.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. As the property encompasses the crest of the hill, any surface flows will be generated on the property and will flow away from the property.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed above or beside the property. The moderately graded slope that falls across the property and continues below is a potential hazard (Hazard One). The proposed excavations are a potential hazard until retaining walls are in place (Hazard Two). The proposed fills for the driveway are a potential hazard until retaining walls are in place (Hazard Three).



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Risk Analysis Summary

HAZARDS Hazard One		Hazard Two	Hazard Three	
ТҮРЕ	The moderate slope that falls across the property and continues below failing and impacting on the proposed works.	The excavation for the new house and driveway (up to a maximum depth of ~5.2m) collapsing onto the work site before retaining structures are in place.	The proposed fill for the driveway (up to a maximum height of ~1.2m) failing and impacting the proposed works.	
LIKELIHOOD	'Unlikely' (10 ⁻⁴)	'Possible' (10 ⁻³)	'Possible' (10 ⁻³)	
CONSEQUENCES TO PROPERTY	'Medium' (12%)	'Medium' (15%)	'Medium' (15%)	
RISK TO PROPERTY	'Low' (2 x 10 ⁻⁵)	'Moderate' (2 x 10 ⁻⁴)	'Moderate' (2 x 10 ⁻⁴)	
RISK TO LIFE	8.3 x 10 ⁻⁷ /annum	8.3 x 10 ⁻⁶ /annum	6.0 x 10 ⁻⁵ /annum	
COMMENTS	This level of risk is 'ACCEPTABLE'.	This level of risk to life and property is 'UNNACEPTABLE'. To move risk to 'ACCEPTABLE' levels, the recommendations in Section 13 and 15 are to be followed.	This level of risk to property is 'TOLERABLE. To move risk to 'ACCEPTABLE' levels the recommendations in Section 14 are to be followed.	

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.



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10. Stormwater

The plans show the proposed stormwater run-off from the house are to be piped through an

easement to Nareen Parade. All stormwater or drainage runoff from the proposed house is

to be piped to the easement through any tanks that may be required by the regulating

authorities.

11. Excavations

Two excavations will be required for the proposed development:

• A cut to create a level platform for the house to a maximum depth of 5.2m.

• An excavation to a maximum depth of 3.2m for the proposed driveway.

The excavations are expected to be through soil and sand over clay with Extremely Low

Strength Rock expected at depths of between ~1.2m and ~2.1m. It is envisaged that

excavations through soil, sand, clay, and Extremely Low Strength Rock can be carried out with

an excavator and toothed bucket.

12. Vibrations

No excessive vibrations will be generated by excavation through soil, clay, and Extremely Low

Strength Rock. Any vibrations generated by a domestic machine and bucket up to 20 tonne

carrying out excavation works will be below the threshold limit for infrastructure or building

damage.

13. Excavation Support Requirements

The excavations for the proposed house will reach a maximum depth of ~5.2m. The

excavation for the proposed driveway will reach a maximum depth of ~3.2m. Allowing 0.5m

for back wall drainage, the setbacks from the proposed excavations to the existing

structures/boundaries are as follows:

• Flush with the W common boundary.

• ~3.9m from the E common boundary.



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- ~4.1m from the S common boundary.
- ~9.5m from the proposed N common boundary.

As such, the E and W common boundaries will lie within the zone of influence of the proposed house and driveway excavations. In this instance, the zone of influence is the area above a theoretical 45° line through clay and shale from the base of the excavation towards the surrounding structures and boundaries. This line reduces to 30° through the fill and soil.

Due to the depth of the excavation and its proximity to the common boundaries, we recommend ground support be installed along the sides of the excavations prior to the commencement of the excavations to ensure the safety of any workers below the cut and integrity of the neighbouring properties. See the site plan attached for the minimum required extent of the shoring shown in blue and orange.

Spaced piling will be required along any portion of the house and driveway excavation that is expected to be deeper than 2.0m.

Pier spacing for the wall is typically ~2.0m but can vary between 1.6 to 2.4m depending on the design. To drill the pier holes for the wall, a mini piling rig or similar that can excavate through Medium to High Strength Rock is recommended as the ground testing did not extend to the likely required depth of the piles. If a machine of this type is not available, we recommend carrying out core drilling before the construction commences to confirm the strength of the rock and to ensure the excavation equipment is capable of reaching the required depths. As the excavations are lowered in 1.5m lifts, infill sprayed concrete panels or similar are added between the piers to form the spaced wall. Drainage is installed behind the panels. The piers can be temporarily supported by embedment below the base of the excavations, or by a combination of embedment and temporary propping. Upon completion of the excavations, the piled walls are to be tied into the concrete slabs of the house and driveway to provide permanent bracing.



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Due to the presence of sand in the upper $^{\sim}$ 0.8m of the profile, we recommend extending the

capping beam to at least this depth.

The geotechnical consultant is to inspect the drilling process of the entire first pile and the

ground materials at the base of all pier holes/excavations for ground support purposes.

The portions of the excavations between 1.5m and 2.0m in depth can be supported with

temporary support such as bulka bags until the permanent retaining walls are in place.

Excavations below 1.5m in depth are expected to stand at near-vertical angles for a short

period of time until the permanent retaining walls are in place, provided they are kept from

becoming saturated.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion

works. All unsupported cut batters through fill, soil, and clay are to be covered to prevent

access of water in wet weather and loss of moisture in dry weather. The covers are to be tied

down with metal pegs or other suitable fixtures so they cannot blow off in a storm. The

materials and labour to construct the retaining walls are to be organised so on completion of

the excavations they can be constructed as soon as possible. The excavations are to be carried

out during a dry period. No excavations are to commence if heavy or prolonged rainfall is

forecast.

All excavation spoil is to be removed from site following the current Environmental Protection

Agency (EPA) waste classification guidelines.

14. Fill

For ease of construction, it is recommended the fill under the proposed driveway be used as

formwork only and the driveway foundations be supported on piers taken to the underlying

Extremely Low Strength Rock.

If it is desired to support the driveway on fill, it will need to be laid as an engineered fill. Our

office can be contacted to provide the requirements for these works upon request.



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15. Retaining Walls

For cantilever or singly-propped retaining walls, it is suggested the design be based on a triangular pressure distribution of lateral pressures using the parameters shown in Table 1.

Table 1 – Likely Earth Pressures for Retaining Walls

,	Earth Pressure Coefficients					
Unit	Unit weight (kN/m³)	'Active' K _a	'At Rest' K₀	Passive		
Soil/Sands	20	0.40	0.55	K _p = 3.0 'ultimate'		
Residual Clays	20	0.35	0.45	K _p = 2.0 'ultimate'		
Extremely Low Strength Rock or better	22	0.25	0.38	K _p = 2.5 'ultimate'		

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure, do not account for any surcharge loads, and assume retaining walls are fully drained.

It should be noted that passive pressure is an ultimate value and should have an appropriate safety factor applied. No passive resistance should be assumed for the top 0.4m to account for any disturbance from the excavation.

Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining walls are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e., Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining walls, the likely hydrostatic pressures are to be accounted for in the structural design.



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16. Foundations

The proposed house and driveway can be supported on a thickened edge/raft slab with piers

taken to Extremely Low Strength Shale where necessary. This ground material is expected to

be exposed across the deepest portions of the excavations. Where it is not exposed, and

where this material drops away with the slope, piers will be required to maintain a uniform

foundation material across the structure. This ground material is expected at depths of

between 1.2m to 2.1m below the current surface in the area of the proposed works.

A maximum allowable bearing pressure of 600kPa can be assumed for footings on Extremely

Low Strength Shale. It should be noted that this material is a soft rock and a rock auger will

cut through it so the builders should not be looking for refusal to end the footings.

As the bearing capacity of clay and shale reduces when it is wet, we recommend the footings

be dug, inspected, and poured in quick succession (ideally the same day if possible). If the

footings get wet, they will have to be drained and the soft layer of wet clay or shale on the

footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible, a sealing

layer of concrete may be added to the footing surface after it has been cleaned.

NOTE: If the contractor is unsure of the footing material required, it is more cost-effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over-excavation in clay-like

shaly-rock but can be valuable in all types of geology.

17. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical engineer as being in

accordance with the geotechnical recommendations. On completion, a Form 2B will be

issued. This form is required for the Construction Certificate to proceed.



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18. Inspections

The client and builder are to familiarise themselves with the following required inspections as well as council geotechnical policy. We cannot provide geotechnical certification for the owners and Occupation Certificate if the following inspections have not been carried out during the construction process.

- The geotechnical consultant is to inspect the ground materials while the first pier for the ground support is being dug to assess the ground strength and to ensure it is in line with our expectations.
- All finished pier holes for piled wall/excavations for ground support are to be inspected and measured before concrete is placed.
- All footings are to be inspected and approved by the geotechnical consultant while the excavation equipment and contractors are still onsite and before steel reinforcing is placed or concrete is poured.

White Geotechnical Group Pty Ltd.

Tyler Jay Johns BEng (Civil)(Hons), Geotechnical Engineer. Reviewed By:

Nathan Gardner B.Sc. (Geol. & Geophys. & Env. Stud.) AIG., RPGeo Geotechnical & Engineering.

No. 10307

Engineering Geologist & Environmental Scientist.





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Photo 2



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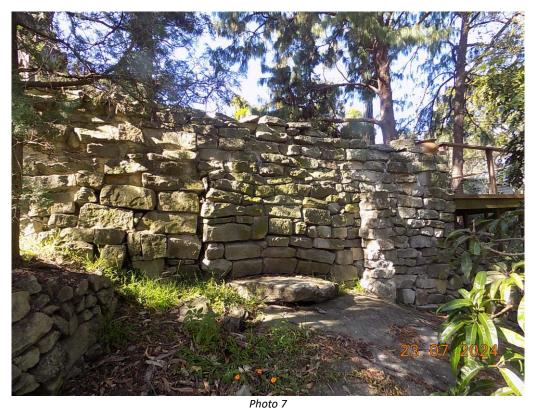




Photo 8



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Photo 11



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Photo 12 (Top to Bottom)



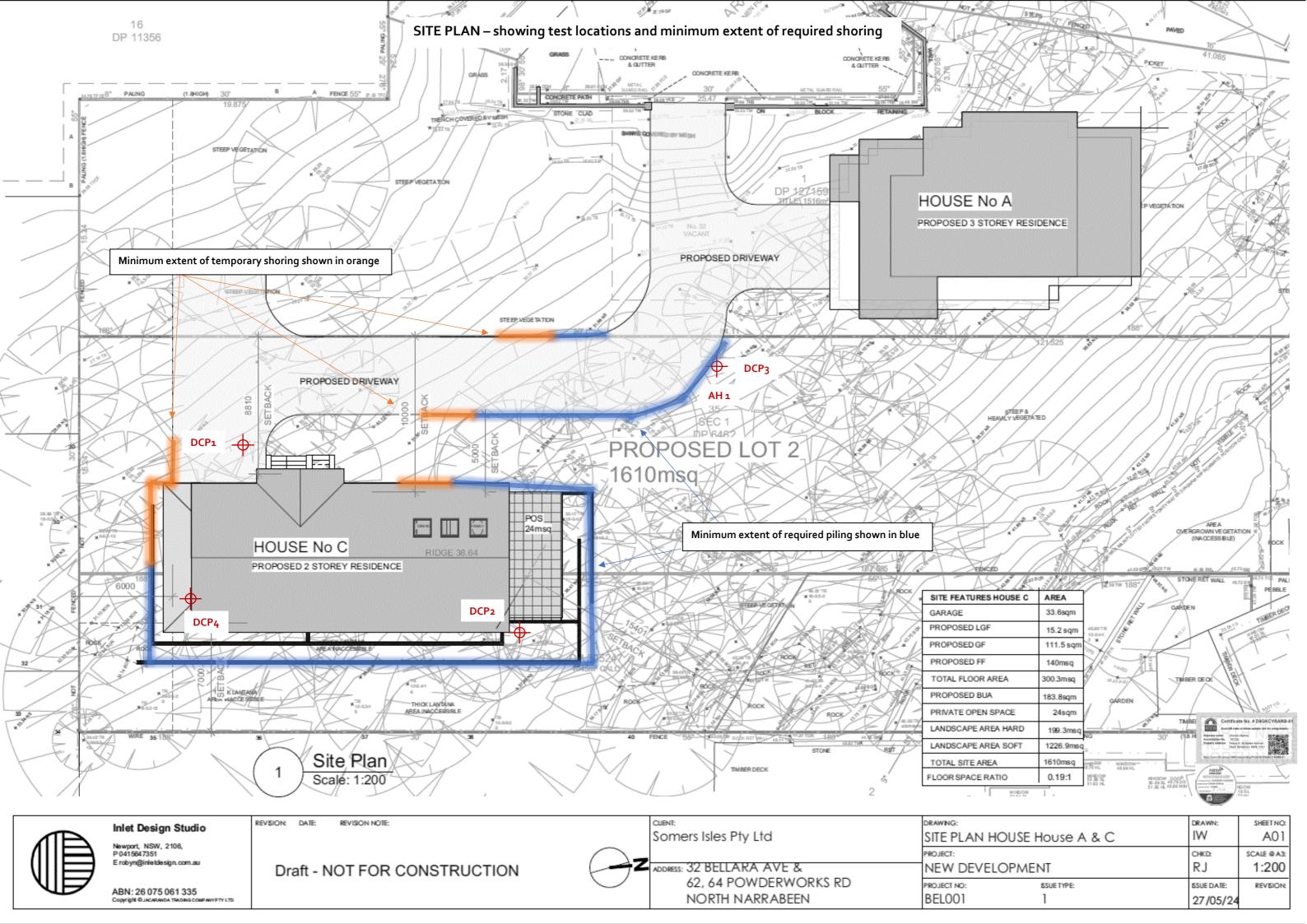
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Important Information about Your Report

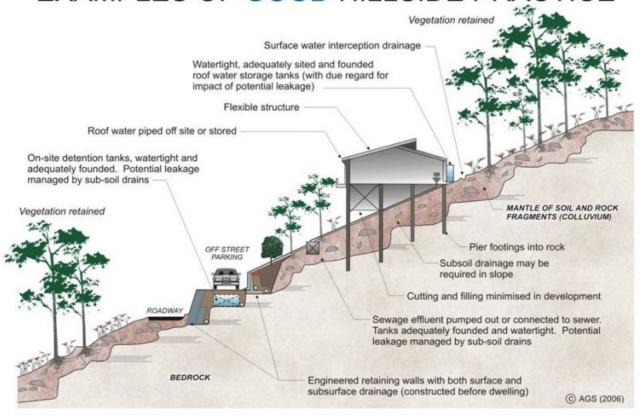
It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any
 questions should be directed to White Geotechnical Group as only we understand the full
 methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.



EXAMPLES OF GOOD HILLSIDE PRACTICE



EXAMPLES OF POOR HILLSIDE PRACTICE

