GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Development Application for							
		Name of Applicant					
Addr	ess of site	10 Kookaburra Close, Bayview					
The following checklist covers the minimum requirements to be addressed in a Geotechnical Risk Declaration made by geotechnical engineer or engineering geologist or coastal engineer (where applicable) as part of a geotechnical report							
l,	Ben White (Insert Name)	on behalf of <u>White Geotechnical Group Pty Ltd</u> (Trading or Company Name)					

on this the ______28/11/24 certify that I am a geotechnical engineer or engineering geologist or coastal engineer as defined by the Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the above organisation/company to issue this document and to certify that the organisation/company has a current professional indemnity policy of at least \$10million.

I:

Please mark appropriate box

- have prepared the detailed Geotechnical Report referenced below in accordance with the Australia Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
- am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater 2009
- have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.
- have examined the site and the proposed development/alteration in detail and I am of the opinion that the Development Application only involves Minor Development/Alteration that does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
- have examined the site and the proposed development/alteration is separate from and is not affected by a Geotechnical Hazard and does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater 2009 requirements.
- □ have provided the coastal process and coastal forces analysis for inclusion in the Geotechnical Report

Geotechnical Report Details:

Report Title: Geotechnical Report **10 Kookaburra Close, Bayview** Report Date: 28/11/24

Author: **BEN WHITE**

Author's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD

Documentation which relate to or are relied upon in report preparation:

Australian Geomechanics Society Landslide Risk Management March 2007.

White Geotechnical Group company archives.

I am aware that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a Development Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	lut
Name	Ben White
Chartered Professional Sta	tus MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Pty Ltd



GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Deve		
Deve	velopment Application for	
Add	dress of site 10 Kookaburra Close, Bayview	
	following checklist covers the minimum requirements to be addressed in a Geotechnical Risk N ort. This checklist is to accompany the Geotechnical Report and its certification (Form No. 1).	Nanagement Geotechnical
Geote	technical Report Details:	
Repo	port Title: Geotechnical Report 10 Kookaburra Close, Bayview	
Repo	port Date: 28/11/24	
Auth	thor: BEN WHITE	
Auth	thor's Company/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD	
leas	se mark appropriate box	
\triangleleft	Comprehensive site mapping conducted <u>5/8/24</u>	
\mathbf{X}	(date) Mapping details presented on contoured site plan with geomorphic mapping to a minimum scal	e of 1:200 (as appropriate)
\triangleleft	Subsurface investigation required	、
	 □ No Justification □ Yes Date conducted 5/8/24 	
3	Geotechnical model developed and reported as an inferred subsurface type-section	
3	Geotechnical hazards identified	
-	Above the site	
	\boxtimes On the site	
	Below the site	
	□ Beside the site	
\triangleleft	Geotechnical hazards described and reported	
\triangleleft	Risk assessment conducted in accordance with the Geotechnical Risk Management Policy for	Pittwater - 2009
	☑ Consequence analysis	
	☑ Frequency analysis	
\triangleleft	Risk calculation	
3	Risk assessment for property conducted in accordance with the Geotechnical Risk Managemer	•
3	Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Managem	
3	Assessed risks have been compared to "Acceptable Risk Management" criteria as defined in th Management Policy for Pittwater - 2009	e Geotechnical Risk
3	Opinion has been provided that the design can achieve the "Acceptable Risk Management" crit specified conditions are achieved.	eria provided that the
3	Design Life Adopted:	
	⊠ 100 years	
	Other specify	
3	Geotechnical Conditions to be applied to all four phases as described in the Geotechnical Risk	Management Policy for
3		

I am aware that Pittwater Council will rely on the Geotechnical Report, to which this checklist applies, as the basis for ensuring that the geotechnical risk management aspects of the proposal have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated, and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	l	il.
Name		Ben White
Chartered Professional St	atus	MScGEOLAusIMM CP GEOL
Membership No.		222757
Company	White	Geotechnical Group Pty Ltd





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GEOTECHNICAL INVESTIGATION:

Alterations and Additions at **10 Kookaburra Close, Bayview**

1. Proposed Development

- **1.1** Construct a new suspended driveway and garage with entryway, lift, and plant/storage below by excavating to a maximum depth of ~1.3m.
- **1.2** Add a new first floor addition to the existing house.
- **1.3** Extend the ground floor of the existing house on the downhill side and over the existing patio at the W corner of the house.
- **1.4** Various other minor internal and external alterations and additions.
- 1.5 Details of the proposed development are shown on 36 drawings prepared by Eoin Architects, project number 2401, drawings numbered DA001, DA002, DA003.1, DA003.2, DA004.1, DA004.2, DA005, DA006, DA101 to DA106, DA201 to DA207, DA301, DA302, DA601, DA602.1, DA602.2, DA603.1, DA603.2, DA604.1, DA604.2, DA605, DA606, DA608 to DA610 and DA700, Issue L, dated 2/9/24.

2. Site Description

2.1 The site was inspected on the 5th August, 2024, and previously on the 7th September, 2018.

2.2 This residential property is on the low side of the road and has a NE aspect. It is located on the steeply graded middle reaches of a hillslope. The natural slope falls across the property at an average angle of ~29°. The slope above the property continues at steep angles for some 50m before decreasing in grade. The slope below the property continues at steep angles for some 70m before decreasing in grade.

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2.3 At the road frontage, a concrete driveway runs to a carport on the uphill side of the property (Photo 1). Fill to an unknown depth provides a level platform for the downhill side for the carport, entry pathway, and road reserve. The fill batter merges into the natural steep moderately-vegetated slope at the uphill side of the house (Photo 2). The SE side of the house has been terraced with a series of treated timber retaining walls. The uppermost wall is ~1.0m high and is tilting downslope significantly (Photo 3). See '**Section 16** Ongoing Maintenance'. The part two storey house is supported on brick walls (Photos 4 & 5). The external supporting walls show no significant signs of movement. A timber balcony with deck below extends off the downhill side of the house (Photo 5). The posts that support the balcony and deck stand vertical. The slope underneath and beside the deck has been terraced with a series of timber retaining walls is tilting downslope significantly (Photos 7 & 8). See '**Section 16** Ongoing Maintenance'.

3. Geology

The Sydney 1:100 000 Geological Sheet indicates the site is underlain by Hawkesbury Sandstone, although the Narrabeen Groups Rocks are shown close to the downhill side of the property and at a residential scale the map is not always accurate. Ground testing and observations of the slope geomorphology indicate the property is underlain by the Newport Formation of the Narrabeen Group. This is described as interbedded laminite, shale, and quartz to lithic quartz sandstone.

4. Subsurface Investigation

One hand Auger Hole (AH) was put down to identify the soil materials. Five Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density of the overlying soil and the depth to weathered rock. The locations of the tests are shown on the site plan attached. It should be noted that a level of caution should be applied when interpreting DCP test results. The test will not pass through hard buried objects so in some instances it can be

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difficult to determine whether refusal has occurred on an obstruction in the profile or on the natural rock surface. This is expected to have occurred for DCPs 1 & 3. Due to the possibility that the actual ground conditions vary from our interpretation there should be allowances in the excavation and foundation budget to account for this. We refer to the appended "Important Information about Your Report" to further clarify. The results are as follows:

AUGER HOLE 1 (~RL52.9) – AH1 (Photo 9)

Depth (m)	Material Encountered
0.0 to 0.6	FILL, sandy soil and clay, with some rock fragments, dark brown, brown, orange, moist, fine to coarse grained.
0.6 to 1.0	TOPSOIL , sandy soil and silty sand, dark brown, brown, damp, fine to medium grained.
1.0 to 1.2	CLAY , light orange brown, grey, maroon, mottled, stiff, moist.

End of hole @ 1.2m in stiff clay. No water table encountered.

DCP TEST RESULTS – Dynamic Cone Penetrometer								
Equipment:	9kg hammer, 51	Standard: AS1	.289.6.3.2 -1997					
Depth(m) Blows/0.3m	DCP 1 (~RL55.3)	DCP 2 (~RL52.9)	DCP 3 (~RL53.0) 8 12 #	DCP 4 (~RL50.1)	DCP 5 (~RL43.8)			
0.0 to 0.3	F	12 10		5	9			
0.3 to 0.6	3F			7	7 14			
0.6 to 0.9	4	7		5				
0.9 to 1.2	#	14		18	51			
1.2 to 1.5		14		20	#			
1.5 to 1.8		43		22				
1.8 to 2.1		#		14				
2.1 to 2.4				#				
	Refusal @ 0.9m	Refusal on Rock @ 1.8m	Refusal @ 0.6m	Refusal on Rock @ 1.9m	End of Test @ 1.1m			

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

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DCP Notes:

DCP1 – Refusal @ 0.9m, DCP bouncing, white impact dust and dark brown soil on moist tip. DCP2 – Refusal on Rock @ 1.8m, DCP bouncing off rock surface, maroon and white shale fragments on moist tip.

DCP3 – Refusal @ 0.6m, DCP bouncing, white impact dust and brown soil on dry tip.

DCP4 – Refusal on Rock @ 1.9m, DCP bouncing off rock surface, orange brown clay and dark brown soil on damp tip.

DCP5 – End of Test @ 1.1m, DCP still very slowly going down, maroon clay and dark brown soil on moist tip.

5. Geological Observations/Interpretation

The slope materials are colluvial at the near surface and residual at depth. In the test locations, the ground materials consist of fill and a thin sandy topsoil over Firm to Very Stiff Clays. Fill to an estimated maximum depth of ~1.5m provides level platforms for the road reserve, the carport, and for garden and paved areas across the property. In the test locations, the clays merge into the weathered zone of the underlying rock at depths of between ~0.9m to ~1.9m below the current surface, being deeper in the filled areas and slightly variable due to a variable weathering profile. The weathered zone of the underlying rock is interpreted as Extremely Low to Low Strength Rock. It is to be noted that this material is a soft rock and can appear as a mottled stiff clay when it is cut up by excavation equipment. See Type Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Ground water seepage is expected to move over the denser and less permeable clay and weathered rock layers in the sub-surface profile. Due to the slope and elevation of the block, the water table is expected to be many metres below the base of the proposed works.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. It is expected that normal sheet wash will move onto the site from above the property during heavy down pours. If the owners know, or become aware in the future, that overland flows

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enter the property during heavy prolonged rainfall events our office is to be informed so appropriate drainage measures can be recommended and installed. It is a condition of the slope stability assessment in Section 8 (**Hazard One**) that this be done.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed beside the property. The steeply graded slope that falls across the property and continues above and below is a potential hazard (**Hazard One**). The proposed excavation is a potential hazard until retaining structures are in place (**Hazard Two**).

HAZARDS	Hazard One	Hazard Two
ТҮРЕ	The steep slope that falls across the property and continues above and below failing and impacting on the property.	The proposed excavation for the plantroom/storage and lift collapsing onto the worksite during the excavation process.
LIKELIHOOD	'Unlikely' (10 ⁻⁴)	'Possible' (10 ⁻³)
CONSEQUENCES TO PROPERTY	'Medium' (12%)	'Medium' (15%)
RISK TO PROPERTY	'Low' (2 x 10 ⁻⁵)	'Moderate' (2 x 10 ⁻⁴)
RISK TO LIFE	8.3 x 10 ⁻⁷ /annum	3.7 x 10 ⁻⁵ /annum
COMMENTS	This level of risk is 'ACCEPTABLE', provided the recommendations in Sections 7 & 16 are carried out.	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk to 'ACCEPTABLE' levels, the recommendations in Section 13 are to be followed.

Geotechnical Hazards and Risk Analysis - Risk Analysis Summary

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.



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10. Stormwater

The fall is away from the street. The stormwater engineer is to refer to council stormwater policy for suitable options.

11. Excavations

An excavation to a maximum depth of ~1.3m will be required to construct the proposed plantroom/storage and lift. The excavation is expected to be through fill, topsoil, and clay.

Excavations through fill, soil, and clay are expected to be carried out with an excavator and toothed bucket.

12. Vibrations

It is expected the proposed excavation will be carried out with an excavator and toothed bucket and the vibrations produced will be below the threshold limit for building or infrastructure damage using a domestic sized excavator up to 16 tonne.

13. Excavation Support Requirements

An excavation to a maximum depth of ~1.3m will be required to construct the proposed plantroom/storage and lift. The excavation is set back sufficiently from the surrounding structures and property boundaries. But due to the steep grade of the slope, the excavation will need to be temporarily or permanently supported prior to the commencement of the excavation, or during the excavation process in a staged manner, so cut batters are not left unsupported. The support will need to be designed by the structural engineer. See the site plan attached for the minimum extent of the required shoring shown in blue.

During the excavation process, the geotechnical consultant is to inspect the cut face in 1.5m intervals as it is lowered to ensure ground materials are as expected and that additional support is not required.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion works. The materials and labour to construct the retaining walls are to be organised so on



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completion of the excavation they can be constructed as soon as possible. The excavation is to be carried out during a dry period. No excavations are to commence if heavy or prolonged rainfall is forecast.

All excavation spoil is to be removed from site following the current Environmental Protection Agency (EPA) waste classification guidelines.

14. Retaining Structures

For cantilever or singly propped retaining structures it is suggested the design be based on a triangular distribution of lateral pressures using the parameters shown in Table 1.

	Earth Pressure Coefficients				
Unit	Unit weight (kN/m³)	'Active' K _a	'At Rest' K₀		
Fill and Topsoil	20	0.40	0.55		
Residual Clays	20	0.35	0.45		

Table 1 – Likely Earth Pressures for Retaining Structures

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region".

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure and do not account for any surcharge loads, noting that surcharge loads from the slope above will be acting on the wall. It also assumes retaining structures are fully drained. Ground materials and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

All retaining structures are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e. Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in



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retaining structures the full hydrostatic pressures are to be accounted for in the retaining structure design.

15. Foundations

The proposed additions are to be supported on piers taken to and embedded no less than 1.0m into Extremely Low Strength Rock or better. This ground material is expected at depths of between ~0.9m to ~2.7m below the current surface, being deeper in the filled areas and slightly variable due to a variable weathering profile. A maximum allowable bearing pressure of 600kPa can be assumed for footings embedded in Extremely Low Strength Rock or better. It should be noted that this material is a soft rock and a rock auger will cut through it so the builders should not be looking for refusal to end the footings.

The foundations supporting the existing house are currently unknown. Ideally, footings should be founded on the same footing material across the old and new portions of the structure. Where the footing material does change across the structure construction joints or similar are to be installed to prevent differential settlement, where the structure cannot tolerate such movement in accordance with a 'Class M' site.

As the bearing capacity of weathered rock reduces when it is wet we recommend the footings be dug, inspected and poured in quick succession (ideally the same day if possible). If the footings get wet, they will have to be drained and the soft layer of weathered rock on the footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible a sealing layer of concrete may be added to the footing surface after it has been cleaned and inspected.

NOTE: If the contractor is unsure of the footing material required it is more cost effective to get the geotechnical professional on site at the start of the footing excavation to advise on footing depth and material. This mostly prevents unnecessary over excavation in clay like shaly rock but can be valuable in all types of geology.



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16. Ongoing Maintenance

The tilting timber retaining walls (Photos 3 & 7) are be monitored by the owners on an annual basis or after heavy and prolonged rainfall events, whichever occurs first. A photographic record of these inspections is to be kept. Should further movement occur the walls are to be remediated or replaced so that they meet current engineering standards.

Where slopes are steep and approach or exceed 30°, such as on this site, it is prudent for the owners to occasionally inspect the slope (say annually or after heavy and prolonged rainfall events, whichever occurs first). Should any of the following be observed: movement or cracking in retaining walls, cracking in any structures, cracking or movement in the slope surface, tilting or movement in established trees, leaking pipes, or newly observed flowing water, or changes in the erosional process or drainage regime, then a geotechnical consultant should be engaged to assess the slope.

The risk assessment in **Section 8** is subject to this ongoing maintenance being carried out. We can carry out these inspections upon request.

17. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical engineer as being in accordance with the geotechnical recommendations. On completion, a Form 2B will be issued. This form is required for the Construction Certificate to proceed.

REQUIRED INSPECTIONS ON NEXT PAGE



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18. Inspections

The client and builder are to familiarise themselves with the following required inspections as well as council geotechnical policy. We cannot provide geotechnical certification for the Occupation Certificate if the following inspections have not been carried out during the construction process.

- During the excavation process, the geotechnical consultant is to inspect the cut face in 1.5m intervals as it is lowered to ensure ground materials are as expected and that additional support is not required.
- All footings are to be inspected and approved by the geotechnical consultant while the excavation equipment and contractors are still onsite and before steel reinforcing is placed or concrete is poured.

White Geotechnical Group Pty Ltd.

Julan

Dion Sheldon BEng(Civil)(Hons), Geotechnical Engineer.

Reviewed By:

wordnes

Nathan Gardner B.Sc. (Geol. & Geophys. & Env. Stud.) AIG., RPGeo Geotechnical & Engineering. No. 10307 Engineering Geologist & Environmental Scientist.



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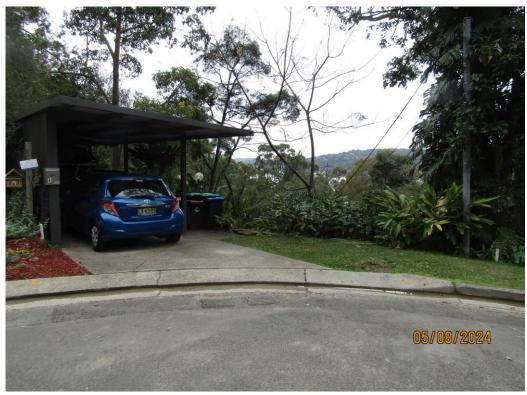


Photo 1



Photo 2

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Photo 3



Photo 4

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Photo 5



Photo 6

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Photo 7



Photo 8

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Photo 9: AH1 – Downhole is from top to bottom.



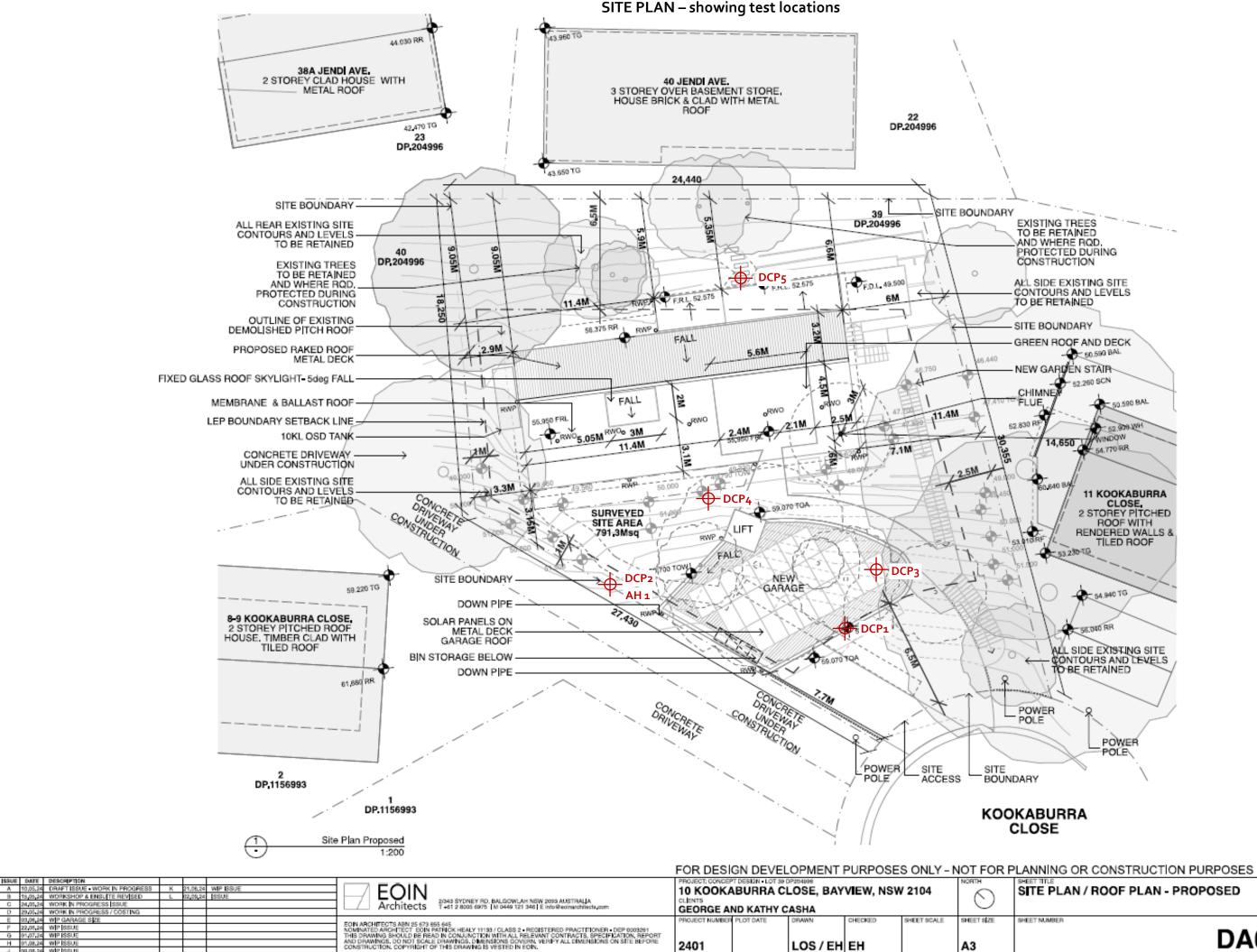
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Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.



2401

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ISSUE DATE DESCRIPTION

H 01.08.24 WIPISSUE J 09.06.24 WIPISSUE

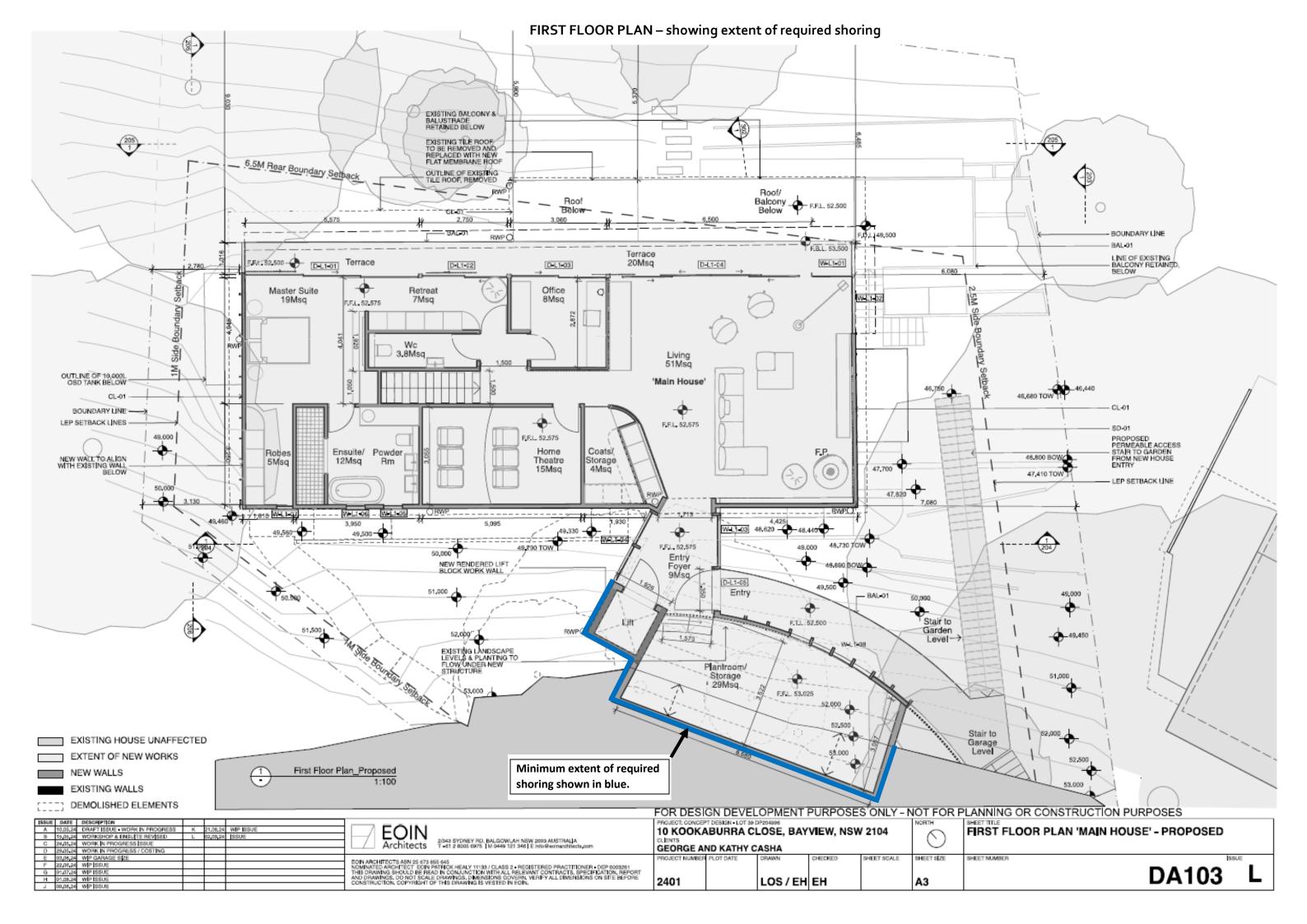
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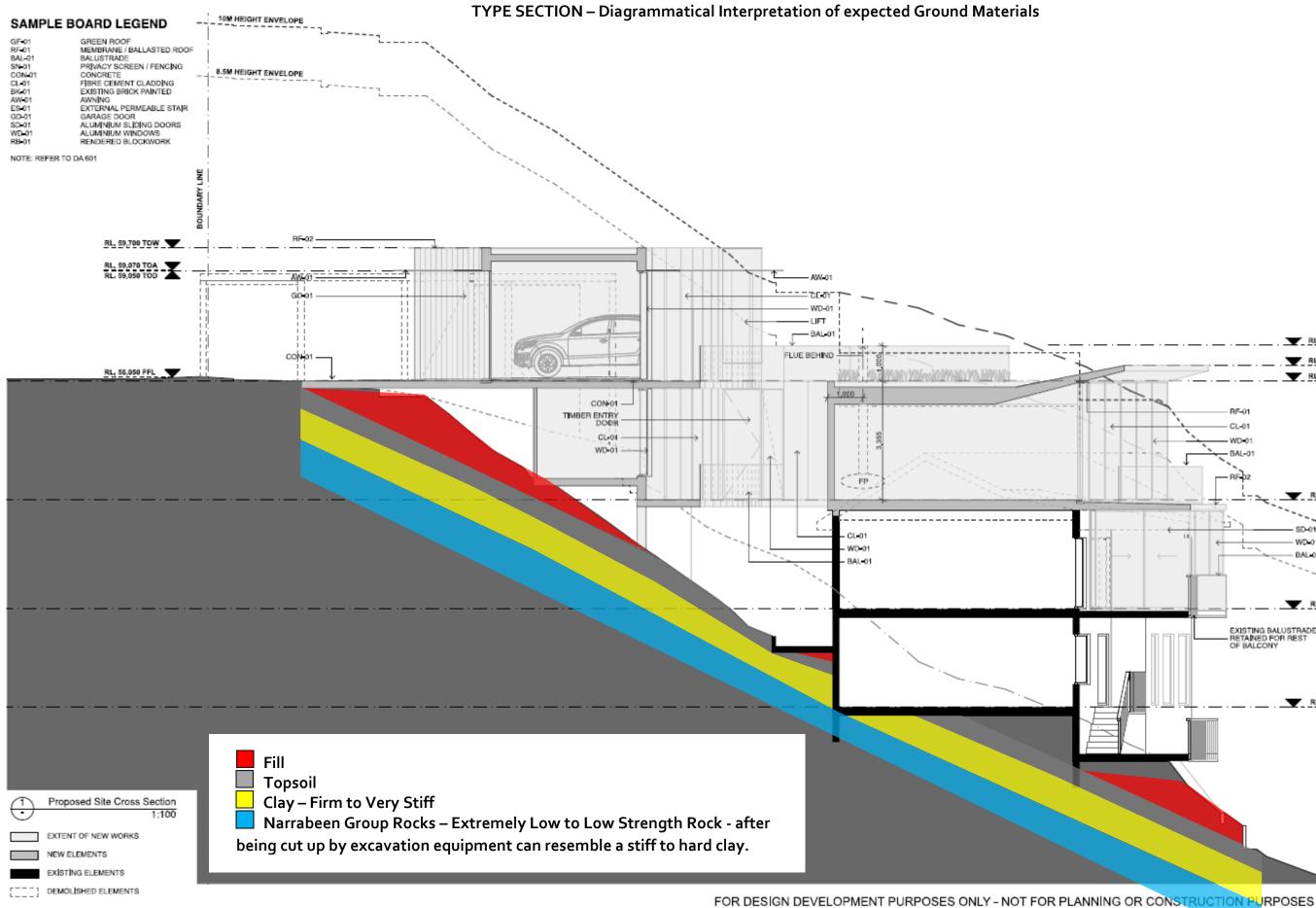
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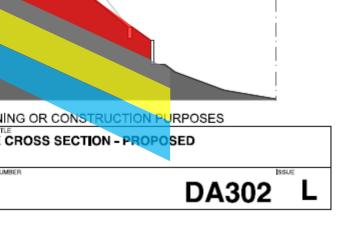
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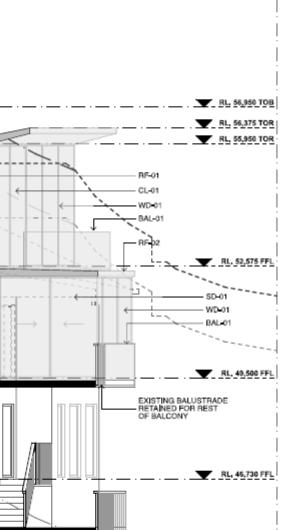
SITE PLAN / ROOF PLAN - PROPOSED



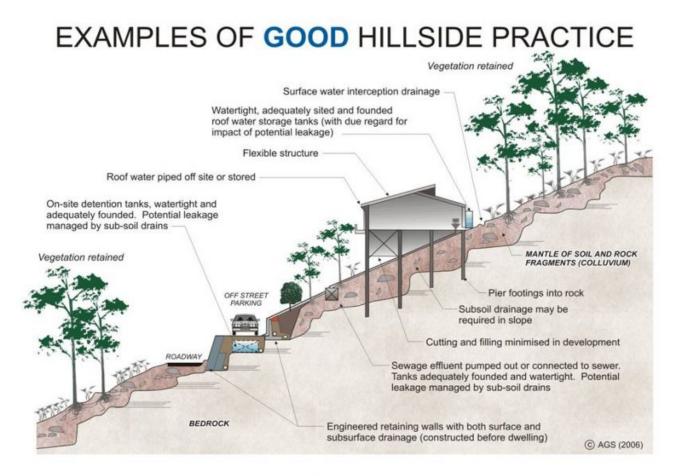


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EXAMPLES OF **POOR** HILLSIDE PRACTICE

