

| <u>Date</u> | <u>Revision</u> |
|------------------|-----------------|
| 3 September 2015 | A |

Icon Homes
PO Box 733
FRESHWATER NSW 2096

Our Ref AWG39667
Your Ref

Site Classification as per AS2870-2011

No.532 Pittwater Road, North Manly

| | |
|---------------------|--|
| Site Classification | CLASS P |
| Site Features | Existing dwelling with grasses and trees |
| Ground Slope | Gentle |
| Proposed Earthworks | Unknown (refer "about your report") |
| Ys Range (normal) | 10-20 mm (Hs = 1800 mm) |
| Ips Value | Too sandy to test |
| Water Table | Not present |

Allowable Bearing Pressures

| | |
|---------|---|
| <50 kPa | At all levels in the natural undisturbed strata |
| 150 kPa | Founded 3000mm and deeper below existing ground level |

The pages that form the last six pages of this report are an integral part of this report. The notes contain advice and recommendations for all stakeholders in this project (i.e. the structural engineer, builder, owner and future owners) and should be read and followed by all concerned. This report may only be copied in full. If there is any doubt whether this report is complete, please check with our office.

Please note that should additional information become available that was not supplied or known at the time of our testing, we reserve the right to revise this report without penalty.

Site Specific Notes

Our testing has encountered significant depth of sand. Within the scope of this report, we can only note the reactivity (negligible) and the bearing capacity of the sand. Sands can be unpredictable when drilled or excavated which is related to grain size and moisture content. Some sands will perform in an acceptable fashion but others will collapse at shallow angles causing excessive blow-out of excavations, which results in problems with keeping pier holes open and standing batters at reasonable angles. If these problems do occur, in most cases a competent contractor can cope, but occasionally further advice and/or testing is required.

The following allowable bearing pressures are available for strip footings and embedment depths, into the natural sands below any fill;

| Depth | Width | | |
|-------|--------|--------|--------|
| | 300mm* | 450mm* | 600mm* |
| 300mm | 60kPa | 80kPa | 105kPa |
| 450mm | 65kPa | 90kPa | 110kPa |
| 600mm | 75kPa | 105kPa | 120kPa |

*Plus depth of fill

This site has received a P Classification as we have encountered strata with a bearing pressure less than the prescribed minimum as outlined in AS2870-2011.

Because of the low reactivity of the strata encountered, in our judgement the provisions of Clause 1.3.3 of AS2870-2011 are not applicable in this case.

There is an existing dwelling on this site which, when removed, will cause some disturbance to the strata down to depths equal to the depth of the footing.

We have assumed that this disturbance will be back-compacted so the performance of the proposed footings is not compromised. If during the earthworks phase it is apparent that the disturbed ground is proving problematic, then the design engineer must be consulted to reconsider the situation.

Furthermore, there are generally several uncharted abandoned sub-surface pipes, which generally hold a limited amount of water both within themselves and in the sand bed around them. If footing excavations encounter any of these pipes some local seepage may occur, but normally a competent contractor can cope with this situation.

Screw piers may be suitable for this development, however further testing is required.

NOTE: Because of limited access, drilling at TS No.2 was carried out with a portable auger. If the design depth of piers (i.e. tree piers or sewer piers etc) is deeper than the depth of our test holes further testing with our 4WD mounted drill rig is recommended (once better access becomes available) or an onsite inspection by a suitable qualified person to confirm the strata below the 1500mm level and the approximate set depths of the proposed piers at time of construction.

Note: Cutting and filling the site by depths equal to or greater than 400mm will result in a 'P' classification, which may increase the design 'ys'. Therefore, when the proposed cut and fill earthworks is known, we should be contacted for further advice.

Although no water table was encountered during our testing, a perched water table or water seepage can occur during or after wet periods, generally where a porous layer overlies less porous strata. This generally results in some water seepage into excavations down to this level but a competent contractor can usually resolve this issue.

Unless specifically mentioned elsewhere within this report, we make no representation about the trafficability of the site during construction, however the thicker the topsoil/estate dressing, the greater the problem with moving construction equipment during or after rain periods.

AW Geotechnical



Bruce L Hargreaves

Dip.App.Sc (Geology)

RPGeo (Geotechnical Engineering)

Affil.I.E. (Aus)., M.A.G.S.,

BSA Licence No. 1058767 (Site Classifier)

TCC Accreditation No. CC4047U (Engineer-Geotechnical)

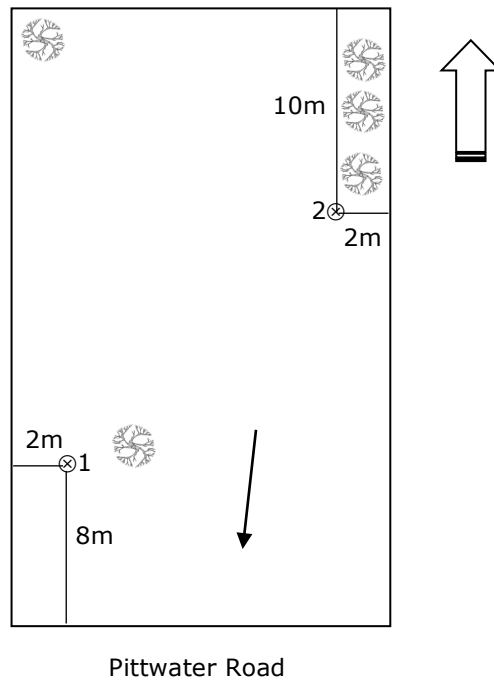
References

- AS 2870-2011 "Residential Slabs & Footings"*
AS 2870-1996 Supplement 1-1996 "Residential Slabs & Footings – Construction Commentary"
SAA HB 28-1997 "The Design of Residential Slabs & Footings"
CSIRO "Foundation Maintenance & Footing Performance A Home Owner's Guide" (Sheet BTF18)
CSIRO "Plant Roots in Drains – Prevention and Cure" (Sheet BTF17)
AS4055-2012 "Wind Loads for Housing"

| TEST SITE 1 | | | | | TEST SITE 2 | | | | |
|---------------|---|------|-----|-----------|---------------|---|------|-----|-----------|
| Depth (mm) | Description Soil Type-Colour-Consistency | FILL | DCP | PP kPa | Depth (mm) | Description Soil Type-Colour-Consistency | FILL | DCP | PP kPa |
| 100 | TOPSOIL | | 2 | | 100 | TOPSOIL | | 1 | |
| 200 | | | 3 | | 200 | | | 1 | |
| 300 | SAND | | 2 | | 300 | SAND | | 1 | |
| 400 | (gy) | | 3 | | 400 | (gy) | | 2 | |
| 500 | moist and med dense | | 2 | | 500 | moist and loose | | 1 | |
| 600 | | | 2 | | 600 | | | 1 | |
| 700 | | | 3 | | 700 | | | 2 | |
| 800 | | | 4 | | 800 | | | 1 | |
| 900 | | | 4 | | 900 | | | 1 | |
| 1000 | | | 3 | | 1000 | | | 1 | |
| 1100 | | | 3 | | 1100 | | | 1 | |
| 1200 | | | 4 | | 1200 | | | 1 | |
| 1300 | | | 4 | | 1300 | | | 1 | |
| 1400 | | | 4 | | 1400 | | | 1 | |
| 1500 | | | 5 | | 1500 | | | 1 | |
| 1600 | | | 4 | | 1600 | END H/A – Limit of testing | | 1 | |
| 1700 | | | 4 | | 1700 | | | 1 | |
| 1800 | | | 3 | | 1800 | | | 1 | |
| 1900 | | | 4 | | 1900 | | | 1 | |
| 2000 | | | 4 | | 2000 | | | 2 | |
| 2100 | | | 5 | | 2100 | | | 2 | |
| 2200 | | | 5 | | 2200 | | | 2 | |
| 2300 | | | 4 | | 2300 | | | 2 | |
| 2400 | | | 4 | | 2400 | | | 3 | |
| 2500 | | | 3 | | 2500 | | | 3 | |
| 2600 | | | 2 | | 2600 | | | 2 | |
| 2700 | | | 3 | | 2700 | | | 3 | |
| 2800 | | | 3 | | 2800 | | | 3 | |
| 2900 | | | 3 | | 2900 | | | 4 | |
| 3000 | | | 3 | | 3000 | | | 5 | |
| 3100 | | | 4 | | 3100 | | | 4 | |
| 3200 | | | 5 | | 3200 | | | 5 | |
| 3300 | (dense) | | 6 | | 3300 | | | 6 | |
| 3400 | | | 9 | | 3400 | | | 7 | |
| 3500 | | | 10 | | 3500 | | | 10 | |
| 3600 | | | 13 | | 3600 | | | 13 | |
| 3700 | | | 16 | | 3700 | | | 14 | |
| 3800 | | | +25 | | 3800 | | | 16 | |
| 3900 | | | utp | | 3900 | | | +25 | |
| 4000 | | | | | 4000 | | | utp | |

NOMENCLATURE: UTP=Unable to Penetrate DCP=9kg Dynamic Cone Penetrometer PP = Pocket Penetrometer A=Auger XW-ROCK=Extremely Weathered Rock Refer Tables 7.3.2 & 7.3.3 AS1726-1993 gy=grey or=orange yell=yellow rd=red wh=white brn=brown bk=black bl=blue gr=green Refer AS1726-1993 Clause A2.4 for classifying soils.

Site Sketch (Not to scale)



Site Photographs



About Your Report

This is a site classification report generally in accordance with AS 2870-2011 and should be sufficient for a qualified person to design footings for structures covered under the scope of this standard.

Where our proposed earthworks specification states "Unknown", AS 2870-2011 Clause 2.5.2 requires the site to be reclassified prior to footing construction if the proposed cut exceeds the lesser of 0.25H_s or 500 mm and the proposed fill exceeds the limits in Clause 2.5.3 of AS 2870-2011. In these instances, the site classification is in the "as tested" state and may not reflect the final site classification after earthworks. Normally this re-classification is done by the design engineer, but upon request, we can do this.

Where the site preparation is stated as "known", our classification is based on the data given, as we envisage the finished building footprint (which conforms to the AS 2870-2011 guidelines), therefore re-classification is only required if these guidelines change. This report may not be adequate for large complex dwellings that are generally outside the scope of AS 2870-2011.

AS 2870-2011 contains a system of classifying soils based on their ability to change volume with changes in soil moisture. These classes are Class A, Class S, Class M, Class H1, Class H2 and Class E (the most severe). These "Normal" classes also have a minimum allowable bearing capacity as outlined in Clause 2.4.5 of AS 2870-2011.

AS 2870-2011 also has a Class P for problem sites covering fill, soft or collapsing soils, potential slope stability problems, mining subsidence and abnormal moisture conditions.

Abnormal Moisture Conditions (AMC) is a particularly contentious area and Clause 1.3.3 of AS 2870-2011 covers many situations where this clause applies. The most common situations are sites with clay soils (normally Class M, H1, H2 or E (ys > 20)) that have either existing structures or trees or gardens within the zone of influence of the proposed footing. Some of these trees may be on adjoining properties. Where this clause is applicable, we have added further explanatory advice.

The soil shrinkage index (Ips) range quoted in this report was assigned after considering the guidelines in Section 2 of AS 2870-2011 and from this we have derived a ys, which is the "characteristic surface movement" under NORMAL moisture conditions.

Footings designed in accordance with AS 2870-2011 have a long-term performance criteria and it should be noted that this does not offer a crack or distress-free performance. It offers a performance criteria that ensures a low probability of foundation failure, provided abnormal moisture conditions, such as over-watering, bad drainage, leaking pipes or nearby trees are not allowed to exist or develop.

These performance criteria are outlined in Appendix C of AS 2870-2011 and under normal conditions a low incidence of Category 1 damage and an occasional incidence of Category 2 damage is expected. This appendix is available from our office upon request.

Where Abnormal Moisture Conditions exist and/or are allowed to continue or develop, then not only will the above probabilities increase, but the damage will be greater. The ultimate responsibility falls on the design engineer to negate the effects of these conditions when they are known and for the owner/occupier to ensure

that they do not develop. Our responsibility is limited to identifying these conditions.

If any potential owner is not satisfied with the performance criteria in AS 2870 (which has been applied Australia wide since 1986) then prior to footing design he/she should consult with the design engineer and have a specially designed footing more suited to their needs.

Classification Limitations

The content of this report is based on the expertise and experience of the author representing this company. Our commission didn't extend to assessing instability due to previous or existing sub-surface mining, landslip or earthquakes, nor did it extend to testing to comply with the relevant contaminated land act or for acid sulfate soils (see note below). If, however any of these exclusions was obvious or where the allotment is within an area where we are aware of a past history of these exclusions, we have made comment and given further advice.

This report is based on the assumption that the test results are representative of the true site conditions. Even under optimum circumstances, actual conditions may differ from those reported to exist. Although our investigation exceeds the minimum requirements of AS 2870-2011, economic constraints necessarily limit the practical extent of any investigation. We therefore cannot accept responsibility for conditions encountered on this site outside the areas tested which are different to those reported. The positions of these test sites have not been surveyed, and should be regarded as approximate. We have followed AS 2870-2011 soil descriptions contained in Clause C2.1 rather than AS 1289 because where there is a conflict between referenced codes, AS 2870-2011 takes precedence.

Underslab Termiticide Irrigation Systems

These are becoming popular and besides serving their obvious purpose, they also inject extra moisture beneath the slab at various times (measured in years). This creates long term "abnormal" moisture conditions that needs to be addressed at the design stage, therefore if one of these is proposed for this project, the design engineer must be informed prior to preparing the slab.

As a general rule, to cope with these systems, the ys must be increased by about 50%, which will generally result in a slab one category higher than would normally be used (refer P12, Supplement to AS 2870-2011). Upon request we can supply more specific advice.

Acid Sulfate Soils (ASS) & Saline Soils

Unless specifically stated, we have not considered the possibility of ASS, which occur around the coastline, generally below AHD 5.0 and occasionally on broad river flood plains at higher levels. Most Councils maintain maps of these areas. In new estates the ASS problem has normally been assessed and neutralised, but it is worthwhile confirming this at land sales, if ASS are suspected. In older areas, the council is normally the best source of advice. ASS, if present, do have the potential to dramatically shorten the life of footings, slabs, reinforcement and bricks. This advice is also relevant for saline soils. Unless specifically stated, we have not considered the possibility of Saline Soils, however we can provide a quotation to complete this testing.

Filled Ground

Controlled Fill - Material that has been placed and compacted in layers by compaction equipment within a defined moisture range to a defined density requirement in accordance with AS 3798-2007 Clause 6.4.2 of AS 2870-2011 defines controlled fill.

Uncontrolled Fill - Fill that does not have sufficient documentation to be classified as controlled is by exclusion, uncontrolled. Where found we have offered further advice within this report.

Topsoil/Estate Dressing

In our soil log section, where we have logged "Topsoil" or "Estate Dressing" it is defined as per clause 1.2.15 of AS 3798-2007 thus:

"A poorly compacted superficial soil containing some organic matter, usually darker than the underlying soils"

Good building practice dictates that all heavy organic strata be scraped clear of the building envelope during the early stages of site preparation and we have assumed that this will be done.

Short Term Site Management

This is the responsibility of the builder, and besides ensuring that the site is handed over to the owner at completion in accordance with accepted practice, the following should also be done:

- Ensure all service trenches are back-filled as soon as possible in accordance with Clause 6.6 of AS 2870-2011, including the clay plug where a service pipe trench exits the building footprint.
- Ensure guttering is connected to the stormwater (via temporary pipes if necessary) as soon as the roof is on.
- Ensure that during construction and at the time of hand-over that the site is maintained as per Clause 5.2.1 of AS 2870-2011.

If any of these practices are not carried out, the site may develop "abnormal" moisture conditions, increasing the risk of damage above the AS 2870-2011 criteria.

Other Construction Issues

The builder must also ensure that other sub-trades such as plumbers, drainers and swimming pool contractors don't establish excavations within the critical zone of influence of the footing system unless the footing is pierced below the influence of these excavations. This critical zone varies from 20° (1V:2H) to 45° (1V:1H), depending on the nature of the strata. If this situation is considered possible, then once the proposal is known we can offer further advice. These excavations include inground tanks. Unless we have specifically given written approval, no inground tanks should be sited within 8 metres of any structural footing.

Furthermore, there should be no in ground disposal or storage of water, (i.e. soakage pits, rubble pits, rain gardens or similar), within eight (8) metres of a structural footing, without our prior written approval.

Where the proposed earthworks involve the establishment of cut/fill batters, advice concerning safe angles is beyond the scope of commission in this report. AS 2870-2011, Clause 6.4.4 offer guidelines.

Long Term Site Management

It is the owner's responsibility to ensure both tenants and future owners are aware of these responsibilities. The referenced CSIRO sheets outline these responsibilities and if the builder does not give the owner a copy, they can be sourced from either the CSIRO (1800 645 051) or our office.

The major danger to dwellings is allowing site conditions to deteriorate to "abnormal" in the long term.

Where abnormal moisture conditions are allowed to continue or to develop, then not only will the above probabilities increase, but the damage will be greater.

The CSIRO sheets define both "normal" and "abnormal" conditions.

The significant (not necessarily in order) abnormal conditions that adversely affect the performance of AS 2870-2011 type footings are:

- Trees growing or allowed to grow within the critical zone of influence of the footings.
- Poor site drainage
- Saturated service trenches (poor site drainage).
- Leaking service pipes

The builder, owner/occupier and engineer should take note that management of trees is the most difficult part of the site management procedures and trees present the greatest risk to the future poor performance of the footing system. Trees (existing or proposed) must not be allowed to grow without taking action to negate their effects within the critical zone of the footing system.

| <u>Class</u> | <u>Normal ys</u> | <u>Critical Zone</u> |
|--------------|------------------|-------------------------|
| Class M | < 40mm | .75 times mature height |
| Class H1 | 40-60mm | 1.0 times mature height |
| Class H2 | 60-75mm | 1.0 times mature height |
| Class E | 75-100mm | 1.5 times mature height |
| Class E | >100mm | 2 times mature height |

These spacings must be increased for groups or rows of trees.

These distances are only a "rule of thumb" as the tree species and their root systems play an equally important role



PO Box 4044 | Eight Mile Plains | 4113 |ph 0433 242 748 | bruce2@ozemail.com.au

Understanding soils, trees and how they can affect your house.

This document is a plain language guide to what should be expected from the construction of single dwellings, townhouses or similar structures not situated vertically above or below another dwelling. It has been compiled by the HEDRA Task Force committee in the belief that the information contained is helpful to the parties mentioned, however no warranty of accuracy or reliability as to the information is given, and no responsibility for loss arising is accepted.

1. EXPLANATIONS

Footings (often incorrectly called foundations) are the “members” that support the building. They are commonly concrete slabs or timber floors supported by strips and stumps. (Fig 1, 2 & 3).

Foundation is the soil or rock supporting the footings. **Reactive Clay foundations** are those that shrink and swell with changing moisture and cause the building and paving to sink or lift.

Reverse slope is one that slopes towards the building. (Fig 18) **Sand foundations** do not shrink or swell but if they are loose they can cause the building to sink. **The Australian Standards** for building footing construction permits minor wall and floor movements. If the foundation conditions are changed after construction the floor and walls may move more than allowed-for by these standards. The designs for building footings in Australian Standard 2870 will perform adequately provided the building site and surrounds have “normal” foundation conditions which are maintained. If the building site and surrounds have “abnormal” moisture conditions, special provisions must be followed by the design engineer, builder and owners. (**AS2870 defines “abnormal” moisture conditions**)

The “reactivity” of clays is their capacity to shrink and swell with changing moisture and is classified as follows :

| | |
|-------------------|----------------------|
| A | Reactivity absent |
| S | Slight reactivity |
| M or M-D | Moderate reactivity |
| H1 or H1-D | High reactivity |
| H2 or H2-D | Very High reactivity |
| E or E-D | Extreme reactivity |

The greater the clay “reactivity” the greater the possibility of damage. Some minor cracking of walls is almost inevitable despite proper design, construction and maintenance. AS2870 suggests that cracks up to 1 mm wide are common and that

cracks up to 5 mm may occur in clay sites subject to significant moisture changes. Some cracks are seasonal but if larger than 5 mm they are regarded as significant and should be investigated before becoming larger.

Fig. 1 Stiffened Raft

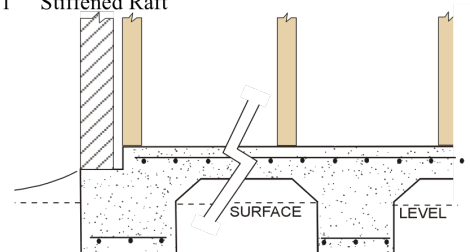


Fig 2 Waffle Slab

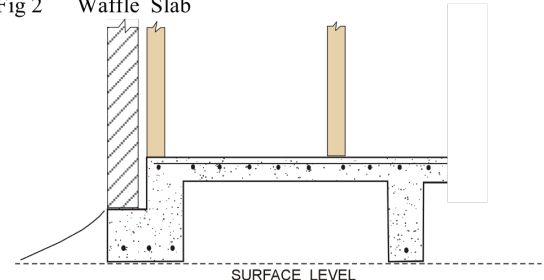
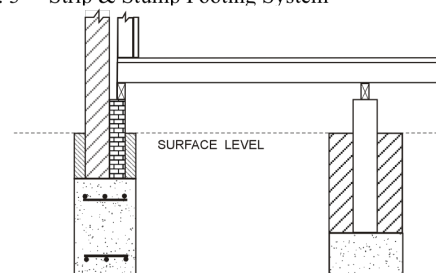


Fig. 3 Strip & Stump Footing System



2. ENGINEERING

The engineer designs house footings to ensure that they can cope with the soil and environmental conditions assessed at the time of the site investigation and perform to their design potential.

3. BUILDING

In the construction of a building the builder needs to comply the Building Code of Australia, relevant Australian Standards, engineering specifications and contract documents. (Fig. 4) The following are important aspects the builder will need to address:

- Builders should ensure that owners understand that failure to maintain adequate drainage may result in damage to the structure.
- Well-drained foundation conditions, which will create "normal" soil moisture and adequate bearing capacity.
- Ensuring that excavations are well supported or are dug to avoid collapses. (Fig. 11)
- Constructing well-compacted and retained 'soil aprons' around the building to stop erosion.
- Special considerations if any excavations are to be dug near adjoining structures. (Fig. 11)
- Sloping the soil and paths away from the building by the minimum amount required by the building regulations to prevent water flowing towards the building foundations. (Fig. 10 & 18)
- Constructing soil drains or moisture barriers in sloping sites to prevent stormwater adversely affecting the building foundations.
- In highly or extremely reactive clay sites Australian Standard 2870 – "Residential slabs and footings" requires *mechanical flexible couplings* for sub-surface drainage pipes and for above-ground connections from the downpipe to the storm water drains. These allow for the movement of the soil and minimise the risk of pipe joints breaking and creating leakage problems. (Fig.6).

4. HOME OWNERS

The home owner should read and become familiar with the Site Classification report provided prior to construction and the type of footing system used in the building. To comply with Australian Standard 2870 – "Residential slabs and footings", and achieve acceptable performance and safety during the design life of the house, the owners shall maintain the garden and foundation soil moistures, paving and drainage systems. (Fig. 7)

Failure to maintain the foundation conditions can lead to cracking of walls and floors. Damage to a building that can be attributed to actions of the owner could diminish the builder's warranty obligations, leaving the owner responsible for the cost of repairs

Fig. 4

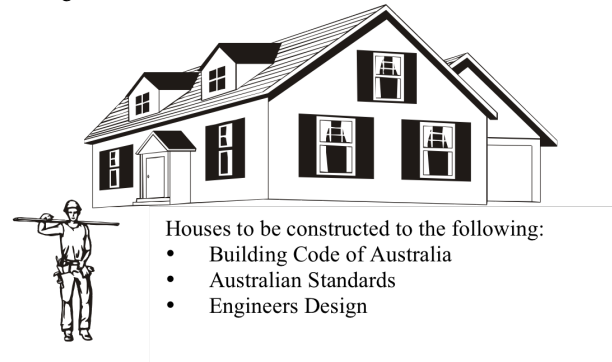


Fig. 5 Well Drained Sites

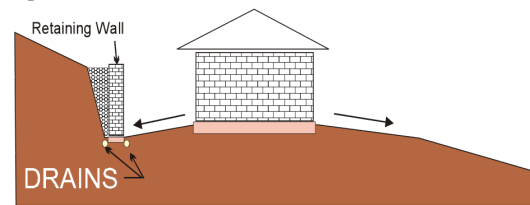


Fig. 6 Mechanical Flexible Couplings to reduce the potential of broken pipes in M/M-D, H1/H1-D, H2/H2-D & E /E-D sites plus all clay based sites with trees

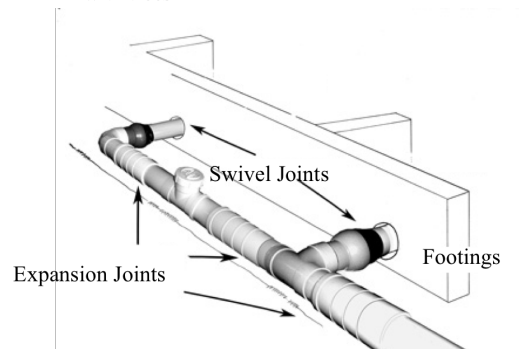


Fig.7



WORKS AFTER TAKING POSSESSION

In some cases foundation conditions are changed by the owner constructing new works such as:

- Constructing sheds or outdoor roofed areas without connecting the roof drainage to storm water lines.
- Constructing paving around the building without sufficient slope away from the building. (In sandy soils and low and moderate “reactivity” clays, a slope of 1:40 up to 1 metre away from the building is adequate. In highly reactive clays a slope of 1:20 works better. In large paved areas a drain and collection pit may be necessary). (Fig. 5 & 18)
- Australian Standard 2870, “Residential Slabs and Footings” requires soil drains and “normal” soil garden moisture in M, H1, H2, E, and P sites to be maintained by the owner. (Fig 10)
- Running machinery over shallow drain pipes may break them causing leaks and subsequent foundation movements.
- Any excavations close to building footings can cause them to sink by disturbing the foundation material or by drying the foundation clay. (Fig 11)
- Footings constructed in reactive clay sites during wet periods may be damaged if the garden is allowed to dry out excessively.
- Footings constructed in reactive clay sites during dry conditions may experience damage if the garden is watered unevenly or excessively.

5. LANDSCAPING AND TREES

Most modern allotments with clayey soils are too small to safely grow large trees without special footings. Generally the larger the root system of the tree(s) the greater the drying effect. If in doubt seek the advice of an expert arboriculturist and designing engineer.

If you are about to build in a clay area and you wish to grow, retain or remove trees near buildings, the builder should be advised of this prior to signing the building contract so that the engineer can design for these conditions.

- Trees can cause damage during their life and even for many months after their removal. If they do not receive sufficient water while alive their roots will dry the soil near buildings or under pavements.

Fig. 8 Drainage concerns

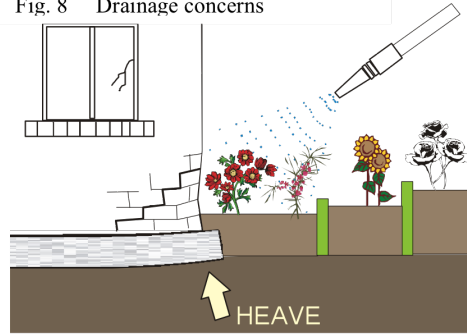


Fig. 9 Slab heave due to water ponding

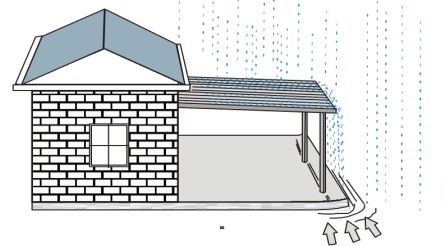


Fig. 10 Soil Drainage Plan

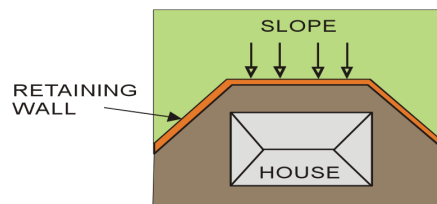


Fig. 11 De-stabilizing house foundations

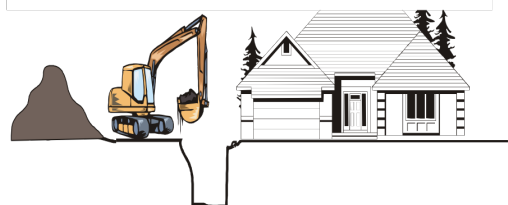
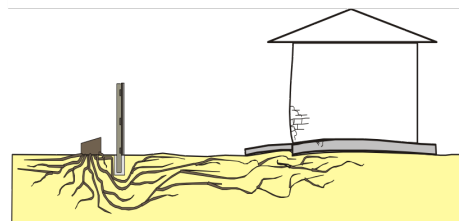


Fig. 12 Damage due to soil moisture changes



If you plan to remove trees after the building is constructed you should consult the designing engineer an expert arboriculturist or a geotechnical practitioner familiar with these problems.

Tree roots in sandy areas rarely cause any damage since sand does not shrink or swell, however if the root ball or large root is very close to a building it may grow and lift the footings of a light structure. (Fig. 13)

Foundation problems in clay sites may also be caused by :

- Excessive watering or under-watering of gardens.
- Watering systems that are overused or discharge water too close to building walls (Fig. 8)
- Constructing terraces, retaining walls or garden walls without good drainage. (Fig. 10)

6. POOR SITE MAINTENANCE

The change of foundation soil moisture is by far the greatest cause of building damage. Changes of drainage or garden watering conditions in adjoining properties can also create problems.

- A drainage system may be necessary if water flows near the building. All possible water leaks and sources should be repaired immediately, e.g.:
- Leaking or blocked roof gutters which cause water to overflow near building walls. (Fig. 14)
- Hot water systems relief valve pipes should be discharged into storm water lines. (Fig. 15)
- Air conditioners operating during hot, humid weather that discharge water near the building footings. (Fig.16)
- Leaking or overflowing water tanks near building footings. (Fig. 17)
- Land or paving that slopes towards the building and cause rain water to flow near the building. (Fig. 18)
- Water from the failure to repair plumbing leaks or leaky taps, hoses or by regularly washing cars in areas near building walls. (Fig. 19)
- Water flowing near buildings (even from neighbouring properties) must be diverted away from the footings or collected. (Fig. 20)

Fig. 13 Root Damage

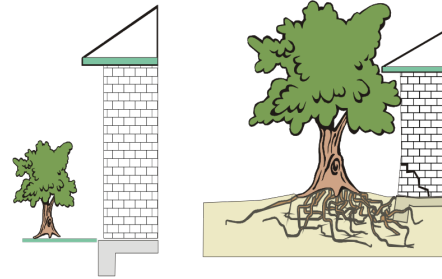


Fig. 14 Overflowing roof Fig. 15 Common leak source

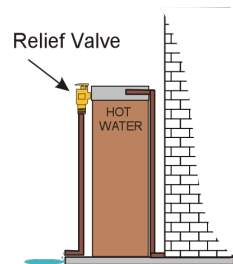
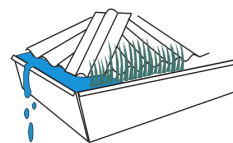


Fig. 16 Air con, up to 35 L/day loss

Fig.17 Leaky pipes

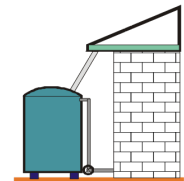
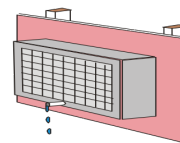


Fig. 18 Reverse Sloping paths

Fig 19 Leaking tap

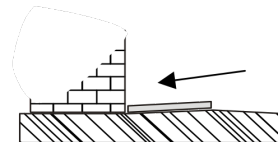
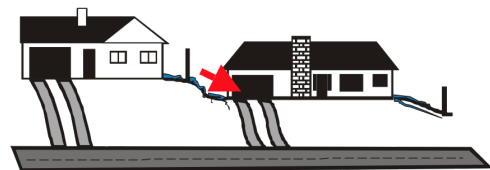


Fig. 20 Adjoining property water flows



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