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#### 11 Coolawin Road, Avalon Beach

Comments on Updates to Plans

We have reviewed the existing geotechnical report, the plans used to carry out the report, and the updated plans for DA shown on 4 drawings prepared by RK Designs, Project number 21-101, sheets numbered 0 to 3, Issue A, dated 1/10/21.

The changes include:

- Relocating the proposed granny flat. This reduces the proposed excavation from ~2.0m to ~0.9m and increases the proposed set back from the upslope retaining wall from close to flush to ~0.4m (allowing for back-wall drainage).
- Various other minor modifications.

Provided the excavation support advice in the original report is followed, the proposed changes do not significantly alter the recommendations or the risk assessment in the report carried out by this firm numbered J3810 and dated the 25<sup>th</sup> October, 2021.

White Geotechnical Group Pty Ltd.

Ben White M.Sc. Geol., AuslMM., CP GEOL.

No. 222757

Engineering Geologist.

#### GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Development Application for Name of Applicant				
Addres	s of site 11 Coolawin Road, Avalon Beach			
	wing checklist covers the minimum requirements to be addressed in a Gonical engineer or engineering geologist or coastal engineer (where a			
l,	Ben White on behalf of White Geotechnical Group (Insert Name) (Trading or Company Name)			
organisa	e 28/10/21 certify that I am a geongineer as defined by the Geotechnical Risk Management Policy for Pitty ion/company to issue this document and to certify that the organisation/cat least \$10million.			
: Please r	nark appropriate box			
$\boxtimes$	have prepared the detailed Geotechnical Report referenced below in Society's Landslide Risk Management Guidelines (AGS 2007) and the Pittwater - 2009			
$\boxtimes$	am willing to technically verify that the detailed Geotechnical Reports accordance with the Australian Geomechanics Society's Landslide Risk Geotechnical Risk Management Policy for Pittwater - 2009			
	have examined the site and the proposed development in detail and have with Section 6.0 of the Geotechnical Risk Management Policy for Pittwa assessment for the proposed development are in compliance with the Pittwater - 2009 and further detailed geotechnical reporting is not require	ater - 2009. I confirm that the results of the risk ne Geotechnical Risk Management Policy for		
	have examined the site and the proposed development/alteration in deta Application only involves Minor Development/Alteration that does Assessment and hence my Report is in accordance with the Geotechnic requirements.	not require a Geotechnical Report or Risk		
	have examined the site and the proposed development/alteration is separated and does not require a Geotechnical Report or Risk Assessme the Geotechnical Risk Management Policy for Pittwater - 2009 requirement Policy for Pittwater - 2009 requireme	nt and hence my Report is in accordance with nents.		
	have provided the coastal process and coastal forces analysis for inclusion	sion in the Geotechnical Report		
Geotech	nical Report Details: Report Title: Geotechnical Report 11 Coolawin Road, Avalon Beac Report Date: 25/10/21	ch		
	Author: BEN WHITE			
	Author's Company/Organisation: WHITE GEOTECHNICAL GROUP PT	Y LTD		
Docume	ntation which relate to or are relied upon in report preparation:			
	Australian Geomechanics Society Landslide Risk Mar	nagement March 2007.		
	White Geotechnical Group company archives.			
Developi Risk Ma	are that the above Geotechnical Report, prepared for the abovementinent Application for this site and will be relied on by Pittwater Council an agement aspects of the proposed development have been adequated ment' level for the life of the structure, taken as at least 100 years unless of	s the basis for ensuring that the Geotechnical y addressed to achieve an "Acceptable Risk		

that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	Bellet
Name	Ben White
Chartered Professional Sta	tus MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Pty Ltd

# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Development Application for				
			Name of Applicant	
Addres	s of site	11 Coolawin Road,	Avalon Beach	
Report. T		company the Geotechnical	ts to be addressed in a Geotechnical Risk Managen I Report and its certification (Form No. 1).	nent Geotechnical
		Report 11 Coolawin Roa	d. Avalon Beach	
		.,		
Report	Date: 25/10/21			
	BEN WHITE			
Author	's Company/Organ	isation: WHITE GEOTECH	HNICAL GROUP PTY LTD	
Please m	nark appropriate bo	x		
$\boxtimes$	Comprehensive site	mapping conducted 18/10/21 (date)		
	Subsurface investiga	ented on contoured site plan tion required Justification	n with geomorphic mapping to a minimum scale of 1:20	0 (as appropriate)
⊠ ⊠	Geotechnical hazard  ⊠ Above  ⊠ On the  □ Below	s identified the site site the site	an inferred subsurface type-section	
	Risk assessment con ⊠ Conse	s described and reported	he Geotechnical Risk Management Policy for Pittwater	- 2009
	Risk calculation	,,		
	Risk assessment for Assessed risks have Management Policy Opinion has been pr	loss of life conducted in accordance been compared to "Acceptation Pittwater - 2009 ovided that the design can accordance be accordance to the conduction of the conducted in accordance of the conduction of t	dance with the Geotechnical Risk Management Policy ordance with the Geotechnical Risk Management Polic ble Risk Management" criteria as defined in the Geotec chieve the "Acceptable Risk Management" criteria prov	y for Pittwater - 2009 chnical Risk
	specified conditions  Design Life Adopted			
	⊠ 100 ye			
	Pittwater - 2009 have Additional action to r	e been specified	phases as described in the Geotechnical Risk Manage e and practical have been identified and included in the n Zone.	
that the g Managen	eotechnical risk mar nent" level for the life	agement aspects of the property of the structure, taken as tical measures have been it	chnical Report, to which this checklist applies, as the oposal have been adequately addressed to achieve at least 100 years unless otherwise stated, and judentified to remove foreseeable risk.	an "Acceptable Risk
		Signature	Selet	
		Name	Ben White	
		Chartered Professional Sta	atus MScGEOLAusIMM CP GEOL	
		Membership No.	222757	

Company White Geotechnical Group Pty Ltd



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#### **GEOTECHNICAL INVESTIGATION:**

New Granny Flat at 11 Coolawin Road, Avalon Beach

#### 1. Proposed Development

- 1.1 Construct a new granny flat on the downhill side of the property by excavating to a maximum depth of ~2.0m into the slope.
- Details of the proposed development are shown on 5 drawings prepared by RK Designs, project number 21-101, sheets numbered 0 to 4, Issue A, dated 1/10/21.

#### 2. Site Description

- **2.1** The site was inspected on the 18<sup>th</sup> October, 2021.
- 2.2 This irregularly-shaped residential property has access from three separate road frontages. It is on the downhill side of The Knoll, is level with Palmgrove Road, and is on the uphill side of Coolawin Road. The property has a NW aspect. It is located on the moderately graded upper reaches of a hillslope. The natural slope rises across the property at an average angle of ~14° before easing to gentle angles near the crest of the slope at The Knoll. The slope below the property gradually eases in grade.
- 2.3 At the road frontage to Palmgrove Road, a gravel driveway runs to a garage under the downhill side of the house (Photos 1 & 2). The fill for the driveway and for a lawn area on the downhill side of the house is supported by a stable mortared sandstone block retaining wall ~1.4m high (Photo 3). Between this wall and the road frontage for Coolawin Road is a gentle to moderate slope with a dense covering of native and exotic grasses and shrubs (Photo 4). The part two-storey rendered masonry and timber framed and clad house is supported on masonry walls (Photo 5). No significant signs of movement were observed in the supporting wall of the house. Between the driveway, house, and road frontage to The Knoll, the slope has been



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terraced with a series of low sandstone flagging walls (Photo 6). The fill for The Knoll is supported by a stable ~0.5m high timber retaining wall that lines the road frontage (Photo 7).

#### 3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by the Newport Formation of the Narrabeen Group. It is described as interbedded laminite, shale and quartz to lithic quartz sandstone.

#### 4. Subsurface Investigation

Four Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil and the depth to weathered rock. The locations of the tests are shown on the site plan attached. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural rock surface. This is not expected to be an issue for the testing on this site. However, excavation and foundation budgets should always allow for the possibility that the interpreted ground conditions in this report vary from those encountered during excavations. See the appended "Important information about your report" for a more comprehensive explanation. The results are as follows:

DCP TEST RESULTS – Dynamic Cone Penetrometer				
Equipment: 9kg hammer, 510mm drop, conical tip. Standard: AS1289.6.3.2 - 19				d: AS1289.6.3.2 - 1997
Depth(m)	DCP 1	DCP 2	DCP 3	DCP 4
Blows/0.3m	(~RL48.8)	(~RL49.7)	(~RL51.2)	(~RL52.6)
0.0 to 0.3	16	27	7	8
0.3 to 0.6	26	50	15	24
0.6 to 0.9	37	#	27	33
0.9 to 1.2	#		#	#
	End of Test @ 0.9m	End of Test @ 0.5m	Refusal on Rock @ 0.9m	End of Test @ 0.9m

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.



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**DCP Notes:** 

DCP1 – End of test @ 0.9m, DCP still very slowly going down, grey and maroon shale on dry tip.

DCP2 – End of test @ 0.5m, DCP still very slowly going down, brown shale on dry tip.

DCP3 – Refusal on rock @ 0.9m, DCP bouncing off rock surface, orange shale fragments on dry tip.

DCP4 – End of test @ 0.9m, DCP still very slowly going down, orange shale on dry tip.

5. Geological Observations/Interpretation

The slope materials are colluvial at the near surface and residual at depth. In the test locations, the ground materials consist of a thin silty soil over firm to hard silty clays. The silty clays merge into the underlying weathered rock at an average depth of ~0.6m below the current surface in the location of the proposed granny flat. The weathered zone is interpreted to be Extremely Low to Very Low Strength Shale. See Type Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and through the cracks. Due to the slope and elevation of the block, the water table is expected to be many metres below the base of the proposed excavation.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. As the property is located immediately below the crest of the hill, any surface flows will be generated immediately above the property and will flow onto the property as The Knoll is not guttered above the subject property.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed below or beside the property. The moderately graded slope that rises across the property and continues below is a potential hazard (Hazard One).



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The proposed excavation collapsing onto the work site before permanent support is in place is a potential hazard (**Hazard Two**). The proposed excavation undercutting the footings of the sandstone block retaining wall is a potential hazard (**Hazard Three**).

#### **Risk Analysis Summary**

HAZARDS	Hazard One	Hazard Two	Hazard Three
ТҮРЕ	The moderately graded slope that rises across the property and continues below is a potential hazard.	The unsupported cut batters of the excavation collapsing onto the work site before permanent support is in place.	The proposed excavation undercutting the footings of the sandstone block retaining wall and causing movement (Photo 3).
LIKELIHOOD	'Unlikely' (10 <sup>-4</sup> )	'Possible' (10 <sup>-3</sup> )	'Possible' (10 <sup>-3</sup> )
CONSEQUENCES TO PROPERTY	'Medium' (12%)	'Medium' (12%)	'Medium' (15%)
RISK TO PROPERTY	'Low' (2 x 10 <sup>-5</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )
RISK TO LIFE	<b>RISK TO LIFE</b> 9.1 x 10 <sup>-7</sup> /annum 5.6 x 10 <sup>-5</sup>		4.8 x 10 <sup>-5</sup> /annum
COMMENTS	This level of risk is 'ACCEPTABLE'.	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk levels to acceptable levels, the recommendations in Section 13 are to be followed.	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk levels to acceptable levels, the recommendations in Section 13 are to be followed.

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)



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9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by

the completion of the proposed development provided it is carried out in accordance with

the requirements of this report and good engineering and building practice.

10. Stormwater

There is fall to Coolawin Road. Roof water from the development is to be piped to the street

drainage system through any tanks that may be required by the regulating authorities.

11. Excavations

An excavation to a maximum depth of ~2.0m is required to construct the proposed granny

flat. It is expected the excavation will be through a thin silty topsoil over a firm to hard clay

and Extremely Low to Very Low Strength Shale.

Excavations through soil, clay, and Extremely Low to Very Low Strength Shale can be carried

out with an excavator and bucket.

12. Vibrations

No excessive vibrations will be generated by excavation through soil, clay, or Extremely Low

to Very Low Strength Shale. Any vibrations generated by a domestic machine and bucket up

to 16 ton will be below the threshold limit for infrastructure or building damage.

13. Excavation Support Requirements

The excavation will reach a maximum depth of ~2.0m and will come flush with the sandstone

block retaining wall below the house (Photo 3). The excavation will be set back sufficiently

from all other surrounding structures and boundaries. As such, the sandstone block retaining

wall will be within the zone of influence of the proposed excavation.



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Where the retaining wall falls within the zone of influence of the excavation, exploration pits in this location will need to be put down by the builder to determine the foundation depth and material. The pits are to be inspected by the geotechnical consultant.

If the wall is found to be supported below the base of the proposed excavation, the excavation may commence. If it is not supported below the base of the proposed excavation, the wall will need to be underpinned prior to the excavation commencing. See the site plan attached showing the minimum extent of the required exploration pits/underpinning.

Underpinning is to follow the underpinning sequence 'hit one miss two'. Under no circumstances is the bulk excavation to be taken to the edge of the wall and then underpinned. Underpins are to be constructed from drives that should be proportioned according to footing type and size. Allowances are to be made for drainage through the underpinning to prevent a build-up of hydrostatic pressure. Underpins that are not designed as retaining walls are to be supported by retaining walls. The void between the retaining walls and the underpinning is to be filled with free-draining material such as gravel.

Where underpinning is not required, the cut batters of the proposed excavation are expected to stand unsupported for a short period until the retaining walls are in place.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion works. Unsupported cut batters are to be covered to prevent access of water in wet weather and loss of moisture in dry weather. The covers are to be tied down with metal pegs or other suitable fixtures so they can't blow off in a storm. The materials and labour to construct the retaining walls are to be organised so on completion of the excavations they can be constructed as soon as possible. The excavations are to be carried out during a dry period. No excavations are to commence if heavy or prolonged rainfall is forecast.

All excavation spoil is to be removed from site following the current Environmental Protection Agency (EPA) waste classification guidelines.



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#### 14. Retaining Walls

For cantilever or singly-propped retaining walls, it is suggested the design be based on a triangular pressure distribution of lateral pressures using the parameters shown in Table 1.

Table 1 - Likely Earth Pressures for Retaining Walls

	Earth Pressure Coefficients			
Unit	Unit weight (kN/m³)	'Active' K <sub>a</sub>	'At Rest' K₀	
Soil and Residual Clays	20	0.40	0.55	
Extremely Low Strength Rock	22	0.25	0.35	
Rock Up to Low Strength Rock	24	0.25	0.35	

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the wall, do not account for any surcharge loads (such as the fill/retaining wall immediately above the proposed cut), and assume retaining walls are fully drained. Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining walls are to have sufficient back-wall drainage and be backfilled immediately behind the wall with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e., Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining walls, the likely hydrostatic pressures are to be accounted for in the structural design.



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15. Foundations

The proposed granny flat can be supported on spread footings and piers taken to Extremely

Low to Very Low Strength Shale. This ground material is expected to be exposed across a

portion of the base of the excavation. Where the slope falls away on the downhill side, this

material is expected at a maximum depth of ~0.6m below the current surface. A maximum

allowable bearing pressure of 600kPa can be assumed for footings on Extremely Low to Very

Low Strength Shale. It should be noted that this material is a soft rock and a rock auger will

cut through it so the builders should not be looking for refusal to end the footings.

As the bearing capacity of clay and shale reduces when it is wet, we recommend the footings

be dug, inspected, and poured in quick succession (ideally the same day if possible). If the

footings get wet, they will have to be drained and the soft layer of wet clay or shale on the

footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible, a sealing

layer of concrete may be added to the footing surface after it has been cleaned.

**NOTE**: If the contractor is unsure of the footing material required, it is more cost-effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over-excavation in clay-like

shaly-rock but can be valuable in all types of geology.

16. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical consultant as being

in accordance with the geotechnical recommendations. On completion, a Form 2B will be

issued. This form is required for the Construction Certificate to proceed.

17. Inspections

The client and builder are to familiarise themselves with the following required inspections

as well as council geotechnical policy. We cannot provide geotechnical certification for the



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regulating authorities or the owner if the following inspections have not been carried out during the construction process.

- The geotechnical consultant is to inspect any test pits dug by the builder to verify foundation depth and material of the existing footings.
- All footings are to be inspected and approved by the geotechnical consultant while the excavation equipment and contractors are still onsite and before steel reinforcing is placed or concrete is poured.

White Geotechnical Group Pty Ltd.

Fellet

Ben White M.Sc. Geol., AusIMM., CP GEOL. No. 222757 Engineering Geologist





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Photo 2



Photo 3



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Photo 4



Photo 5



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Photo 6



Photo 7



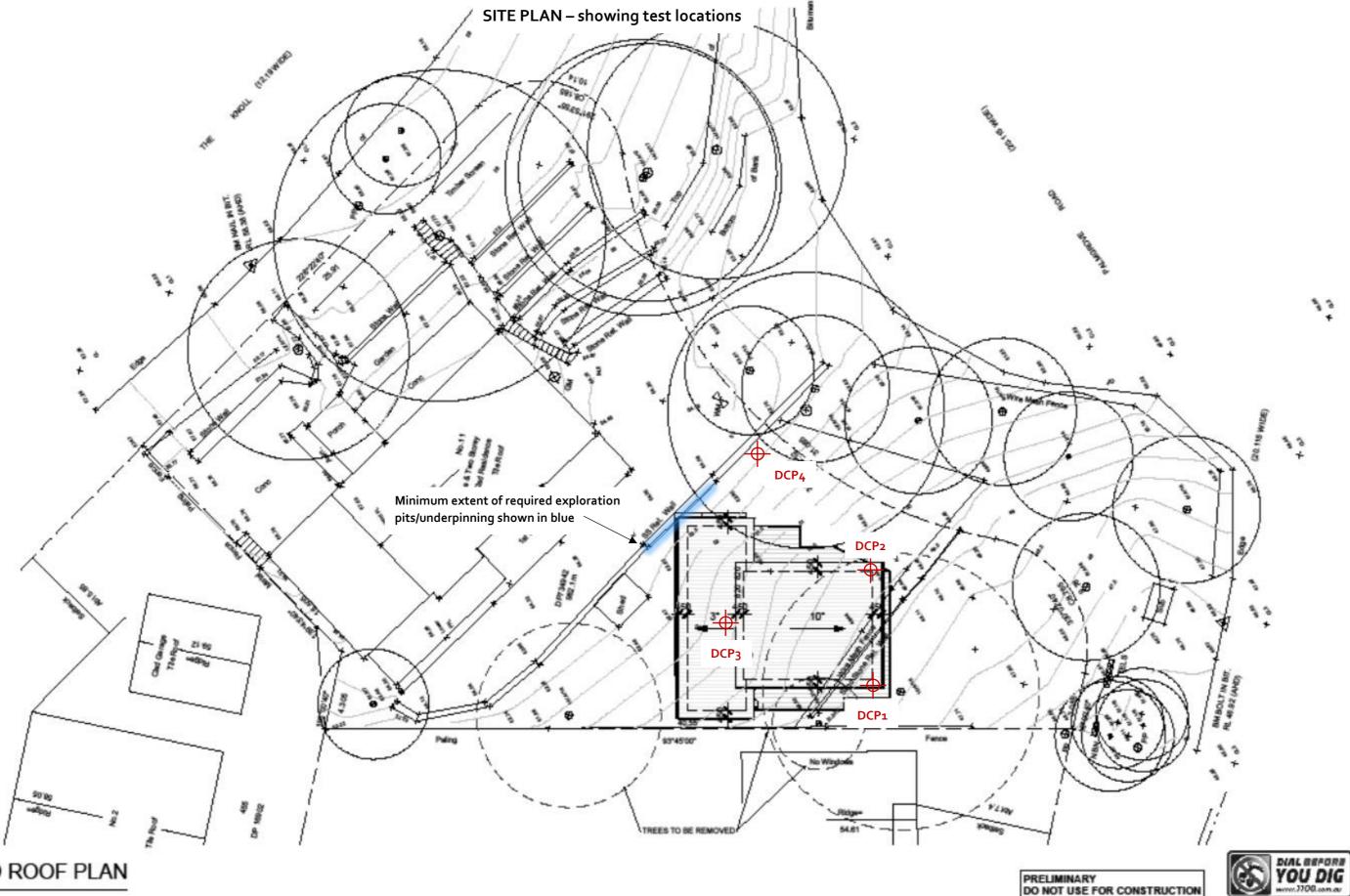
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#### Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any
  questions should be directed to White Geotechnical Group as only we understand the full
  methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.





## SITE AND ROOF PLAN

1:200

settacts are confirmed and used, the boundary settacts take precedence over all other dimensions. The flurwy work must.

In the event of encountering any discrepancies on these dimensions, appetituation or subsequent instructions because, the fluir designer better proceeding further with any work.

All construction, control joints and expansion joints in the wall, floors, other locations shall be in strict accordance with the combinate other than specified, are allowed without written permission from the Engineer.

Measurements for the floorization of secondary components such as, windows, doors, internal frames, structural steel component these documents. Measurements must be taken on alle to suit the work as constructed.

All endeting structures need to be assembled for structural adequacy, and it is the Contractor's responsibility to ensure that a assistable prior to the start of any work.

drawn date Issue amendment EC 01/10/21 A ISSUE FOR DA

PROPOSED CONSTRUCTION OF A GRANNY FLAT AT 11 COOLAWIN ROAD, AVALON BEACH 2107 LOT 2 DP 734942.



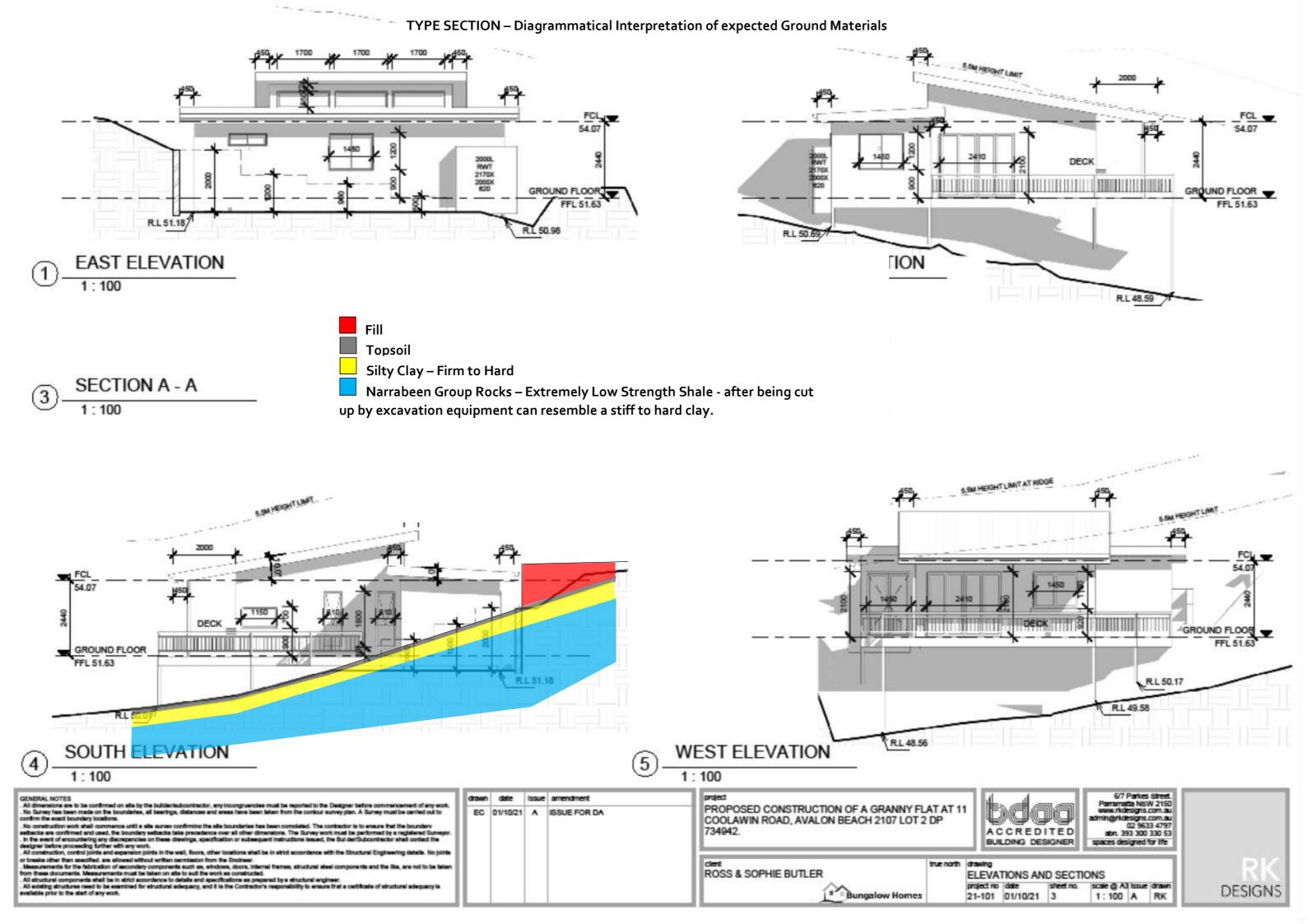
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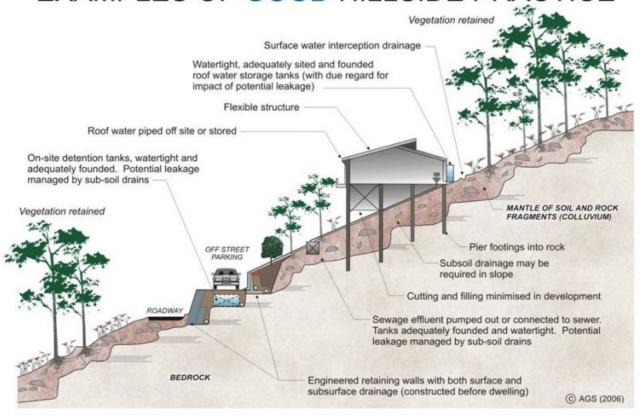


clent ROSS & SOPHIE BUTLER true north drawing Bungalow Homes

SITE AND ROOF PLAN project no date scale @ A3 issue drawn 21-101 01/10/21 1 1:200 A RK



# EXAMPLES OF GOOD HILLSIDE PRACTICE



### EXAMPLES OF POOR HILLSIDE PRACTICE

