

REPORT ON GEOTECHNICAL SITE INVESTIGATION

for

PROPOSED ALTERATIONS AND ADDITIONS

at

18 – 20 STURDEE LANE, LOVETT BAY

Prepared For

Fiona Loader

Project No.: 2018-116

September, 2018

Document Revision Record

Issue No	Date	Details of Revisions
0	18 th September, 2018	Original issue

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GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER **FORM NO. 1 – To be submitted with Development Application**

Development Application for _____

Name of Applicant

Address of site 18 – 20 Sturdee Lane, Lovett Bay

Declaration made by geotechnical engineer or engineering geologist or coastal engineer (where applicable) as part of a geotechnical report

I, Troy Crozier on behalf of Crozier Geotechnical Consultants on this the 18th September 2018 certify that I am a geotechnical engineer or engineering geologist or coastal engineer as defined by the Geotechnical Risk Management Policy for Pittwater - 2009 and I am authorised by the above organisation/company to issue this document and to certify that the organisation/company has a current professional indemnity policy of at least \$2million.

I:

- ☐ have prepared the detailed Geotechnical Report referenced below in accordance with the Australia Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
- ☒ am willing to technically verify that the detailed Geotechnical Report referenced below has been prepared in accordance with the Australian Geomechanics Society's Landslide Risk Management Guidelines (AGS 2007) and the Geotechnical Risk Management Policy for Pittwater - 2009
- ☐ have examined the site and the proposed development in detail and have carried out a risk assessment in accordance with Section 6.0 of the Geotechnical Risk Management Policy for Pittwater - 2009. I confirm that the results of the risk assessment for the proposed development are in compliance with the Geotechnical Risk Management Policy for Pittwater - 2009 and further detailed geotechnical reporting is not required for the subject site.
- ☐ have examined the site and the proposed development/alteration in detail and I am of the opinion that the Development Application only involves Minor Development/Alteration that does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
- ☐ have examined the site and the proposed development/alteration is separate from and is not affected by a Geotechnical Hazard and does not require a Geotechnical Report or Risk Assessment and hence my Report is in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009 requirements.
- ☐ have provided the coastal process and coastal forces analysis for inclusion in the Geotechnical Report

Geotechnical Report Details:

Report Title: Proposed Alterations and Additions at 18-20 Sturdee Lane, Lovett Bay

Report Date: 18th September 2018

Project No.: 2018-116

Author: Kieron Nicholson

Author's Company/Organisation: Crozier Geotechnical Consultants

Documentation which relate to or are relied upon in report preparation:

Architectural drawings supplied by James de Soyres and Associates, Project No.: 1708, Drawing No.'s: DA02 to DA04, DA 11 to DA15, DA21 to DA23, DA31 to DA34, DA90 to DA93, Dated: 7th June, 2018.

Site survey plan supplied by SDG Land Development Solutions, Reference No. 7430, Dated 10/11/2017.

I am aware that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a Development Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature _____

Name ... Troy Crozier

Chartered Professional Status... RPGeo (AIG)

Membership No. ... 10197

Company... Crozier Geotechnical Consultants



GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER
FORM NO. 1(a) - Checklist of Requirements For Geotechnical Risk Management Report for Development Application

Development Application for _____
 Name of Applicant _____
 Address of site _____ 18 – 20 Sturdee Lane, Lovett Bay _____

The following checklist covers the minimum requirements to be addressed in a Geotechnical Risk Management Geotechnical Report. This checklist is to accompany the Geotechnical Report and its certification (Form No. 1).

Geotechnical Report Details:

Report Title: Proposed Alterations and Additions at 18-20 Sturdee Lane, Lovett Bay
Report Date: 18th September 2018 **Project No.:** 2018-116
Author: Kieron Nicholson
Author's Company/Organisation: Crozier Geotechnical Consultants

Please mark appropriate box

- ☒ Comprehensive site mapping conducted 6th July 2018
 (date)
- ☒ Mapping details presented on contoured site plan with geomorphic mapping to a minimum scale of 1:200 (as appropriate)
- ☒ Subsurface investigation required
 - ☐ No Justification
 - ☒ Yes Date conducted6th July, 2018.....
- ☒ Geotechnical model developed and reported as an inferred subsurface type-section
- ☒ Geotechnical hazards identified
 - ☒ Above the site
 - ☐ On the site
 - ☐ Below the site
 - ☐ Beside the site
- ☒ Geotechnical hazards described and reported
- ☒ Risk assessment conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009
 - ☒ Consequence analysis
 - ☒ Frequency analysis
- ☒ Risk calculation
- ☒ Risk assessment for property conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009
- ☒ Risk assessment for loss of life conducted in accordance with the Geotechnical Risk Management Policy for Pittwater - 2009
- ☒ Assessed risks have been compared to "Acceptable Risk Management" criteria as defined in the Geotechnical Risk Management Policy for Pittwater - 2009
- ☒ Opinion has been provided that the design can achieve the "Acceptable Risk Management" criteria provided that the specified conditions are achieved.
- ☒ Design Life Adopted:
 - ☒ 100 years
 - ☐ Other specify
- ☒ Geotechnical Conditions to be applied to all four phases as described in the Geotechnical Risk Management Policy for Pittwater - 2009 have been specified
- ☒ Additional action to remove risk where reasonable and practical have been identified and included in the report.
- ☐ Risk assessment within Bushfire Asset Protection Zone.

I am aware that Pittwater Council will rely on the Geotechnical Report, to which this checklist applies, as the basis for ensuring that the geotechnical risk management aspects of the proposal have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated, and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature _____
 Name ... **Troy Crozier**
 Chartered Professional Status... **RPGeo (AIG)**
 Membership No. ... **10197**
 Company... **Crozier Geotechnical Consultants**



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- 5** Hillside Construction Guidelines

Date: 5th September, 2018

Project No: 2018-116

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**GEOTECHNICAL REPORT FOR ALTERATIONS & ADDITIONS TO EXISTING STRUCTURE
WITH CONSTRUCTION OF SECONDARY DWELLING
18-20 STURDEE LANE, LOVETT BAY, NSW**

1. INTRODUCTION:

This report details the results of a geotechnical investigation carried out for proposed alterations and additions to the existing house and construction of a secondary dwelling at No. 18-20 Sturdee Lane, Lovett Bay, NSW. The investigation was undertaken by Crozier Geotechnical Consultants (CGC) at the request of James de Soyres and Associates on behalf of Fiona Loader.

It is understood that the proposed works involve alterations and additions to the existing house along with construction of a separate secondary dwelling. It is understood that the works will involve the replacement of existing retaining walls as well as the construction of new retaining walls to support proposed excavations. Excavations within the site are not anticipated to exceed approximately 2.00m depth.

The site is located within the H1 (highest category) landslip hazard zone as identified within Pittwater Councils Geotechnical Hazard Mapping (Geotechnical Risk Management Policy for Pittwater 6 2009). To meet the Councils Policy requirements for land classified as H1 this report must meet the requirements of Paragraph 6.5 of that policy. Therefore this report must include; a landslide risk assessment of the site and proposed works, plans, geological sections and recommendations for construction and to ensure stability is maintained for a design life of 100 years.

This report is suitable for Council submission and preliminary design and construction purposes, it includes;

- A detailed description of the field work including field observations and test results.
- A plan showing geotechnical mapping and test locations.
- A site cross section showing a geological model including interpreted/determined depths to bedrock.
- A geotechnical assessment of the proposed works.
- Site specific risk assessment in accordance with Pittwater Council's requirements.
- Design and construction recommendations on:

Project No: 2018-116, Lovett Bay, September, 2018

- Site classification and footing design.
 - Excavation methods and suitable equipment and precautions.
 - Temporary and permanent excavation support.
 - Storm water Control and Disposal.
- Complete Forms 1 and 1a of Council's Policy.

The investigation and reporting were undertaken as per the Tender: P18-199, Dated: 18th June 2018.

The investigation comprised:

- a) A detailed geotechnical inspection and mapping of the site and adjacent properties by a Senior Engineering Geologist.
- b) Drilling of four boreholes using hand tools along with four Dynamic Cone Penetrometer (DCP) Tests to investigate the subsurface geology, depth to bedrock and identification of ground water conditions.

The following plans and drawings were supplied for the work:

- Survey Plans by SDG Land Development Solutions, Reference: 7430, Dated: 10th November 2017.
- Preliminary Development Application by James de Soyres and Associates, Project No: 1708, Drawing: DA02-04, DA11-15, DA21-23, DA31-34, DA90-93, Dated: 7th June 2018.

2. SITE FEATURES:

2.1. Description:

The site is broadly a long rectangular shaped block, reducing in width towards the rear of the property, and is located on the low north side of Sturdee Lane. The front of the site is bounded by Lovett Bay foreshore. The site has south, east and west boundaries of approximately 13.3m, 116.0m and 108.2m respectively. The front north boundary is approximately 29.5m and is delineated by the Mean High Water Mark (MHW) as defined by RMS, and referenced from the provided survey plan

An aerial photograph of the site and its surrounds is provided below (Photograph 1), as sourced from NSW Government Six Map spatial data.



Photograph 1: Aerial photo of site and surrounds

The site dwelling comprises a two storey weatherboard house with a one storey timber cabin at the rear and a jetty at the front. Two general views of the site are shown in Photograph 2 and Photograph 3.



Photograph 2: View of the front of site looking south from the property jetty.

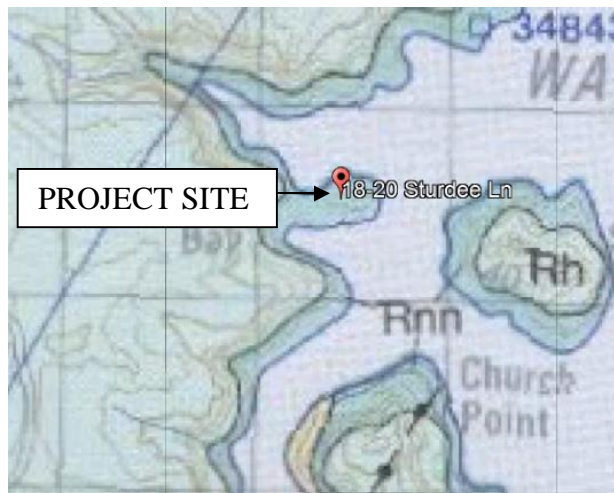


Photograph 3: View of the rear of existing house, looking north.

2.2. Geology:

Reference to the Sydney 1: 100,000 Geological Series sheet (9130) indicates that the site is underlain by Newport Formation (Rnn) of the Upper Narrabeen Group. Newport Formation (Upper Narrabeen Group) is of middle Triassic Age and typically comprises interbedded laminite, shale and quartz to lithic quartz sandstones and pink clay pellet sandstones.

Narrabeen Group rocks are dominated by shales and thin siltstone/sandstone beds and often form rounded convex ridge tops with moderate angle ($<20^\circ$) side slopes. These side slopes can be either concave or convex depending on geology, internally they comprise interbedded shale and siltstone beds with close spaced bedding partings that have either close spaced vertical joints or in extreme cases large space convex joints. The shale often forms deeply weathered profiles with silty or medium to high plasticity clays and a thin silty colluvial cover. Exposures of this unit were identified within and surrounding the site.



3. FIELD WORK:

3.1. Methods:

The field investigation comprised a walk over inspection and mapping of the site and adjacent properties on the 6th July 2018 by a Senior Engineering Geologist. It included a photographic record of site conditions as well as a geological/geomorphological mapping of the site and adjacent land with examination of soil slopes, rock outcrops, existing structures and neighbouring properties. It also included the drilling of four boreholes (BH1 to BH4) using a hand auger to investigate sub-surface geology. A hand auger was used as access to the majority of the site for a conventional drilling rig was unavailable.

DCP testing was carried out from ground surface adjacent to and within the boreholes in accordance with AS1289.6.3.2 ó 1997, öDetermination of the penetration resistance of a soil ó 9kg Dynamic Cone Penetrometerö to estimate near surface soil conditions and confirm depths to bedrock.

Explanatory notes are included in Appendix: 1. Mapping information and test locations are shown on Figure: 1, along with detailed Borehole log sheets and Dynamic Penetrometer Test Sheet in Appendix: 2. A geological model/section is provided as Figure: 2, Appendix: 2.

3.2. Field Observations:

The site is situated on the low north side of Sturdee Lane, on the foreshore of Lovett Bay, within moderately to steeply north dipping topography. The site residence comprises a two storey weatherboard house with a single storey timber cabin located approximately 10.5m to the south of the main residence.

The site is accessed from the water via a jetty which leads to a paved courtyard adjacent to the north-west corner of the house. The pavers in the courtyard do not display any obvious signs of cracking or settlement.

The front of the site contains a two storey weatherboard house that is in reasonable condition and does not display any obvious signs of cracking or distress. The timber cabin to the rear of the site residence is accessed via winding pathway that traverses the site adjacent to a number of gardens supported by retaining walls Ö1.50m in height. Where the path has been cut into the existing stone, interbedded low strength sandstone and very low strength mudstone was observed (see Photograph 4 below).



Photograph 4: Interbedded sandstone and shale adjacent to the pathway.

The remainder of the site contains a winding pathway, which leads to Sturdee Lane at the rear of the site, and gardens containing moderate levels of vegetation. Sandstone boulders are visible throughout the upper (south) end of the site however were not observed in the vicinity of the proposed excavations. (Photograph 5).



Photograph 5: Sandstone boulders located in the upper south end of the site.

The neighbouring property to the west, No. 22 Sturdee Lane, contains a two-storey split level timber residential house located within approximately 4.2m from the common boundary with the site. The ground surface level within this property is similar to the site immediately adjacent to the shared boundary the boundary with the remainder of the block moderately to steeply north dipping.

The neighbouring property to the east, No. 16 Sturdee Lane, contains a two storey timber residential house within approximately 3.0m of the common boundary with the site. The property also contains a timber cabin in the rear within approximately 2.0m of the common boundary with the site. The ground surface level within this property is similar to the site at the boundary with the remainder of the block moderately to steeply north dipping.

The neighbouring properties and structures were inspected from the site, however visible aspects showed no indications of significant geotechnical hazard that may impact the site.

3.3. Field Testing:

The boreholes (BH1 to BH4) were drilled using hand auger and refusal was encountered at 0.75m, 0.60m, 0.50m and 0.30m within BH1 to BH4 respectively. The DCP tests reached a maximum depth of 2.25m (DCP3) prior to refusal.

Based on the field borehole logs and DCP test results, the sub-surface conditions at the project site can be broadly classified as follows:

- **TOPSOIL/FILL** ó This layer was encountered at all test locations to a maximum depth of 0.60m (BH2) below the existing ground surface. It comprised brown to dark brown, fine to medium grained, silty/clayey sand with roots, clay zones and gravel. All boreholes encountered refusal in the fill with the exception of BH1.
- **COLLUVIUM** ó BH1 encountered natural colluvial soils comprising firm to silty stiff clay between 0.40 and 0.75m depth.
- **RESIDUAL SOILS** ó Based on DCP test results residual soils comprising firm to hard sandy clay were interpreted to depths between 1.50m (DCP 4) and of 2.10m (BH3) below the existing ground surface.
- **INTERBEDDED SANDSTONE/SHALE** ó Based on DCP results and visual assessment of exposed outcrops, interbedded sandstone and shale of at least very low strength was interpreted to vary from 1.35m (BH4) to 2.10m (BH3) below the existing ground surface.

A free standing ground water table or significant water seepage were not identified within any of the boreholes. No signs of ground water were observed after the retrieval of the DCP rods.

4. COMMENTS:

4.1. Geotechnical Assessment:

The site investigation identified the presence of a layer fill of shallow thickness (Ö0.60m) underlain by colluviums to 0.75m depth (BH1 only) in turn underlain by residual clay soils which grade to weathered bedrock of shale/sandstone of very low strength. Based on DCP test results, the depth to the bedrock of minimum very low strength was interpreted to vary from 1.35m to 2.25m. The bedrock is expected to grade quickly to low strength and may contain medium strength sandstone bands.

The site investigation identified no signs of previous or impending shallow or deep seated landslip instability within the site and there were no landslip hazards identified within the neighbouring properties.

The proposed works involve alterations and additions to the existing residential dwelling and construction of a secondary drilling . Excavations up to approximately 2.00m depth will be required for the proposed development which will be supported by new retaining walls.

Based on the investigation results, the proposed excavation for the development is expected to intersect fill along with near surface colluvial soils up to 1.50m to 2.0m depth. Underlying the colluvial soils, residual clay soils are anticipated which likely grades to extremely to very low strength sandstone/siltstone at a maximum depth of 2.25m.

Considering the relatively shallow depth of the propped excavations along with the separation distances from the site boundaries, safe temporary batter slopes of 1.50H: 1.00V (natural soils) and 1.00H: 1.00V (weathered bedrock) appear to be generally achievable. Where insufficient space exists, it will be necessary to provide temporary support to excavated faces to ensure the continued stability. Where replacement of existing retaining walls is proposed it is recommended that the replacement is done in stages such that exposed (vertical) excavation faces of greater than approximately 0.75m width are not left unsupported.

The exact strength of the bedrock which may be encountered during excavation is unconfirmed and is likely to vary with depth and across the site. There is a potential for localized excavations to intersect low strength and potentially medium strength (MS) bedrock. However the proposed excavations are relatively limited and small (<200kg) rock hammers could be used if required which will maintain low ground vibrations levels as per the AS2187.2-2006 requirements.

Where trees require removal to allow the construction of new structures, it will be necessary to ensure all root bowl material is removed from any settlement sensitive areas to reduce the potential for future, non-uniform settlements.

New footings should extend through the fill/colluvial soils and found within either hard residual clay or weathered bedrock encountered underlying the site.

The proposed works are considered suitable for the site and may be completed with negligible impact to existing nearby structures within the site or neighbouring properties provided the recommendations of this report are implemented in the design and construction phases.

The recommendations and conclusions in this report are based on an investigation utilising only surface observations and hand drilling tools due to access limitations. This test equipment provides limited data from small isolated test points across the entire site with limited penetration into rock, therefore some minor variation to the interpreted sub-surface conditions is possible, especially between test locations. However the results of the investigation provide a reasonable basis for the Development Application analysis and subsequent initial design of the proposed works.

4.2. Site Specific Risk Assessment:

Based on our site investigation we have identified the following geological/geotechnical landslip hazard which needs to be considered in relation to the existing site and the proposed works. This hazard is:

- A. Earth slide of fill/natural soils due to excavation.

A qualitative assessment of risk to life and property related to this hazard is presented in Table A and B, Appendix: 3, and is based on methods outlined in Appendix: C of the Australian Geomechanics Society (AGS) Guidelines for Landslide Risk Management 2007. AGS terms and their descriptions are provided in Appendix: 4.

Due to the separation distance of the proposed works from the property boundaries and adjacent structures, along with the scale of excavation, the hazard has sensibly only a potential impact to site users following excavation.

The Risk to Life from Hazard A was estimated to be up to 2.50×10^{-6} , whilst the Risk to Property was considered to be '**Low**'. The risk to life was therefore considered to be 'Acceptable' when assessed against the criteria of the AGS 2007

4.3. Design & Construction Recommendations:

Design and the construction recommendations are tabulated below:

4.3.1. New Footings:	
Site Classification as per AS2870 ó 2011 for new footing design	<ul style="list-style-type: none"> - Class -Mø for clay soils - Class -Aø for footings founded within bedrock
Type of Footing	Strip/Pad or Slab at base of excavation, piers external to excavations or to ensure consistent foundation.
Sub-grade material and Maximum Allowable Bearing Capacity	<ul style="list-style-type: none"> - Hard Clay bedrock ó 400kPa - Weathered, ELS bedrock: 600kPa - Weathered, VLS bedrock: 800kPa - Weathered, LS bedrock: 1000kPa
Site sub-soil classification as per <i>Structural design actions AS1170.4 – 2007, Part 4: Earthquake actions in Australia</i>	B _e ó Rock site (provided entire new structures founded to bedrock).
Remarks: <ul style="list-style-type: none"> - All permanent structure footings should be founded off bedrock of similar strength to prevent differential settlement unless structure is designed to accommodate some movement. - All new footings must be inspected by an experienced geotechnical professional before concrete or steel are placed to verify their bearing capacity and the in-situ nature of the founding strata. This is mandatory to allow them to be -certifiedø at the end of the project. 	

4.3.2. Excavation:		
Depth of Excavation	Minor excavations up to 2.00m depth.	
Distance of Excavation to Neighbouring Properties/structures	No. 16 ó 1.00m from boundary, house 6.00m from boundary. No. 22 ó 2.50m from boundary, house 4.20m from boundary.	
Type of Material to be Excavated	Topsoil/Fill (Ö0.50m depth)	
	Firm to Hard Natural Soils (up to 2.10m depth)	
	Interbedded Sandstone/Shale (possibly)	
Guidelines for batter slopes for general information are tabulated below:		
Material	Safe Batter Slope (H:V)	
	Short Term/ Temporary	Long Term/ Permanent
Natural soils and extremely low strength bedrock	1.5:1	2:1
Very Low to low strength bedrock	1:1	1.25:1
Remarks:		

<p>Seepage through the sandy/clayey soils can reduce the stability of batter slopes and invoke the need to implement additional support measures. Where safe batter slopes are not implemented the stability of the excavation cannot be guaranteed until the installation of permanent support measures. This should also be considered with respect to safe working conditions.</p> <p>Geotechnical inspection of batters will be required at regular intervals to assess their stability, especially for permanent batters.</p> <p>Excavation outlines and impacts must also be assessed by an arborist.</p>		
Equipment for Excavation	Natural soils	Excavator with Bucket
	VLS bedrock	Excavator with ripper and bucket
ELS ó extremely low strength, VLS ó very low strength, LS ó low strength, MS ó medium strength		
Recommended Vibration Limits (Maximum Peak Particle Velocity (PPV))	Not applicable	
Vibration Calibration Tests Required	Not required	
Full time vibration Monitoring Required	Not required	
Geotechnical Inspection Requirement	Yes, recommended that these inspections be undertaken as per below mentioned sequence: <ul style="list-style-type: none">• For assessment of batter slopes• Where unexpected ground conditions are identified or any other concerns are held.• Following footing excavations to confirm founding material strength	
Dilapidation Surveys Requirement	Not required	
Remarks: <p>Water ingress into exposed excavations can result in erosion and stability concerns in both sandy and clayey soils. Drainage measures will need to be in place during excavation works to divert any surface flow away from the excavation crest and any batter slope, whilst any groundwater seepage must be controlled within the excavation and prevented from ponding or saturating slopes/batters.</p>		

4.3.3. Retaining Structures:	
Required	New retaining structures will be required as part of the proposed development.
Types	Steel reinforced concrete/concrete block walls post excavation/pre fill, or installed progressively during excavation designed in accordance with Australian Standards AS4678-2002 Earth Retaining Structures.

Parameters for calculating pressures acting on retaining walls for the materials likely to be retained:					
Material	Unit Weight (kN/m ³)	Long Term (Drained)	Earth Pressure Coefficients		Passive Earth Pressure Coefficient *
			Active (K _a)	At Rest (K ₀)	
Sandy Colluvial Soils	18	$\phi' = 29^\circ$	0.35	0.52	N/A
Clay Soils	20	$\phi' = 30^\circ$	0.33	0.47	3.25
ELS bedrock	22	$\phi' = 38^\circ$	0.15	0.20	200 kPa
VLS to LS bedrock	23	$\phi' = 40^\circ$	0.10	0.15	400 kPa
Remarks: In suggesting these parameters it is assumed that the retaining walls will be fully drained with suitable subsoil drains provided at the rear of the wall footings. If this is not done, then the walls should be designed to support full hydrostatic pressure in addition to pressures due to the soil backfill. It is suggested that the retaining walls should be back filled with free-draining granular material (preferably not recycled concrete) which is only lightly compacted in order to minimize horizontal stresses. Retaining structures near site boundaries or existing structures should be designed with the use of at rest (K ₀) earth pressure coefficients to reduce the risk of movement in the excavation support and resulting surface movement in adjoining areas. Backfilled retaining walls within the site, away from site boundaries or existing structures, that may deflect can utilize active earth pressure coefficients (K _a).					

4.3.4. Drainage and Hydrogeology		
Groundwater Table or Seepage identified in Investigation		No
Excavation likely to intersect	Water Table	No
	Seepage	Minor (<0.50L/min), within sandy/clayey soils at bedrock surface or along defects in the bedrock
Site Location and Topography		Dipping north to foreshore.
Impact of development on local hydrogeology		Negligible
Onsite Stormwater Disposal		It is envisaged drainage will discharge directly into Lovett Bay
Remarks: As the excavation faces are expected to encounter some seepage, an excavation trench should be installed at the base of excavation cuts to below floor slab levels to reduce the risk of resulting dampness issues.		

Trenches, as well as all new building gutters, down pipes and stormwater intercept trenches should be connected to a stormwater system designed by a Hydraulic Engineer which discharges to the Council's stormwater system off site.

4.4. Conditions Relating to Design and Construction Monitoring:

To allow certification as part of construction, building and post-construction activity for this project, it will be necessary for Crozier Geotechnical Consultants to:

1. Review and approve the structural design drawings, including the retaining structure design and construction methodology, for compliance with the recommendations of this report prior Construction Certificate.
2. Conduct inspections as per Section 4.3 of this report.
3. Inspect all new footings to confirm compliance to design assumptions with respect to allowable bearing pressure and stability prior to the placement of steel or concrete.

The client and builder should make themselves familiar with the requirements spelled out in this report for inspections during the construction phase. Crozier Geotechnical Consultants cannot provide certification for the Occupation Certificate if it has not been called to site to undertake the required inspections.

4.5. Design Life of Structure:

We have interpreted design life requirements to refer to structural elements designed to support the house etc, the adjacent slope, control stormwater and maintain the risk of instability within acceptable limits. Specific structures and features that may affect the maintenance and stability of the site in relation to the proposed and existing development are considered to comprise:

- stormwater and subsoil drainage systems,
- rock excavation stability and retaining walls,
- maintenance of trees/vegetation on this and adjacent properties.

Man-made features should be designed and maintained for a design life consistent with surrounding structures (as per AS2870 6 2011 (50 years)). It will be necessary for the structural and geotechnical engineers to incorporate appropriate design and inspection procedures during the construction period as per the recommendations of this report. Additionally the property owner should adopt and implement a maintenance and inspection program.

If this maintenance and inspection schedule are not maintained the design life of the property may not be attained. A recommended maintenance program is given in Table: C in Appendix: 3 and should also include the following guidelines:

- The conditions on the block don't change from those present at the time this report was prepared, except for the changes due to this development.
- There is no change to the property due to an extraordinary event external to this site.
- The property is maintained in good order and in accordance with the guidelines set out in;
 - a) CSIRO sheet BTF 18
 - b) Australian Geomechanics "Landslide Risk Management" Volume 42, March 2007
 - c) AS 2870 6 2011, Australian Standard for Residential Slabs and Footings

Where changes to site conditions are identified during the maintenance and inspection program, reference should be made to the relevant professionals (e.g. structural engineer, geotechnical engineer or Council). Where the property owner has any lack of understanding or concerns about the implementation of any component of the maintenance and inspection program the relevant engineer should be contacted for advice or to complete the component. It is assumed that Pittwater Municipal Council will control development on neighbouring properties, carry out regular inspections and maintenance of the road verge, stormwater systems and large trees on public land adjacent to the site so as to ensure that stability conditions do not deteriorate with potential increase in risk level to the site. Also individual Government Departments will maintain public utilities in the form of power lines, water and sewer mains to ensure they don't leak and increase either the local groundwater level or landslide potential.

5. CONCLUSION:

The site investigation identified the presence of fill/colluvium underlain by residual clay soils which grade to weathered bedrock of at least very low strength. Based on DCP test results, the depth to the bedrock of minimum very low strength (VLS) was interpreted to 1.35-2.25m underlying the site.

Excavations up to 2.0m depth will be required for proposed new structures and footings should extend through the fill/colluvium and found within either hard residual clay or weathered bedrock. The new footings will require inspection to verify their bearing capacity and the in-situ nature of the founding strata.

Temporary and permanent batters can be generally achieved and the potential for slope instability is relatively low however where insufficient space is available support will be required.

The risk from geological/geotechnical hazard which was identified in relation to the existing site and proposed works, is limited to minor landslip failure of soils due to excavation and is considered ~~Acceptable~~ when assessed against the criteria of the AGS 2007.

The risks associated with the proposed development can be maintained within ~~Acceptable~~ levels with negligible impact to neighbouring or structures, provided the recommendations of this report and any future geotechnical directive are implemented. As such the site is considered suitable for the proposed construction works provided that the recommendations outlined in this report are followed.



Prepared by:
Kieron Nicholson
Senior Engineering Geologist



Reviewed by:
Troy Crozier
Principal Engineering Geologist
MAIG. RPGeo; 10197

6. REFERENCES:

1. Australian Geomechanics Society 2007, "Landslide Risk Assessment and Management", Australian Geomechanics Journal Vol. 42, No 1, March 2007.
2. Geological Society Engineering Group Working Party 1972, "The preparation of maps and plans in terms of engineering geology" Quarterly Journal Engineering Geology, Volume 5, Pages 295 - 382.
3. C. W. Fetter 1995, "Applied Hydrology" by Prentice Hall. V. Gardiner & R. Dackombe 1983, "Geomorphological Field Manual" by George Allen & Unwin
4. Australian Standard AS 3798 ó 2007, Guidelines on Earthworks for Commercial and Residential Developments.
5. Australian Standard AS 2870 ó 1996, Residential Slabs and Footings ó Construction
6. Australian Standard AS1170.4 ó 2007, Part 4: Earthquake actions in Australia

Appendix 1

NOTES RELATING TO THIS REPORT

Introduction

These notes have been provided to amplify the geotechnical report in regard to classification methods, specialist field procedures and certain matters relating to the Discussion and Comments section. Not all, of course, are necessarily relevant to all reports.

Geotechnical reports are based on information gained from limited subsurface test boring and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

Description and classification Methods

The methods of description and classification of soils and rocks used in this report are based on Australian Standard 1726, Geotechnical Site Investigation Code. In general, descriptions cover the following properties - strength or density, colour, structure, soil or rock type and inclusions.

Soil types are described according to the predominating particle size, qualified by the grading of other particles present (eg. Sandy clay) on the following bases:

<u>Soil Classification</u>	<u>Particle Size</u>
Clay	less than 0.002 mm
Silt	0.002 to 0.06 mm
Sand	0.06 to 2.00 mm
Gravel	2.00 to 60.00mm

Cohesive soils are classified on the basis of strength either by laboratory testing or engineering examination. The strength terms are defined as follows:

<u>Classification</u>	<u>Undrained Shear Strength kPa</u>
Very soft	Less than 12
Soft	12 - 25
Firm	25 - 50
Stiff	50 - 100
Very stiff	100 - 200
Hard	Greater than 200

Non-cohesive soils are classified on the basis of relative density, generally from the results of standard penetration tests (SPT) or Dutch cone penetrometer tests (CPT) as below:

<u>Relative Density</u>	<u>SPT</u> "N" Value (blows/300mm)	<u>CPT</u> Cone Value (Qc - MPa)
Very loose	less than 5	less than 2
Loose	5 - 10	2 - 5
Medium dense	10 - 30	5 - 15
Dense	30 - 50	15 - 25
Very dense	greater than 50	greater than 25

Rock types are classified by their geological names. Where relevant, further information regarding rock classification is given on the following sheet.

Sampling

Sampling is carried out during drilling to allow engineering examination (and laboratory testing where required) of the soil or rock.

Disturbed samples taken during drilling to allow information on colour, type, inclusions and, depending upon the degree of disturbance, some information on strength and structure.

Undisturbed samples are taken by pushing a thin-walled sample tube into the soil and withdrawing a sample of the soil in a relatively undisturbed state. Such samples yield information on structure and strength, and are necessary for laboratory determination of shear strength and compressibility. Undisturbed sampling is generally effective only in cohesive soils.

Drilling Methods

The following is a brief summary of drilling methods currently adopted by the company and some comments on their use and application.

Test Pits – these are excavated with a backhoe or a tracked excavator, allowing close examination of the insitu soils if it is safe to descent into the pit. The depth of penetration is limited to about 3m for a backhoe and up to 6m for an excavator. A potential disadvantage is the disturbance caused by the excavation.

Large Diameter Auger (eg. Pengo) – the hole is advanced by a rotating plate or short spiral auger, generally 300mm or larger in diameter. The cuttings are returned to the surface at intervals (generally of not more than 0.5m) and are disturbed but usually unchanged in moisture content. Identification of soil strata is generally much more reliable than with continuous spiral flight augers, and is usually supplemented by occasional undisturbed tube sampling.

Continuous Sample Drilling – the hole is advanced by pushing a 100mm diameter socket into the ground and withdrawing it at intervals to extrude the sample. This is the most reliable method of drilling soils, since moisture content is unchanged and soil structure, strength, etc. is only marginally affected.

Continuous Spiral Flight Augers – the hole is advanced using 90 – 115mm diameter continuous spiral flight augers which are withdrawn at intervals to allow sampling or insitu testing. This is a relatively economical means of drilling in clays and in sands above the water table. Samples are returned to the surface, or may be collected after withdrawal of the auger flights, but they are very disturbed and may be contaminated. Information from the drilling (as distinct from specific sampling by SPT's or undisturbed samples) is of relatively lower reliability, due to remoulding, contamination or softening of samples by ground water.

Non-core Rotary Drilling - the hole is advanced by a rotary bit, with water being pumped down the drill rods and returned up the annulus, carrying the drill cuttings. Only major changes in stratification can be determined from the cuttings, together with some information from 'feel' and rate of penetration.

Rotary Mud Drilling – similar to rotary drilling, but using drilling mud as a circulating fluid. The mud tends to mask the cuttings and reliable identification is again only possible from separate intact sampling (eg. From SPT).

Continuous Core Drilling – a continuous core sample is obtained using a diamond-tipped core barrel, usually 50mm internal diameter. Provided full core recovery is achieved (which is not always possible in very weak rocks and granular soils), this technique provides a very reliable (but relatively expensive) method of investigation.

Standard Penetration Tests

Standard penetration tests (abbreviated as SPT) are used mainly in non-cohesive soils, but occasionally also in cohesive soils as a means of determining density or strength and also of obtaining a relatively undisturbed sample. The test procedures is described in Australian Standard 1289, "Methods of Testing Soils for Engineering Purposes" – Test 6.3.1.

The test is carried out in a borehole by driving a 50mm diameter split sample tube under the impact of a 63kg hammer with a free fall of 760mm. It is normal for the tube to be driven in three successive 150mm increments and the 'N' value is taken

as the number of blows for the last 300mm. In dense sands, very hard clays or weak rock, the full 450mm penetration may not be practicable and the test is discontinued.

The test results are reported in the following form.

- In the case where full penetration is obtained with successive blow counts for each 150mm of say 4, 6 and 7 as 4, 6, 7 then $N = 13$
- In the case where the test is discontinued short of full penetration, say after 15 blows for the first 150mm and 30 blows for the next 40mm then as 15, 30/40mm.

The results of the test can be related empirically to the engineering properties of the soil. Occasionally, the test method is used to obtain samples in 50mm diameter thin wall sample tubes in clay. In such circumstances, the test results are shown on the borelogs in brackets.

Cone Penetrometer Testing and Interpretation

Cone penetrometer testing (sometimes referred to as Dutch Cone – abbreviated as CPT) described in this report has been carried out using an electrical friction cone penetrometer. The test is described in Australia Standard 1289, Test 6.4.1.

In tests, a 35mm diameter rod with a cone-tipped end is pushed continually into the soil, the reaction being provided by a specially designed truck or rig which is fitted with an hydraulic ram system. Measurements are made of the end bearing resistance on the cone and the friction resistance on a separate 130mm long sleeve, immediately behind the cone. Transducers in the tip of the assembly are connected by electrical wires passing through the centre of the push rods to an amplifier and recorder unit mounted on the control truck.

As penetration occurs (at a rate of approximately 20mm per second) their information is plotted on a computer screen and at the end of the test is stored on the computer for later plotting of the results.

The information provided on the plotted results comprises: -

- Cone resistance – the actual end bearing force divided by the cross-sectional area of the cone – expressed in MPa.
- Sleeve friction – the frictional force on the sleeve divided by the surface area – expressed in kPa.
- Friction ratio - the ratio of sleeve friction to cone resistance, expressed in percent.

There are two scales available for measurement of cone resistance. The lower scale (0 – 5 MPa) is used in very soft soils where increased sensitivity is required and is shown in the graphs as a dotted line. The main scale (0 – 50 MPa) is less sensitive and is shown as a full line. The ratios of the sleeve friction to cone resistance will vary with the type of soil encountered, with higher relative friction in clays than in sands. Friction ratios 1% - 2% are commonly encountered in sands and very soft clays rising to 4% - 10% in stiff clays.

In sands, the relationship between cone resistance and SPT value is commonly in the range: -

$$Q_c \text{ (MPa)} = (0.4 \text{ to } 0.6) N \text{ blows (blows per 300mm)}$$

In clays, the relationship between undrained shear strength and cone resistance is commonly in the range: -

$$Q_c = (12 \text{ to } 18) C_u$$

Interpretation of CPT values can also be made to allow estimation of modulus or compressibility values to allow calculations of foundation settlements.

Inferred stratification as shown on the attached reports is assessed from the cone and friction traces and from experience and information from nearby boreholes, etc. This information is presented for general guidance, but must be regarded as being to some extent interpretive. The test method provides a continuous profile of engineering properties, and where precise information on soil classification is required, direct drilling and sampling may be preferable.

Dynamic Penetrometers

Dynamic penetrometer tests are carried out by driving a rod into the ground with a falling weight hammer and measuring the blows for successive 150mm increments of penetration. Normally, there is a depth limitation of 1.2m but this may be extended in certain conditions by the use of extension rods.

Two relatively similar tests are used.

- Perth sand penetrometer – a 16mm diameter flattened rod is driven with a 9kg hammer, dropping 600mm (AS1289, Test 6.3.2). The test was developed for testing the density of sands (originating in Perth) and is mainly used in granular soils and filling.
- Cone penetrometer (sometimes known as Scala Penetrometer) – a 16mm rod with a 20mm diameter cone end is driven with a 9kg hammer dropping 510mm (AS 1289, Test 6.3.2). The test was developed initially for pavement sub-grade investigations, and published correlations of the test results with California bearing ratio have been published by various Road Authorities.

Laboratory Testing

Laboratory testing is generally carried out in accordance with Australian Standard 1289 “Methods of Testing Soil for Engineering Purposes”. Details of the test procedure used are given on the individual report forms.

Borehole Logs

The bore logs presented herein are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable, or possible to justify on economic grounds. In any case, the boreholes represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes, the frequency of sampling and the possibility of other than ‘straight line’ variations between the boreholes.

Details of the type and method of sampling are given in the report and the following sample codes are on the borehole logs where applicable:

D	Disturbed Sample	E	Environmental sample
B	Bulk Sample	PP	Pocket Penetrometer Test
U50	50mm Undisturbed Tube Sample	SPT	Standard Penetration Test
U63	63mm “ “ “ “ “		

Ground Water

Where ground water levels are measured in boreholes there are several potential problems:

- In low permeability soils, ground water although present, may enter the hole slowly or perhaps not at all during the time it is left open.
- A localised perched water table may lead to an erroneous indication of the true water table.
- Water table levels will vary from time to time with seasons or recent weather changes. They may not be the same at the time of construction as are indicated in the report.
- The use of water or mud as a drilling fluid will mask any ground water inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water observations are to be made. More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be interference from a perched water table.

Engineering Reports

Engineering reports are prepared by qualified personnel and are based on the information obtained and on current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal (eg. A three-storey building), the information and interpretation may not be relevant if the design proposal is changed (eg. to a twenty-storey building). If this happens, the Company will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface condition, discussion of geotechnical aspects and recommendations or suggestions for design and construction. However, the Company cannot always anticipate or assume responsibility for:

- unexpected variations in ground conditions – the potential for this will depend partly on bore spacing and sampling frequency,
- changes in policy or interpretation of policy by statutory authorities,
- the actions of contractors responding to commercial pressures,

If these occur, the Company will be pleased to assist with investigation or advice to resolve the matter.

Site Anomalies

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, the Company requests that it immediately be notified. Most problems are much more readily resolved when conditions are exposed than at some later stage, well after the event.

Reproduction of Information for Contractual Purposes

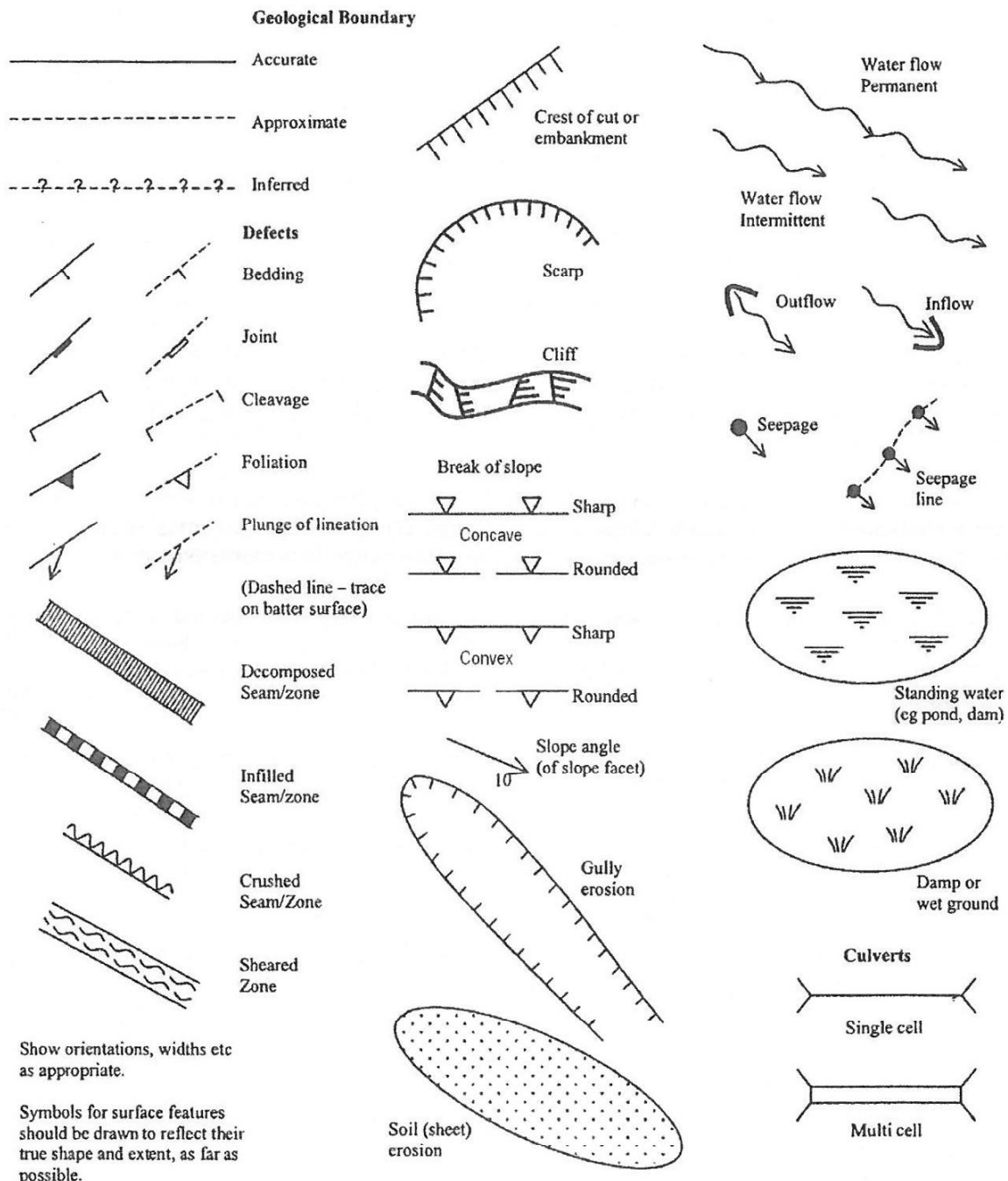
Attention is drawn to the document “Guidelines for the Provision of Geotechnical Information in Tender Documents”, published by the Institution of Engineers Australia. Where information obtained from this investigation is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a special ally edited document. The Company would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

Site Inspection

The Company will always be pleased to provide engineering inspection services for geotechnical aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

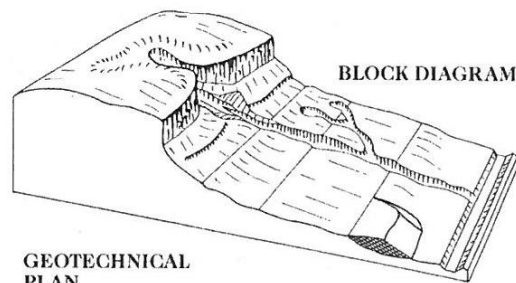
PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

APPENDIX E - GEOLOGICAL AND GEOMORPHOLOGICAL MAPPING SYMBOLS AND TERMINOLOGY

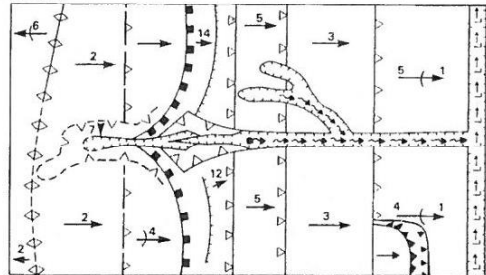


Examples of Mapping Symbols (after Guide to Slope Risk Analysis Version 3.1 November 2001, Roads and Traffic Authority of New South Wales).

PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007



GEOTECHNICAL
PLAN

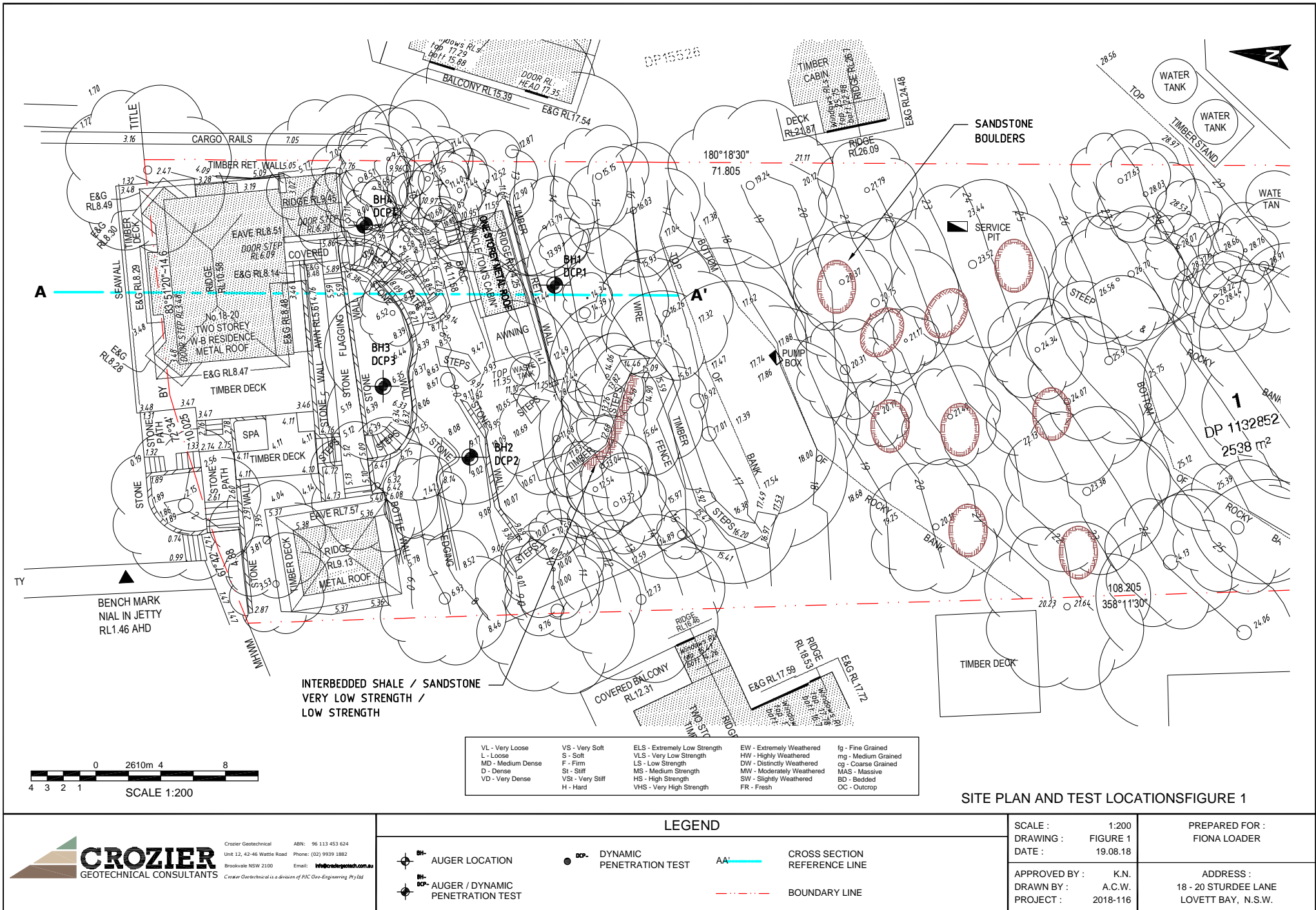


SYMBOL	GROUND PROFILE	
		Convex
		Concave
		Convex
		Concave
		Convex and concave too close together to allow the use of separate symbols
		Sharp
		Rounded
		Cliff or escarpment or sharp break 40' or more (estimated height in metres)
		Uniform slope
		Concave slope
		Convex slope
		Top
		Bottom
		Hummocky or irregular ground
		Open drain, unlined
		Open drain, lined
		Fenceline
		Property boundary
		Dry stone wall
		Major joint in rock face (opening in millimetres)
		Tension crack (opening in millimetres)

Example of Mapping Symbols

(after V Gardiner & R V Dackombe (1983). Geomorphological Field Manual. George Allen & Unwin).

Appendix 2



CROZIER
GEOTECHNICAL CONSULTANTS

Crozier Geotechnical
Unit 12, 42-46 Watlie Road
Brookvale NSW 2100
Phone: (02) 9939 1882
Email: info@croziergeotech.com.au
Crozier Geotechnical is a division of RJC Geo-Engineering Pty Ltd

ABN: 96 113 453 624

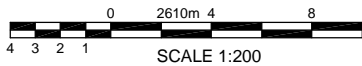
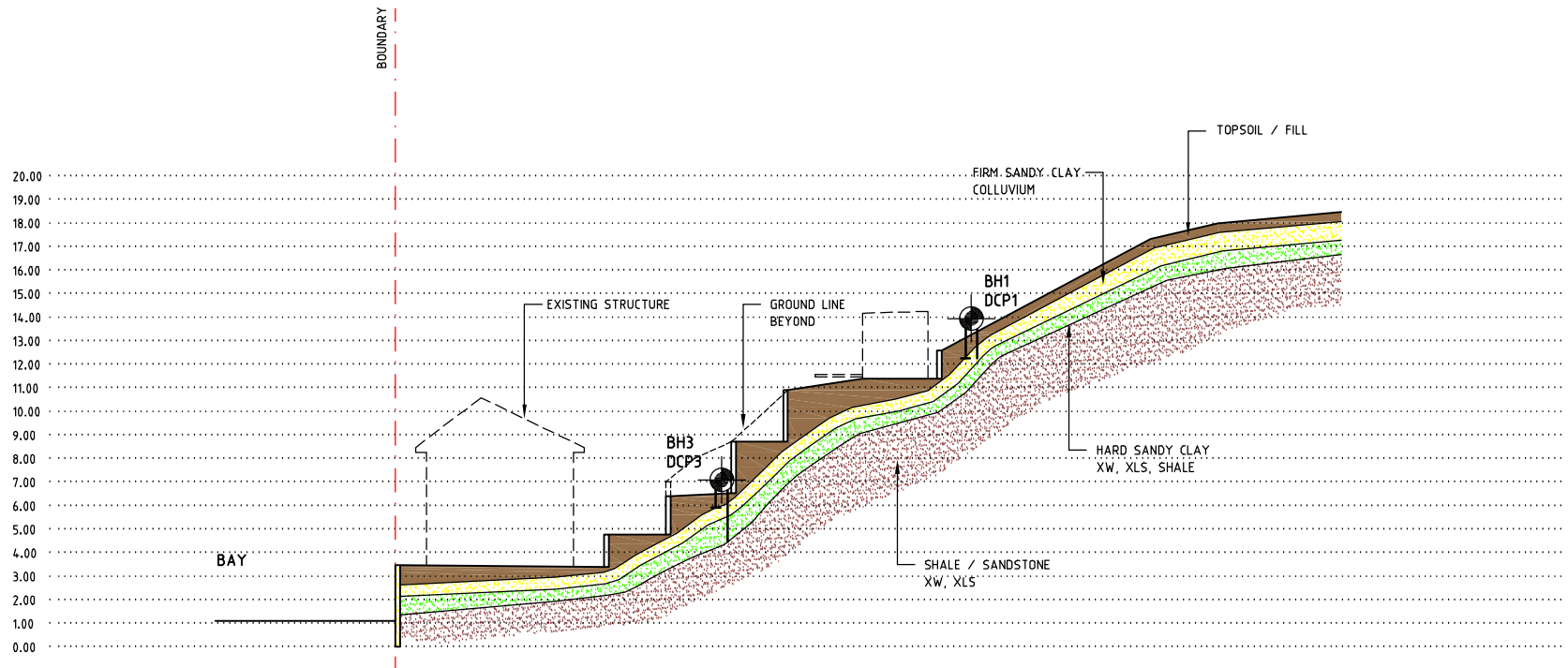
SITE PLAN AND TEST LOCATIONSFIGURE 1

A

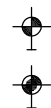
NORTH

A'

SOUTH



GEOLOGICAL MODEL FIGURE 2



AUGER LOCATION

AUGER / DYNAMIC
PENETRATION TESTDCP- DYNAMIC
PENETRATION TEST

BOUNDARY LINE

FILL
BROWN SANDSTIFF TO HARD
SANDY CLAYELS - VLSFIRM / SANDY CLAY
(COLLUVIUM)

SHALE / SANDSTONE

SCALE : 1:200
DRAWING : FIGURE 2
DATE : 19.08.18

PREPARED FOR :
FIONA LOADER

APPROVED BY : K.N.
DRAWN BY : A.C.W.
PROJECT : 2018-116

ADDRESS :
18 - 20 STURDEE LANE
LOVETT BAY, N.S.W.

BOREHOLE LOG

CLIENT: Fiona Loader

DATE: 6/07/2018

BORE No.: 1

PROJECT: Alterations to existing house,
construction of secondary dwelling

PROJECT No.: 2018-116

SHEET: 1 of 1

LOCATION: 18-20 Sturdee Lane, Lovett Bay

SURFACE LEVEL: RL ¹ 13.0m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing		
		Type	Depth (m)	Type	Results	
0.00						
0.40	TOPSOIL/FILL - Dark brown, fine to medium, silty sand with gravel and clay zones.		0.65 0.70			
	Sandy grey CLAY (CL) - Firm to stiff, light brown, low plasticity, dry friable, sandy clay. (Colluvium)					
0.75	Hand Auger Refusal at 0.75m on sandy clay with gravel.	D				
1.00						
2.00						

RIG: N/A

DRILLER: CL LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: No free ground water encountered.

REMARKS:

CHECKED:

BOREHOLE LOG

CLIENT: Fiona Loader

DATE: 6/07/2018

BORE No.: 2

PROJECT: Alterations to existing house,
construction of secondary dwelling

PROJECT No.: 2018-116

SHEET: 1 of 1

LOCATION: 18-20 Sturdee Lane, Lovett Bay

SURFACE LEVEL: RL ¹ 8.5m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing		
		Type	Depth (m)	Type	Results	
0.00						
0.10	TOPSOIL/FILL - Dark brown, fine to medium, dry, silty sand with gravel and clay zones.					
	Sandy SILT/CLAY - Very stiff to hard, brown, fine grained sand with fine to medium grained gravel, friable sandy silt/clay. (Possible fill)		0.20			
		D	0.30			
0.60	Hand Auger Refusal at 0.60m on sandy silt/clay with gravel. (Possible fill)					
1.00						
2.00						

RIG: N/A DRILLER: CL LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: No free ground water encountered.

REMARKS: CHECKED:

BOREHOLE LOG

CLIENT: Fiona Loader

DATE: 6/07/2018

BORE No.: 3

PROJECT: Alterations to existing house,
construction of secondary dwelling

PROJECT No.: 2018-116

SHEET: 1 of 1

LOCATION: 18-20 Sturdee Lane, Lovett Bay

SURFACE LEVEL: RL ¹ 6.4m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing		
		Type	Depth (m)	Type	Results	
0.00	TOPSOIL/FILL - Dark brown, fine to medium grained, moist silty sand.					
0.50	Hand Auger Refusal at 0.50m on silty sand with gravel. (Possible fill)					
1.00						
2.00						

RIG: N/A

DRILLER: CL LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: No free ground water encountered.

REMARKS:

CHECKED:

BOREHOLE LOG

CLIENT: Fiona Loader

DATE: 6/07/2018

BORE No.: 4

PROJECT: Alterations to existing house,
construction of secondary dwelling

PROJECT No.: 2018-116

SHEET: 1 of 1

LOCATION: 18-20 Sturdee Lane, Lovett Bay

SURFACE LEVEL: RL 1 7.5m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing		
		Type	Depth (m)	Type	Results	
0.00						
0.30	TOPSOIL/FILL - Brown, fine to medium grained, moist clayey sand with fine to medium gravel of sandstone.					
	Hand Auger Refusal at 0.30m on clayey sand with gravel. (Possible fill)					
1.00						
2.00						

RIG: N/A

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: No free ground water encountered.

REMARKS:

CHECKED:

DYNAMIC PENETROMETER TEST SHEET

CLIENT: Fiona Loader

DATE: 6/07/2018

PROJECT: Alterations to existing house, co

PROJECT No.: 2018-116

LOCATION: 18-20 Sturdee Lane, Lovett Bay

SHEET: 1 of 1

Depth (m)	Test Location							
	DCP1	DCP2	DCP3	DCP4				
0.00 - 0.15	4	5	1	--				
0.15 - 0.30	2	10	4	--				
0.30 - 0.45	2	19	5	3				
0.45 - 0.60	4	15	5	6				
0.60 - 0.75	3	4	3	16				
0.75 - 0.90	3	9	2	20				
0.90 - 1.05	3	7	3	10				
1.05 - 1.20	5	5	2	6				
1.20 - 1.35	13	7	2	17				
1.35 - 1.50	14	10	4	35				
1.50 - 1.65	12	14	4	End				
1.65 - 1.80	22	23	6					
1.80 - 1.95	34	22	9					
1.95 - 2.10	End	22	14					
2.10 - 2.25		End	32					
2.25 - 2.40			End					
2.40 - 2.55								
2.55 - 2.70								
2.70 - 2.85								
2.85 - 3.00								

TEST METHOD: AS 1289. F3.2, CONE PENETROMETER
AS 1289. F3.3, PERTH SAND PENETROMETER

REMARKS: (B) Test hammer bouncing upon refusal on solid object
-- No test undertaken at this level due to prior excavation of soils

Appendix 3

TABLE : A

Landslide risk assessment for Risk to life

HAZARD	Description	Impacting	Likelihood of Slide	Spatial Impact of Slide		Occupancy	Evacuation	Vulnerability	Risk to Life
A	Landslip (earth slide 2m³) from soils at crest of excavation for retaining structures		Likely excavation within fill/colluvial soils over residual soils then bedrock up to approximately 2.00m depth.	a) Base of excavation		a) Person in area new section of basement 8 hrs per/day average.	a) Likely to not evacuate	a) Person in building, unlikely impacted	
			Possible	Prob. of Impact	Impacted				
		a) Base of excavation	0.001	1.00	0.10	0.3330	0.75	0.1	2.50E-06

* hazards considered in current condition and/or without remedial/stabilisation measures

* likelihood of occurrence for design life of 100 years

* Spatial Impact - Probability of Impact refers to slide impacting structure/area expressed as a % (1.00 = 100% probability of slide impacting area if it occurs), Impacted refers to % of area/structure impacted if slide occurred

* neighbouring houses considered for bedroom impact unless specified

* considered for person most at risk

* considered for adjacent premises/buildings founded via shallow footings unless indicated

* evacuation scale from Almost Certain to not evacuate (1.0), Likely (0.75), Possible (0.5), Unlikely (0.25), Rare to not evacuate (0.01). Based on likelihood of person knowing of landslide and completely evacuating area prior to landslide impact.

* vulnerability assessed using Appendix F - AGS Practice Note Guidelines for Landslide Risk Management 2007

TABLE : B

Landslide risk assessment for Risk to Property

HAZARD	Description	Impacting	Likelihood		Consequences		Risk to Property
A	Landslip (earth slide 2m ³) from soils at crest of excavation for retaining structures	a) Base of excavation	Unlikely	The event might occur under very adverse circumstances over the design life.	Minor	Limited Damage to part of structure or site requires some stabilisation or INSIGNIFICANT damage to neighbouring properties.	Low

* hazards considered in current condition, without remedial/stabilisation measures and during construction works.

* qualitative expression of likelihood incorporates both frequency analysis estimate and spatial impact probability estimate as per AGS guidelines.

* qualitative measures of consequences to property assessed per Appendix C in AGS Guidelines for Landslide Risk Management.

* Indicative cost of damage expressed as cost of site development with respect to consequence values: Catastrophic : 200%, Major: 60%, Medium: 20%, Minor: 5%, Insignificant: 0.5%.

TABLE: 2

Recommended Maintenance and Inspection Program

Structure	Maintenance/ Inspection Item	Frequency
Stormwater drains.	Owner to inspect to ensure that the drains, and pipes are free of debris & sediment build-up. Clear surface grates and litter.	Every year or following each major rainfall event.
Retaining Walls. or remedial measures	Owner to inspect walls for deviation from as constructed condition and repair/replace. Replace poorly constructed rock walls	Every two years or following major rainfall event. As soon as practicable
Large Trees on or adjacent to site	Arbourist to check condition of trees and remove as required. Where tree within steep slopes or adjacent to structures require geotechnical inspection prior to removal	Every five years
Slope Stability	Hydraulics (stormwater) & Geotechnical Consultants to check on site stability at same time and provide report.	One year after construction is completed.

N.B. Provided the above shedule is maintained the design life of the property should conform with Pittwater Councils Risk Management Policy.

Appendix 4

APPENDIX A

DEFINITION OF TERMS

INTERNATIONAL UNION OF GEOLOGICAL SCIENCES WORKING GROUP
ON LANDSLIDES, COMMITTEE ON RISK ASSESSMENT

Risk – A measure of the probability and severity of an adverse effect to health, property or the environment.

Risk is often estimated by the product of probability x consequences. However, a more general interpretation of risk involves a comparison of the probability and consequences in a non-product form.

Hazard – A condition with the potential for causing an undesirable consequence (*the landslide*). The description of landslide hazard should include the location, volume (or area), classification and velocity of the potential landslides and any resultant detached material, and the likelihood of their occurrence within a given period of time.

Elements at Risk – Meaning the population, buildings and engineering works, economic activities, public services utilities, infrastructure and environmental features in the area potentially affected by landslides.

Probability – The likelihood of a specific outcome, measured by the ratio of specific outcomes to the total number of possible outcomes. Probability is expressed as a number between 0 and 1, with 0 indicating an impossible outcome, and 1 indicating that an outcome is certain.

Frequency – A measure of likelihood expressed as the number of occurrences of an event in a given time. See also Likelihood and Probability.

Likelihood – used as a qualitative description of probability or frequency.

Temporal Probability – The probability that the element at risk is in the area affected by the landsliding, at the time of the landslide.

Vulnerability – The degree of loss to a given element or set of elements within the area affected by the landslide hazard. It is expressed on a scale of 0 (no loss) to 1 (total loss). For property, the loss will be the value of the damage relative to the value of the property; for persons, it will be the probability that a particular life (the element at risk) will be lost, given the person(s) is affected by the landslide.

Consequence – The outcomes or potential outcomes arising from the occurrence of a landslide expressed qualitatively or quantitatively, in terms of loss, disadvantage or gain, damage, injury or loss of life.

Risk Analysis – The use of available information to estimate the risk to individuals or populations, property, or the environment, from hazards. Risk analyses generally contain the following steps: scope definition, hazard identification, and risk estimation.

Risk Estimation – The process used to produce a measure of the level of health, property, or environmental risks being analysed. Risk estimation contains the following steps: frequency analysis, consequence analysis, and their integration.

Risk Evaluation – The stage at which values and judgements enter the decision process, explicitly or implicitly, by including consideration of the importance of the estimated risks and the associated social, environmental, and economic consequences, in order to identify a range of alternatives for managing the risks.

Risk Assessment – The process of risk analysis and risk evaluation.

Risk Control or Risk Treatment – The process of decision making for managing risk, and the implementation, or enforcement of risk mitigation measures and the re-evaluation of its effectiveness from time to time, using the results of risk assessment as one input.

Risk Management – The complete process of risk assessment and risk control (*or risk treatment*).

Individual Risk – The risk of fatality or injury to any identifiable (named) individual who lives within the zone impacted by the landslide; or who follows a particular pattern of life that might subject him or her to the consequences of the landslide.

Societal Risk – The risk of multiple fatalities or injuries in society as a whole: one where society would have to carry the burden of a landslide causing a number of deaths, injuries, financial, environmental, and other losses.

Acceptable Risk – A risk for which, for the purposes of life or work, we are prepared to accept as it is with no regard to its management. Society does not generally consider expenditure in further reducing such risks justifiable.

Tolerable Risk – A risk that society is willing to live with so as to secure certain net benefits in the confidence that it is being properly controlled, kept under review and further reduced as and when possible.

In some situations risk may be tolerated because the individuals at risk cannot afford to reduce risk even though they recognise it is not properly controlled.

Landslide Intensity – A set of spatially distributed parameters related to the destructive power of a landslide. The parameters may be described quantitatively or qualitatively and may include maximum movement velocity, total displacement, differential displacement, depth of the moving mass, peak discharge per unit width, kinetic energy per unit area.

Note: Reference should also be made to Figure 1 which shows the inter-relationship of many of these terms and the relevant portion of Landslide Risk Management.

PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007
APPENDIX C: LANDSLIDE RISK ASSESSMENT
QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY

QUALITATIVE MEASURES OF LIKELIHOOD

Approximate Annual Probability		Implied Indicative Landslide Recurrence Interval		Description	Descriptor	Level
Indicative Value	Notional Boundary					
10 ⁻¹	5x10 ⁻²	10 years	20 years	The event is expected to occur over the design life.	ALMOST CERTAIN	A
10 ⁻²		100 years		The event will probably occur under adverse conditions over the design life.	LIKELY	B
10 ⁻³	5x10 ⁻³	1000 years	200 years 2000 years	The event could occur under adverse conditions over the design life.	POSSIBLE	C
10 ⁻⁴		10,000 years		The event might occur under very adverse circumstances over the design life.	UNLIKELY	D
10 ⁻⁵	5x10 ⁻⁵	100,000 years	20,000 years	The event is conceivable but only under exceptional circumstances over the design life.	RARE	E
10 ⁻⁶	5x10 ⁻⁶	1,000,000 years	200,000 years	The event is inconceivable or fanciful over the design life.	BARELY CREDIBLE	F

Note: (1) The table should be used from left to right; use Approximate Annual Probability or Description to assign Descriptor, not *vice versa*.

QUALITATIVE MEASURES OF CONSEQUENCES TO PROPERTY

Approximate Cost of Damage		Description	Descriptor	Level
Indicative Value	Notional Boundary			
200%	100%	Structure(s) completely destroyed and/or large scale damage requiring major engineering works for stabilisation. Could cause at least one adjacent property major consequence damage.	CATASTROPHIC	1
60%		Extensive damage to most of structure, and/or extending beyond site boundaries requiring significant stabilisation works. Could cause at least one adjacent property medium consequence damage.	MAJOR	2
20%	40%	Moderate damage to some of structure, and/or significant part of site requiring large stabilisation works. Could cause at least one adjacent property minor consequence damage.	MEDIUM	3
5%	10%	Limited damage to part of structure, and/or part of site requiring some reinstatement stabilisation works.	MINOR	4
0.5%	1%	Little damage. (Note for high probability event (Almost Certain), this category may be subdivided at a notional boundary of 0.1%. See Risk Matrix.)	INSIGNIFICANT	5

- Notes:** (2) The Approximate Cost of Damage is expressed as a percentage of market value, being the cost of the improved value of the unaffected property which includes the land plus the unaffected structures.
- (3) The Approximate Cost is to be an estimate of the direct cost of the damage, such as the cost of reinstatement of the damaged portion of the property (land plus structures), stabilisation works required to render the site to tolerable risk level for the landslide which has occurred and professional design fees, and consequential costs such as legal fees, temporary accommodation. It does not include additional stabilisation works to address other landslides which may affect the property.
- (4) The table should be used from left to right; use Approximate Cost of Damage or Description to assign Descriptor, not *vice versa*

PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

APPENDIX C: – QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY (CONTINUED)

QUALITATIVE RISK ANALYSIS MATRIX – LEVEL OF RISK TO PROPERTY

LIKELIHOOD		CONSEQUENCES TO PROPERTY (With Indicative Approximate Cost of Damage)				
	Indicative Value of Approximate Annual Probability	1: CATASTROPHIC 200%	2: MAJOR 60%	3: MEDIUM 20%	4: MINOR 5%	5: INSIGNIFICANT 0.5%
A – ALMOST CERTAIN	10 ⁻¹	VH	VH	VH	H	M or L (5)
B - LIKELY	10 ⁻²	VH	VH	H	M	L
C - POSSIBLE	10 ⁻³	VH	H	M	M	VL
D - UNLIKELY	10 ⁻⁴	H	M	L	L	VL
E - RARE	10 ⁻⁵	M	L	L	VL	VL
F - BARELY CREDIBLE	10 ⁻⁶	L	VL	VL	VL	VL

Notes: (5) For Cell A5, may be subdivided such that a consequence of less than 0.1% is Low Risk.

(6) When considering a risk assessment it must be clearly stated whether it is for existing conditions or with risk control measures which may not be implemented at the current time.

RISK LEVEL IMPLICATIONS

Risk Level		Example Implications (7)
VH	VERY HIGH RISK	Unacceptable without treatment. Extensive detailed investigation and research, planning and implementation of treatment options essential to reduce risk to Low; may be too expensive and not practical. Work likely to cost more than value of the property.
H	HIGH RISK	Unacceptable without treatment. Detailed investigation, planning and implementation of treatment options required to reduce risk to Low. Work would cost a substantial sum in relation to the value of the property.
M	MODERATE RISK	May be tolerated in certain circumstances (subject to regulator's approval) but requires investigation, planning and implementation of treatment options to reduce the risk to Low. Treatment options to reduce to Low risk should be implemented as soon as practicable.
L	LOW RISK	Usually acceptable to regulators. Where treatment has been required to reduce the risk to this level, ongoing maintenance is required.
VL	VERY LOW RISK	Acceptable. Manage by normal slope maintenance procedures.

Note: (7) The implications for a particular situation are to be determined by all parties to the risk assessment and may depend on the nature of the property at risk; these are only given as a general guide.

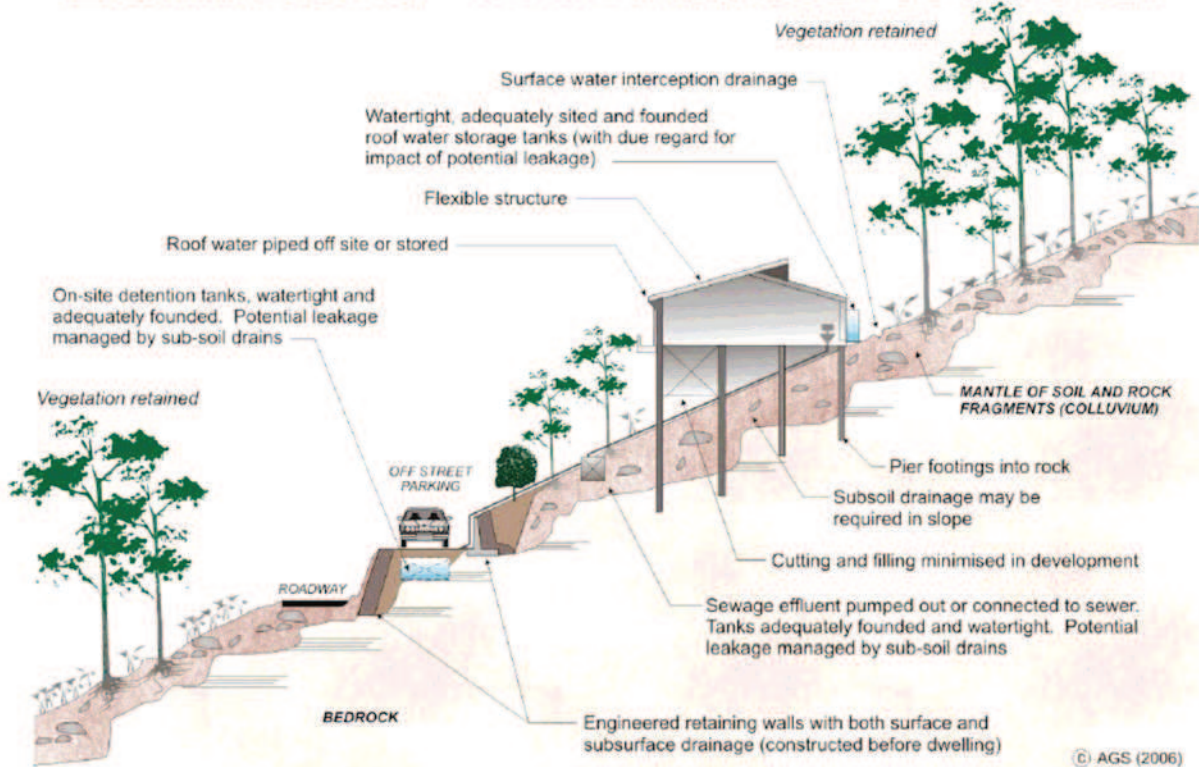
Appendix 5

PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

APPENDIX G - SOME GUIDELINES FOR HILLSIDE CONSTRUCTION

ADVICE		GOOD ENGINEERING PRACTICE	POOR ENGINEERING PRACTICE
GEOTECHNICAL ASSESSMENT	Obtain advice from a qualified, experienced geotechnical practitioner at early stage of planning and before site works.		Prepare detailed plan and start site works before geotechnical advice.
PLANNING			
SITE PLANNING	Having obtained geotechnical advice, plan the development with the risk arising from the identified hazards and consequences in mind.		Plan development without regard for the Risk.
DESIGN AND CONSTRUCTION			
HOUSE DESIGN	Use flexible structures which incorporate properly designed brickwork, timber or steel frames, timber or panel cladding. Consider use of split levels. Use decks for recreational areas where appropriate.		Floor plans which require extensive cutting and filling. Movement intolerant structures.
SITE CLEARING	Retain natural vegetation wherever practicable.		Indiscriminately clear the site.
ACCESS & DRIVEWAYS	Satisfy requirements below for cuts, fills, retaining walls and drainage. Council specifications for grades may need to be modified. Driveways and parking areas may need to be fully supported on piers.		Excavate and fill for site access before geotechnical advice.
EARTHWORKS	Retain natural contours wherever possible.		Indiscriminatory bulk earthworks.
CUTS	Minimise depth. Support with engineered retaining walls or batter to appropriate slope. Provide drainage measures and erosion control.		Large scale cuts and benching. Unsupported cuts. Ignore drainage requirements
FILLS	Minimise height. Strip vegetation and topsoil and key into natural slopes prior to filling. Use clean fill materials and compact to engineering standards. Batter to appropriate slope or support with engineered retaining wall. Provide surface drainage and appropriate subsurface drainage.		Loose or poorly compacted fill, which if it fails, may flow a considerable distance including onto property below. Block natural drainage lines. Fill over existing vegetation and topsoil. Include stumps, trees, vegetation, topsoil, boulders, building rubble etc in fill.
ROCK OUTCROPS & BOULDERS	Remove or stabilise boulders which may have unacceptable risk. Support rock faces where necessary.		Disturb or undercut detached blocks or boulders.
RETAINING WALLS	Engineer design to resist applied soil and water forces. Found on rock where practicable. Provide subsurface drainage within wall backfill and surface drainage on slope above. Construct wall as soon as possible after cut/fill operation.		Construct a structurally inadequate wall such as sandstone flagging, brick or unreinforced blockwork. Lack of subsurface drains and weepholes.
FOOTINGS	Found within rock where practicable. Use rows of piers or strip footings oriented up and down slope. Design for lateral creep pressures if necessary. Backfill footing excavations to exclude ingress of surface water.		Found on topsoil, loose fill, detached boulders or undercut cliffs.
SWIMMING POOLS	Engineer designed. Support on piers to rock where practicable. Provide with under-drainage and gravity drain outlet where practicable. Design for high soil pressures which may develop on uphill side whilst there may be little or no lateral support on downhill side.		
DRAINAGE			
SURFACE	Provide at tops of cut and fill slopes. Discharge to street drainage or natural water courses. Provide general falls to prevent blockage by siltation and incorporate silt traps. Line to minimise infiltration and make flexible where possible. Special structures to dissipate energy at changes of slope and/or direction.		Discharge at top of fills and cuts. Allow water to pond on bench areas.
SUBSURFACE	Provide filter around subsurface drain. Provide drain behind retaining walls. Use flexible pipelines with access for maintenance. Prevent inflow of surface water.		Discharge roof runoff into absorption trenches.
SEPTIC & SULLAGE	Usually requires pump-out or mains sewer systems; absorption trenches may be possible in some areas if risk is acceptable. Storage tanks should be water-tight and adequately founded.		Discharge sullage directly onto and into slopes. Use absorption trenches without consideration of landslide risk.
EROSION CONTROL & LANDSCAPING	Control erosion as this may lead to instability. Revegetate cleared area.		Failure to observe earthworks and drainage recommendations when landscaping.
DRAWINGS AND SITE VISITS DURING CONSTRUCTION			
DRAWINGS	Building Application drawings should be viewed by geotechnical consultant		
SITE VISITS	Site Visits by consultant may be appropriate during construction/		
INSPECTION AND MAINTENANCE BY OWNER			
OWNER'S RESPONSIBILITY	Clean drainage systems; repair broken joints in drains and leaks in supply pipes. Where structural distress is evident see advice. If seepage observed, determine causes or seek advice on consequences.		

EXAMPLES OF **GOOD** HILLSIDE PRACTICE



EXAMPLES OF **POOR** HILLSIDE PRACTICE

