# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Devel	opment Application	n forName of Applicant			
		··			
Address of site 197 McCarrs Creek Road, Church Point					
		ers the minimum requirements to be addressed in a Geotechnical Risk <b>Declaration made by</b> engineering geologist or coastal engineer (where applicable) as part of a geotechnical reports	ort		
l,	Ben White (Insert Name)	on behalf of White Geotechnical Group Pty Ltd (Trading or Company Name)			
organisa	engineer as defined	certify that I am a geotechnical engineer or engineering geologis. I by the Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the absue this document and to certify that the organisation/company has a current professional indeminant.	ove		
: Please	mark appropriate b	рох			
$\boxtimes$		ne detailed Geotechnical Report referenced below in accordance with the Australia Geomechande Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy			
$\boxtimes$	am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009				
	have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.				
	have examined th Application only Assessment and I	he site and the proposed development/alteration in detail and I am of the opinion that the Development involves Minor Development/Alteration that does not require a Geotechnical Report or R hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 20	Risk		
	Hazard and does	ne site and the proposed development/alteration is separate from and is not affected by a Geotechnic not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance v Risk Management Policy for Pittwater - 2009 requirements.			
		e coastal process and coastal forces analysis for inclusion in the Geotechnical Report			
Geotec	nnical Report Deta	ills:			
	Report Title: Geote Report Date: 15/9	echnical Report 197 McCarrs Creek Road, Church Point 3/22			
	Author: BEN WH	ITE			
	Author's Company	y/Organisation: WHITE GEOTECHNICAL GROUP PTY LTD			
Docum	entation which rela	ate to or are relied upon in report preparation:			
	Australian Ge	eomechanics Society Landslide Risk Management March 2007.			
	White Geoted	chnical Group company archives.			
Develop	ment Application fo	e Geotechnical Report, prepared for the abovementioned site is to be submitted in support of this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnic of the proposed development have been adequately addressed to achieve an "Acceptable R	ical		

Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

3	Elect
Signature	
Name	Ben White
Chartered Professional State	us MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Ptv Ltd

# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Develo	pment Application for	or		
		Na	ame of Applicant	
Addres	s of site	197 McCarrs Creek Ro	oad, Church Point	
Report. 7	This checklist is to acc	company the Geotechnical R	o be addressed in a Geotechnical Risk Mana eport and its certification (Form No. 1).	agement Geotechnical
Report	nical Report Details:	: eport 197 McCarrs Creek	Road Church Point	
Report	Title. Geoleciiileai Te	port 137 modal13 dicer	ricad, Ondron'r Onic	
Report	Date: 15/9/22			
	BEN WHITE			
Author	's Company/Organis	sation: WHITE GEOTECHN	ICAL GROUP PTY LTD	
Please m	nark appropriate box	1		
$\boxtimes$	Comprehensive site n	napping conducted 18/5/22 (date)		
$\boxtimes$	Mapping details prese	(/	ith geomorphic mapping to a minimum scale of	1:200 (as appropriate)
	Subsurface investigat	ion required		
	□ No	Justification		
	⊠ Yes	Date conducted 18/5/22	nferred subsurface type-section	
	Geotechnical hazards		mened subsurface type-section	
	⊠ Above t	he site		
	⊠ On the s	site		
	⊠ Below to			
_	☐ Beside t			
		described and reported	Contachnical Diels Management Delies for Ditte	2000
	_	uence analysis	Geotechnical Risk Management Policy for Pitty	vater - 2009
		ncy analysis		
$\boxtimes$	Risk calculation	ioy analysis		
$\boxtimes$	Risk assessment for p	property conducted in accordan	nce with the Geotechnical Risk Management Po	olicy for Pittwater - 2009
$\boxtimes$	Risk assessment for I	oss of life conducted in accord	lance with the Geotechnical Risk Management	Policy for Pittwater - 2009
$\boxtimes$			Risk Management" criteria as defined in the G	eotechnical Risk
	Management Policy for		ava tha "Assautable Diek Managament" suitavia	musicials at the states
$\boxtimes$	specified conditions a	_	eve the "Acceptable Risk Management" criteria	provided that the
$\boxtimes$	Design Life Adopted:	io domovod.		
	⊠ 100 yea	irs		
	☐ Other _			
	0	specify	described in the Ocean bridge Birth Mar	
	Pittwater - 2009 have		ases as described in the Geotechnical Risk Mar	nagement Policy for
$\boxtimes$		•	and practical have been identified and included i	in the report.
		in Bushfire Asset Protection Z	•	·
that the g Managen	eotechnical risk mana nent" level for the life	agement aspects of the propo of the structure, taken as a	nical Report, to which this checklist applies, osal have been adequately addressed to ach t least 100 years unless otherwise stated, a ntified to remove foreseeable risk.	ieve an "Acceptable Risk
		X	celet	
	9	Signature		
	1	Name	Ben White	
	<u>(</u>	Chartered Professional Statu	s MScGEOLAusIMM CP GEOL	
	1	Membership No.	222757	

Company White Geotechnical Group Pty Ltd



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#### **GEOTECHNICAL INVESTIGATION:**

New Extension, Deck, Swim Spa & Spa at 197 McCarrs Creek Road, Church Point

#### 1. Proposed Development

- **1.1** Construct a lower floor extension to the uphill side of the house.
- 1.2 Install a swim spa and a spa on the N side of the property by excavating to a maximum depth of ~1.2m.
- **1.3** Construct a deck off the downhill side of the house.
- **1.4** Various other minor internal alterations and additions.
- **1.5** Details of the proposed development are shown on 14 drawings prepared by Action Plans, drawings numbered DA03 to DA16, dated 15.6.22.

#### 2. Site Description

- **2.1** The site was inspected on the 18<sup>th</sup> May, 2022.
- 2.2 This residential property is on the high side of the road and has an E aspect. It is located on the steeply graded middle reaches of a hillslope. The natural slope falls from the Right of Carriageway (ROW) at an average angle of ~22°. The slope above and below the property continues at similar angles.
- 2.3 The property is accessed by a ROW off the uphill side of the road. The cut for the ROW is supported by large dimensioned sandstone boulders (Photo 1). A concrete driveway diverts off the downhill side of the ROW to a suspended carport on the uphill side of the property (Photo 2). In between the ROW frontage and the house is a steeply sloping embankment (Photo 3). The toe of the slope has been cut vertically to heights of up to some ~0.8m. See Section 16 for advice regarding this cut. The two-storey clad house is steel framed and supported on steel posts. The steel posts appear to stand



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vertical. Several large boulders are embedded in the slope in stable positions (Photo

4). A level lawn area extends off the N side of the house to the N boundary. The fill for

the level lawn area is supported by a stable ~1.2m high stack rock retaining wall and a

stable ~1.2m high timber retaining wall (Photo 5). The retaining walls and lawn area

are to be demolished as part of the proposed works. A steeply sloping lawn area

extends from the downhill side of the house to the lower boundary (Photo 6). The

lower two-thirds of the property is densely vegetated and was unable to be assessed

in terms of stability (Photo 7 & 8).

3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by the Newport

Formation of the Narrabeen Group. This is described as interbedded laminite, shale and

quartz to lithic quartz sandstone.

4. Subsurface Investigation

One exposed cut batter was logged to identify soil materials. Five Dynamic Cone

Penetrometer (DCP) tests were put down to determine the relative density of the overlying

soil and the depth to weathered rock. The locations of the tests are shown on the site plan

attached. It should be noted that a level of caution should be applied when interpreting DCP

test results. The test will not pass through hard buried objects so in some instances it can be

difficult to determine whether refusal has occurred on an obstruction in the profile or on the

natural rock surface. This is not expected to be an issue for the testing on this site. However,

excavation and foundation budgets should always allow for the possibility that the

interpreted ground conditions in this report vary from those encountered during excavations.

See the appended "Important information about your report" for a more comprehensive

explanation. The results are as follows:

**GROUNDTEST RESULTS ON THE NEXT PAGE** 



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#### **EXPOSED CUT BATTER** (~RL66.2) – AH1 (Photo 9)

Depth (m)	Material Encountered
0.0 to 0.2	TOPSOIL, dark brown clayey soil, medium grained, loose, fine trace of
	organic matter, dry.
0.2 to 0.5	Colluvium, orange, fine grained, dry.
0.5 to 0.7	FLOATER, fine grained sandstone.

DCP TEST RESULTS – Dynamic Cone Penetrometer							
Equipment: 9kg	Equipment: 9kg hammer, 510mm drop, conical tip. Standard: AS1289.6.3.2 - 1997						
Depth(m) Blows/0.3m	DCP 1 (~RL63.5)	DCP 2 (~RL63.5)	<b>DCP 3</b> (~RL66.2)	<b>DCP 4</b> (~RL66.2)	DCP 5 (~RL66.2)		
0.0 to 0.3	1F	2	2	1	1		
0.3 to 0.6	1	3	3	5	4		
0.6 to 0.9	4	6	5	7	7		
0.9 to 1.2	8	9	8	13	12		
1.2 to 1.5	12	14	14	20	18		
1.5 to 1.8	27	18	22	29	25		
1.8 to 2.1	36	28	31	35	31		
2.1 to 2.4	#	36	#	#	#		
2.4 to 2.7		#					
	End of Test @ 2.1m	End of Test @ 2.4m	End of Test @ 2.1m	End of Test @ 2.1m	End of Test @ 2.1m		

#refusal/end of test. F=DCP fell after being struck showing little resistance through all or part of the interval.

#### **DCP Notes:**

DCP1 – End of test @ 2.1m, DCP still going down slowly, orange and white clay on damp tip.

DCP2 – End of test @ 2.4m, DCP still going down slowly, orange and white clay on damp tip.

DCP3 – End of test @ 2.1m, DCP still going down slowly, orange clay on damp tip.

DCP4 – End of test @ 2.1m, DCP still going down slowly, brown clay on damp tip.

DCP5 – End of test @ 2.1m, DCP still going down slowly, orange clay on damp tip.



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5. Geological Observations/Interpretation

The slope materials are colluvial to depths of at least ~0.8m under the driveway and house.

This colluvium on the uphill side of the house is unsupported and battered at angles of 30°+.

In the test locations, the ground materials consist of fill and soil over clays. The clay merges

into the underlying weathered rock at depths of between ~1.5m to ~1.8m below the current

surface. The weathered zone is interpreted to be Extremely Low Strength Shale. See Type

Section attached for a diagrammatical representation of the expected ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and

through the cracks. Due to the slope and elevation of the block, the water table is expected

to be many metres below the base of the proposed works.

7. Surface Water

Minor scour channels had been cut into the topsoil above the drainage pipe below the house

(Photo 10) and under the house.

As the weather on the east coast is modelled to become more extreme in the future, on steep

slopes such as this, it is recommended that a dish drain at least 0.5m be installed. This is to

be installed behind the proposed retaining wall across the uphill side of the house. Any pits

and piping to direct flows to the stormwater system for the road are to be oversized (min.

150mm \( \varnothing \) pipe) and designed to cope with extreme rainfall events. The drain is to be designed

by a stormwater/civil engineer in consultation with the geotechnical consultant. It is a

condition of the risk assessment in **Section 8** that this be done.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed beside the property. The steeply graded slope that

falls across the property and continues above and below is a potential hazard (Hazard One).

The proposed excavations are a potential hazard until retaining walls are in place



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(Hazard Two). The unsupported fill batter under the driveway is a potential hazard (Hazard Three).

#### **Risk Analysis Summary**

HAZARDS	Hazard One	Hazard Two	Hazard Three
TYPE	The steep slope that falls across the property and continues above and below failing and impacting on the proposed works.	The excavation for the proposed swim spa and spa (up to a maximum depth of ~1.2m) collapsing onto the work site before retaining structures are in place.	The large unsupported colluvial slope under the driveway failing and impacting on the subject house.
LIKELIHOOD	'Unlikely' (10 <sup>-4</sup> )	'Possible' (10 <sup>-3</sup> )	'Possible' (10 <sup>-3</sup> )
CONSEQUENCES TO PROPERTY	'Medium' (15%)	'Medium' (15%)	'Medium' (30%)
RISK TO PROPERTY	'Low' (2 x 10 <sup>-5</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )	'Moderate' (4 x 10 <sup>-4</sup> )
RISK TO LIFE	9.1 x 10 <sup>-7</sup> /annum	8.3 x 10 <sup>-6</sup> /annum	8.3 x 10 <sup>-6</sup> /annum
COMMENTS	This level of risk is 'ACCEPTABLE', provided the recommendations in Section 7 & 16 are followed.	This level of risk to property is 'UNNACEPTABLE'. To move risk to 'ACCEPTABLE' levels, the recommendations in  Section 13 and 14 are to be followed.	This level of risk to property is 'UNNACEPTABLE'. To move risk to 'ACCEPTABLE' levels, the recommendations in Section 16 are to be followed.

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

#### 9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.



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10. Stormwater

The fall is to McCarrs Creek Road. If the land between the subject property and the road is

council land or owned by another government department, stormwater from the proposed

and existing development is to be piped to the street drainage system through any tanks that

may be required by the regulating authorities.

If the land between the subject property and the road is privately owned, the stormwater

from the proposed and existing development can be piped down the slope to a level spreader

system located 3m above the lower boundary. The spreader system is to be at least ~6m in

length and run perpendicular to the slope.

Pipe diameter for the stormwater should be oversized to cope with extreme rainfall events

(minimum 150mm  $\emptyset$ ).

11. Excavations

An excavation to a maximum depth of ~1.2m is required to install the proposed spa. The

excavation is expected to be through shallow soil over clay with Extremely Low Strength Shale

expected at depths of between ~1.5m and ~1.8m. It is envisaged that excavations through

soil, clay, and Extremely Low Strength Shale can be carried out with an excavator and bucket.

12. Vibrations

No excessive vibrations will be generated by excavation through soil, clay, and Extremely Low

Strength Shale. Any vibrations generated by a domestic machine and bucket up to 16 ton

carrying out excavation works will be below the threshold limit for infrastructure or building

damage.

13. Excavation Support Advice

The excavation for the proposed swim spa and spa will reach a maximum depth of ~1.2m. The

setbacks are as follows:



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~2.2m from the uphill boundary.

As such, no structures or boundaries are expected to lie within the zone of influence of the

excavation.

The sides of the proposed swim spa and spa excavation are expected to stand at near-vertical

angles for short periods of time until the swim spa and spa structures are installed, provided

the cut batters are kept from becoming saturated. If the cut batters through fill, soil, and clay

remain unsupported for more than a few days before swim spa construction commences,

they are to be supported with typical swim spa shoring until the swim spa structure is in place.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion

works. Unsupported cut batters through fill, soil, and clay are to be covered to prevent access

of water in wet weather and loss of moisture in dry weather. The covers are to be tied down

with metal pegs or other suitable fixtures so they can't blow off in a storm. The materials and

labour to construct the swim spa/spa structures are to be organised so on completion of the

excavation they can be constructed as soon as possible. The excavation is to be carried out

during a dry period. No excavations are to commence if heavy or prolonged rainfall is forecast.

All excavation spoil is to be removed from site following the current Environmental Protection

Agency (EPA) waste classification guidelines.

14. Retaining Structures

For cantilever or singly-propped retaining structures, it is suggested the design be based on a

triangular pressure distribution of lateral pressures using the parameters shown in Table 1.

**TABLE 1 ON THE NEXT PAGE** 



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Table 1 – Likely Earth Pressures for Retaining Structures

,	Earth Pressure Coefficients				
Unit	Unit weight (kN/m³)	'Active' K <sub>a</sub>	'At Rest' K₀		
Soil, and Residual Clays	20	0.35	0.45		
Extremely Low Strength Shale	22	0.3	0.25		

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the structure, do not account for any surcharge loads, and assume retaining structures are fully drained. Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.

NOTE: If the proposed swim spa is not designed to retain the slope above, a retaining wall will need to be built.

All retaining structures are to have sufficient back-wall drainage and be backfilled immediately behind the structure with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e., Bidim A34 or similar), to prevent the drainage from becoming clogged with silt and clay. If no back-wall drainage is installed in retaining structures, the likely hydrostatic pressures are to be accounted for in the structural design.

#### 15. Foundations

As the proposed swim spa and spa are of fiberglass construction, it will be required that they be supported on a concrete slab with shallow piers taken to and embedded ~0.6m into the underlying Extremely Low Strength Shale.



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The proposed deck and extension are also to be supported on piers taken to and embedded

at least ~0.6m into the underlying Extremely Low Strength Shale from the downhill side of the

foundation.

This material is expected at depths of between 1.5m to 1.8m below the current surface in the

area of the proposed works. As such, the required depths of the piered foundations are

expected to be between 2.1m and 2.4m below the current surface measured from the

downhill side of the pier hole.

A maximum allowable bearing pressure of 600kPa can be assumed for footings on Extremely

Low Strength Shale. It should be noted that this material is a soft rock and a rock auger will

cut through it so the builders should not be looking for refusal to end the footings.

As the bearing capacity of clay and shale reduces when it is wet, we recommend the footings

be dug, inspected, and poured in quick succession (ideally the same day if possible). If the

footings get wet, they will have to be drained and the soft layer of wet clay or shale on the

footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible, a sealing

layer of concrete may be added to the footing surface after it has been cleaned.

**NOTE**: If the contractor is unsure of the footing material required, it is more cost-effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over-excavation in clay-like

shaly-rock but can be valuable in all types of geology.

16. Remedial Works / Site Maintenance

A) The steep unsupported fill batter underneath the driveway requires a retaining wall

constructed across the toe of the slope to prevent and limit failure. This wall is to be built

some ~0.4m higher than the slope level to 'catch' any localised soil movement. The wall is to

be designed by a structural engineer to cope with surcharge loads from the steep slope above.



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B) To reduce the likelihood of future slope failure, a dish drain at least 0.5m in diameter is to

be installed. This is to be installed behind the retaining wall proposed above. Any pits and

piping to direct flows to the stormwater system for the road are to be oversized (min. 150mm

ø pipe) and designed to cope with extreme rainfall events. The drain is to be designed by a

stormwater/civil engineer in consultation with the geotechnical consultant.

C) Any stormwater from the proposed and existing development is to be piped to the street

drainage system through council land. If the area is not council land, a level spreader system

is to be used. See Section 10 for more details. Pipe diameter for the stormwater should be

oversized to cope with extreme rainfall events (minimum 150mm  $\emptyset$ ).

D) Where slopes approach or exceed 20°, such as on this site, it is prudent for the owners to

occasionally inspect the slope (say annually or after heavy rainfall events, whichever occurs

first). Should any of the following be observed: movement or cracking in retaining walls,

cracking in any structures, cracking or movement in the slope surface, tilting or movement in

established trees, leaking pipes, or newly observed flowing water, or changes in the erosional

process or drainage regime, then a geotechnical consultant should be engaged to assess the

slope. We can carry out these inspections upon request. The risk assessment in **Section 8** is

subject to this site maintenance being carried out.

17. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical engineer as being in

accordance with the geotechnical recommendations. On completion, a Form 2B will be

issued. This form is required for the Construction Certificate to proceed.

18. Inspection

The client and builder are to familiarise themselves with the following required inspection as

well as council geotechnical policy. We cannot provide geotechnical certification for the

owners and Occupation Certificate if the following inspection has not been carried out during

the construction process.



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 All footings are to be inspected and approved by the geotechnical consultant while the excavation equipment and contractors are still onsite and before steel reinforcing is placed or concrete is poured.

White Geotechnical Group Pty Ltd.

Ben White M.Sc. Geol., AuslMM., CP GEOL.

Feelect

No. 222757

Engineering Geologist.



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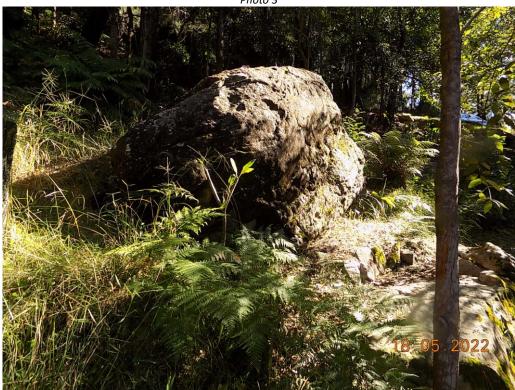


Photo 2



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Photo 5



Photo 6



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Photo 8



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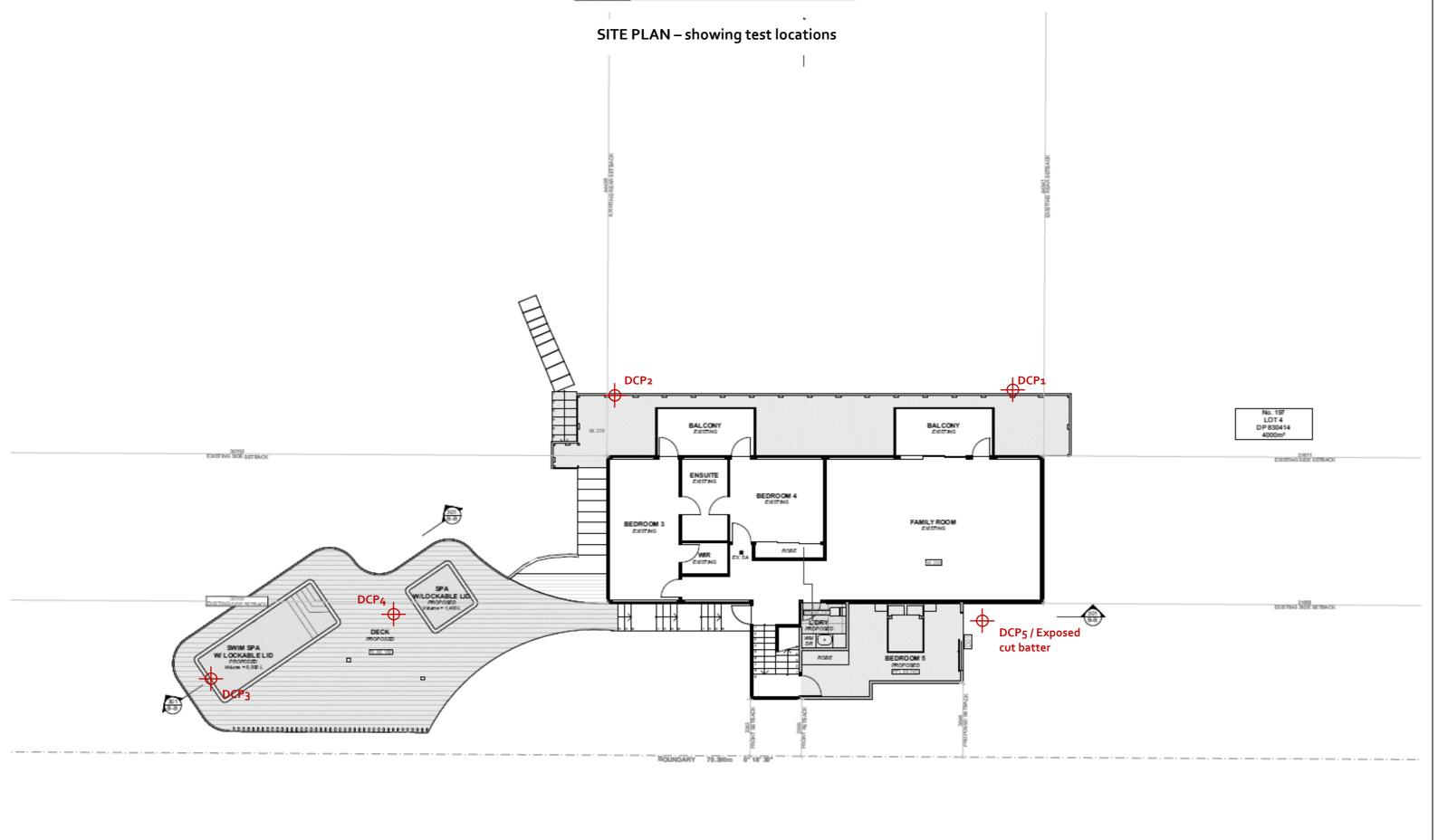
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#### Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes to suit the previous experience of the contractors involved). If alternative design and construction processes are required to those described in this report, contact White Geotechnical Group. We are familiar with a variety of techniques to reduce risk and can advise if your proposed methods are suitable for the site conditions.



PROPOSED LOWER GROUND FLOOR PLAN

1:100

ACTION PLANS

REV.	DATE	COMMENTS	NOTES This drawing is the copyright of Action Plans and not be
	3904303	DA - PRELIMINARY ISSUE	altered, repeduced or fanantified in any form or by any means in part or in whole with the written permission of
			Action Plans.  Do not scale measure from develops. Rigued dimensions.
			are to be used only.  The Builder Contractor shall check and worty all levels and
			dimensions on alle prior to commendement of any work, caustion of shop drawings, or fabrication of components.
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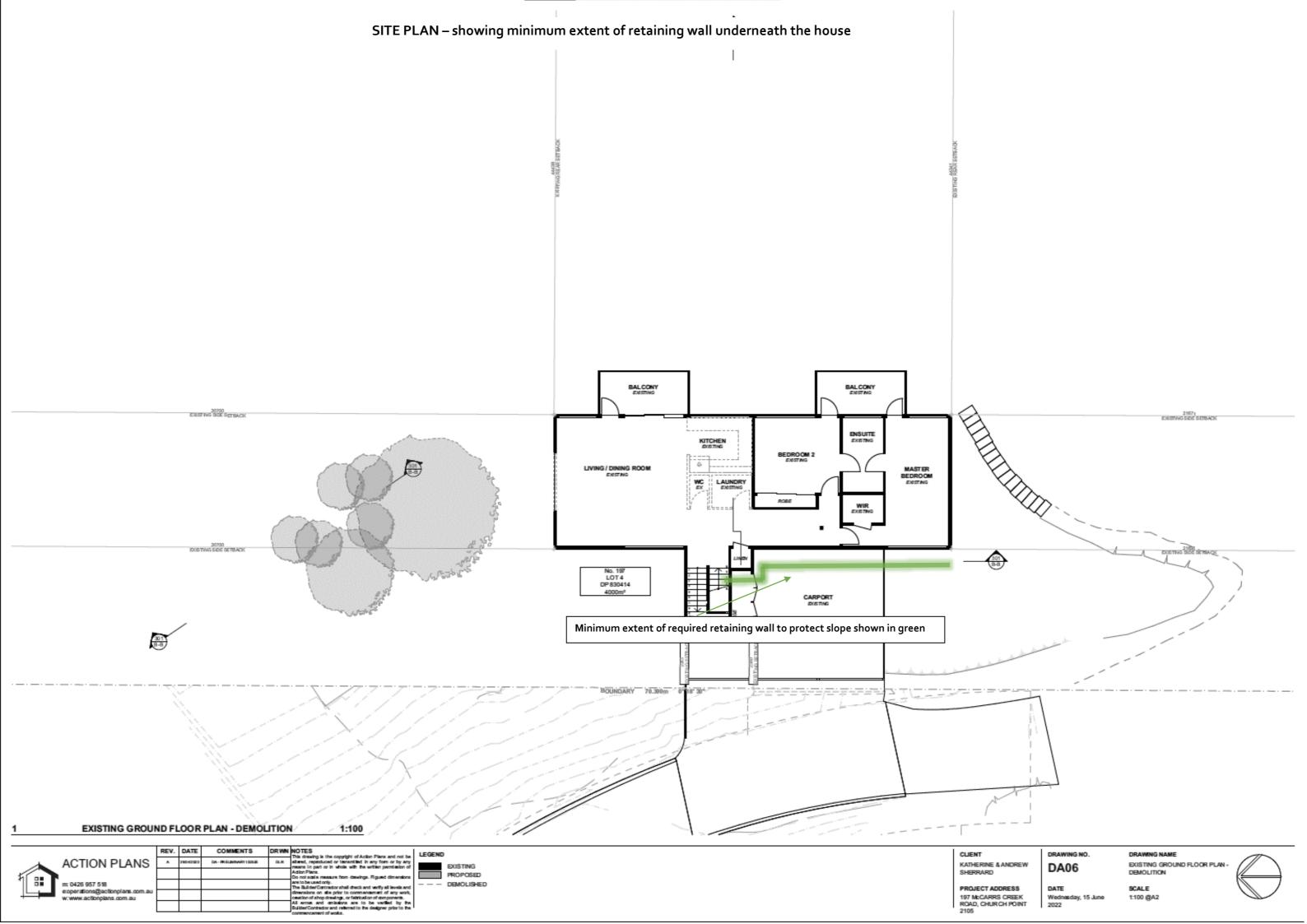
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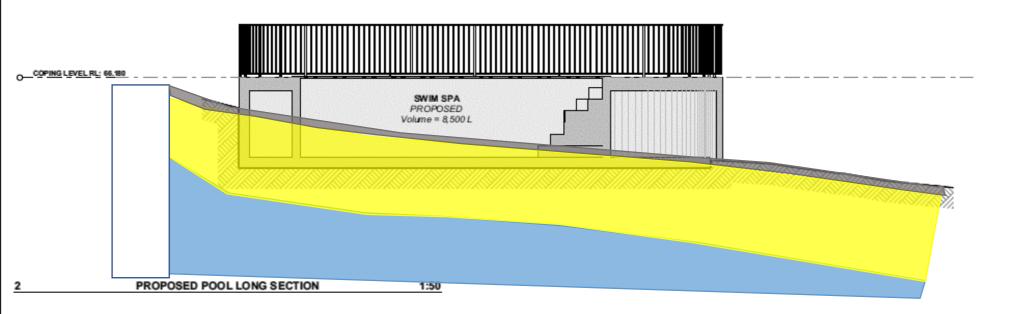
KATHERINE & ANDREW SHERRARD

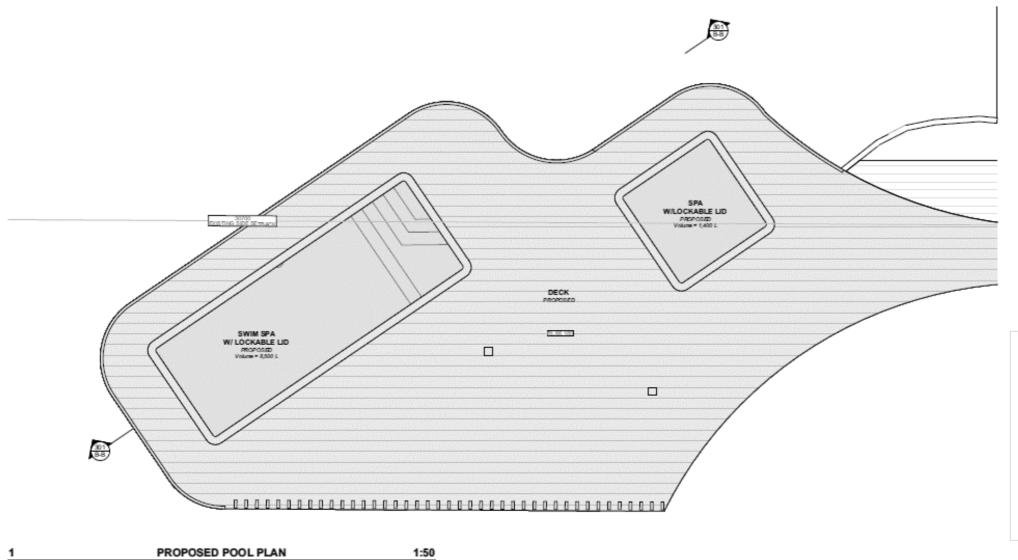
DA07 PROJECT ADDRESS 197 McCARRS CREEK ROAD, CHUR CH POINT 2105

PROPOSED LOWER GROUND FLOOR PLAN









# Fill Topsoil Clay – Firm to Stiff Narrabeen Group Rocks – Extremely Low Strength Shale after being cut up by excavation equipment can resemble a stiff to hard clay.

NOTE: SWIM SPA & SPATO INCLUDE LOCKABLE LIDS

ACTION PLANS

m: 0426 957 518
ecoperations@actionplans.com.au
w:www.actionplans.com.au

EV. DATE COMMENTS DR WN
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CLIENT KATHERINE & ANDREW SHERRARD

PROJECT ADDRESS

197 McCARRS CREEK ROAD, CHURCH POINT

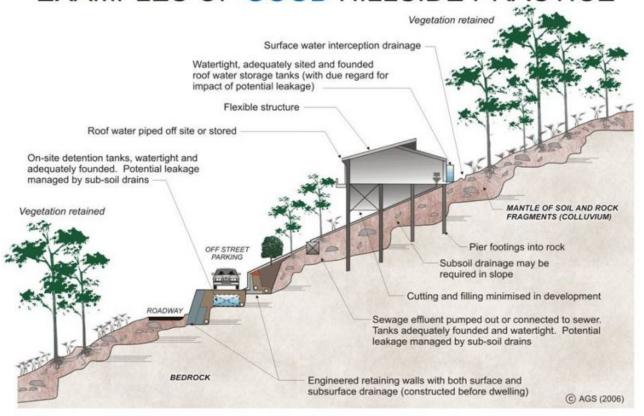
DA12

g no. Drawing name

POOL PLAN & LONG SECTION

DATE Wednesday, 15 June SCALE 1:50 @A2

## EXAMPLES OF GOOD HILLSIDE PRACTICE



### EXAMPLES OF POOR HILLSIDE PRACTICE

