# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1 – To be submitted with Development Application

Develop	ment Application	n for				
			Name of A	pplicant		
Address	s of site	9 Wandeen Ro	oad, Clareville		_	
		ers the minimum requencing engineering geolog				ation made by a geotechnical report
,	Ben White (Insert Name)	on behalf of _	White Geotech (Trading or	nical Group Pt Company Name)	y Ltd_	
organisatio	ngineer as defined	sue this document ar	al Risk Management	Policy for Pittwate	er - 2009 and I am au	ngineering geologist or uthorised by the above professional indemnity
: Please ma	ark appropriate b	юх				
			•			ustralia Geomechanics Management Policy for
	accordance with t		nechanics Society's	Landslide Risk Ma		nas been prepared in es (AGS 2007) and the
	have examined the with Section 6.0 cassessment for the	e site and the propos of the Geotechnical R	osed development in Risk Management P opment are in com	detail and have carelicy for Pittwater pliance with the G	- 2009. I confirm tha Geotechnical Risk M	essment in accordance at the results of the risk lanagement Policy for
	Application only	involves Minor Dev	evelopment/Alteratio	n that does not	require a Geotech	n that the Development nnical Report or Risk licy for Pittwater - 2009
	Hazard and does the Geotechnical		echnical Report or R Policy for Pittwater -	tisk Assessment a 2009 requirement	nd hence my Reports.	cted by a Geotechnical t is in accordance with Report
Geotechn	nical Report Deta	ils:				
F		echnical Report 9 W	/andeen Road, C	lareville		
A	Author: BEN WH	ITE				
A	Author's Company	//Organisation: WHIT	TE GEOTECHNICA	L GROUP PTY L	TD	
Docum <u>en</u>	ntation which rela	ate to or are relied u	upon in report pre	paration:		
1	Australian Ge	omechanics So	ociety Landslid	e Risk Manag	ement March	2007.
7	White Geoted	chnical Group c	company archi	ves.		
am awa Developm	re that the above	Geotechnical Report this site and will be	ort, prepared for the relied on by Pittw	e abovementione ater Council as th	d site is to be subre basis for ensuring	mitted in support of a that the Geotechnical

I am aware that the above Geotechnical Report, prepared for the abovementioned site is to be submitted in support of a Development Application for this site and will be relied on by Pittwater Council as the basis for ensuring that the Geotechnical Risk Management aspects of the proposed development have been adequately addressed to achieve an "Acceptable Risk Management" level for the life of the structure, taken as at least 100 years unless otherwise stated and justified in the Report and that reasonable and practical measures have been identified to remove foreseeable risk.

Signature	Kelub
Name	Ben White
Chartered Professional Sta	atus MScGEOLAusIMM CP GEOL
Membership No.	222757
Company	White Geotechnical Group Pty Ltd

# GEOTECHNICAL RISK MANAGEMENT POLICY FOR PITTWATER FORM NO. 1(a) - Checklist of Requirements for Geotechnical Risk Management Report for Development Application

Develop	Development Application for Name of Applicant					
Addres	s of site	9 Wandeen Road, Cla	reville			
Report. T		company the Geotechnical Re	o be addressed in a Geotechnical Risk Management Geotechnical eport and its certification (Form No. 1).			
Report	Title: Geotechnical R	eport <b>9 Wandeen Road, C</b>	Clareville			
	Date: 16/4/21	,				
	BEN WHITE					
		sation: WHITE GEOTECHNI	CAL GROUP PTY LTD			
Please m	nark appropriate box	(				
$\boxtimes$		napping conducted 15/4/21				
	Comprehensive site i	(date)				
	Subsurface investigat	ented on contoured site plan wi ion required Justification	th geomorphic mapping to a minimum scale of 1:200 (as appropriate)			
_		Date conducted 15/4/21				
			nferred subsurface type-section			
	Geotechnical hazards					
	⊠ Above t					
	⊠ On the					
	☐ Below t ☐ Beside					
		described and reported				
			Geotechnical Risk Management Policy for Pittwater - 2009			
	_		Geolechilical Risk Management Folicy for Filtwater - 2009			
		uence analysis ncy analysis				
$\boxtimes$	Risk calculation	icy arialysis				
		property conducted in accordan	nce with the Geotechnical Risk Management Policy for Pittwater - 2009			
			ance with the Geotechnical Risk Management Policy for Pittwater - 2009			
			Risk Management" criteria as defined in the Geotechnical Risk			
	Management Policy f		Trisk Management officina as defined in the Geoleoninoa Mak			
$\boxtimes$	,		eve the "Acceptable Risk Management" criteria provided that the			
	specified conditions a	re achieved.	•			
$\boxtimes$	Design Life Adopted:					
		ars				
	☐ Other _					
	Contachnical Canditi	specify	and an electrical in the Contrological Diels Management Policy for			
$\boxtimes$	Pittwater - 2009 have		ises as described in the Geotechnical Risk Management Policy for			
$\boxtimes$		•	nd practical have been identified and included in the report.			
		in Bushfire Asset Protection Zo	·			
that the g	eotechnical risk mana nent" level for the life	agement aspects of the propo of the structure, taken as at	ical Report, to which this checklist applies, as the basis for ensuring sal have been adequately addressed to achieve an "Acceptable Ris least 100 years unless otherwise stated, and justified in the Reportation to remove foreseeable risk.			
	;	Signature	Ellet			
		Name	Ben White			
	_	Chartered Professional Statu				
	_					
	<u>_</u>	Membership No.	222757			

Company White Geotechnical Group Pty Ltd



J3342 16<sup>th</sup> April, 2021 Page 1.

#### **GEOTECHNICAL INVESTIGATION:**

New House at 9 Wandeen Road, Clareville

#### 1. Proposed Development

- **1.1** Demolish the existing house and construct a new part three-storey house by excavating to a maximum depth of ~1.8m into the slope.
- 1.2 Details of the proposed development are shown on 20 drawings prepared by Action Plans, drawings numbered DA01 to DA20, Revision E, dated 13/4/21.

#### 2. Site Description

- **2.1** The site was inspected on the 15<sup>th</sup> April, 2021.
- 2.2 This residential property is level with the road and has a W aspect. It is located on the gently graded lower middle reaches of a hillslope. The natural slope falls across the property at an average angle of  $^{\sim}7^{\circ}$ . The land surface above the property continues at increasing angles. The slope below the property continues at gentle angles before increasing closer to the waterfront.
- 2.3 At the road frontage, a concrete driveway runs to a garage under the downhill side of the house (Photo 1). Between the road frontage and the house is a gently sloping lawn-covered fill (Photo 2). The fill is supported by a sleeper retaining wall reaching ~1.5m high (Photo 3). The wall was observed to be tilting downslope to a maximum angle of ~5° from the vertical. The plans show the wall is to remain as part of the proposed works. See Section 16 for recommendations regarding this wall. Large sandstone floaters appear to be sitting in stable positions within the lawn area between the road frontage and the house (Photo 4). The single-storey timber framed and clad house will be demolished as part of the proposed works (Photo 5). Overgrown lawns and gardens surround the house in its current state. Another large sandstone



J3342 16<sup>th</sup> April, 2021 Page 2.

floater was observed to be sitting in a stable position between the S side of the house

and the S common boundary (Photo 6).

3. Geology

The Sydney 1:100 000 Geological sheet indicates the site is underlain by the Newport

Formation of the Narrabeen Group. It is described as interbedded laminite, shale and quartz

to lithic quartz sandstone.

4. Subsurface Investigation

Six Dynamic Cone Penetrometer (DCP) tests were put down to determine the relative density

of the overlying soil and the depth to weathered rock. The locations of the tests are shown

on the site plan attached. It should be noted that a level of caution should be applied when

interpreting DCP test results. The test will not pass through hard buried objects so in some

instances it can be difficult to determine whether refusal has occurred on an obstruction in

the profile or on the natural rock surface. This is not expected to be an issue for the testing

on this site. However, excavation and foundation budgets should always allow for the

possibility that the interpreted ground conditions in this report vary from those encountered

during excavations. See the appended "Important information about your report" for a more

comprehensive explanation. The results are as follows:

**GROUND TEST RESULTS ARE ON THE NEXT PAGE** 



J3342 16<sup>th</sup> April, 2021 Page 3.

	DCP TEST RESULTS – Dynamic Cone Penetrometer						
Equipment: 9kg hammer, 510mm drop, conical tip. Standard: AS1289.6.3.2 - 19						9.6.3.2 - 1997	
Depth(m)	DCP 1	DCP 2	DCP 3	DCP 4	DCP 5	DCP 6	
Blows/0.3m	(~RL28.9)	(~RL28.1)	(~RL28.9)	(~RL28.4)	(~RL26.4)	(~RL25.9)	
0.0 to 0.3	8	5	Floating Boulder	11	5	25	
0.3 to 0.6	#	9	Exposed at Surface	10	7	30	
0.6 to 0.9		16		11	7	30	
0.9 to 1.2		23		40	10	#	
1.2 to 1.5		#		#	30		
1.5 to 1.8					#		
	Refusal on Rock @ 0.2m	Refusal on Rock @ 1.1m		End of Test @ 1.2m	End of Test @ 1.5m	End of Test @ 0.8m	

<sup>#</sup>refusal/end of test. F = DCP fell after being struck showing little resistance through all or part of the interval.

#### **DCP Notes:**

DCP1 – Refusal on rock @ 0.2m, DCP bouncing off floater, white impact dust on dry tip.

DCP2 – Refusal on rock @ 1.1m, DCP thudding, brown and white shale fragments on dry tip, grey clay in collar above tip.

DCP3 – Rock exposed at surface.

DCP4 – Test taken between two exposed sandstone floaters. End of test @ 1.2m, DCP still very slowly going down, grey shale on dry tip.

DCP5 – End of test @ 1.5m, DCP still very slowly going down, brown shale on dry tip.

DCP6 – End of test @ 1.8m, DCP still very slowly going down, brown shale on dry tip.

#### 5. Geological Observations/Interpretation

The slope materials are colluvial at the near surface and residual at depth. In the test locations, the ground materials consist of a thin silty soil over firm to hard clays. The clays merge into the underlying weathered rock at an average depth of ~0.9m below the current surface across the property. The weathered zone is interpreted to be Extremely Low to Very Low Strength Shale. The sandstone boulders over the surface are interpreted to have historically moved down the slope from the Hawkesbury Sandstone that outcrops further



J3342 16<sup>th</sup> April, 2021

Page 4.

upslope. See Type Section attached for a diagrammatical representation of the expected

ground materials.

6. Groundwater

Normal ground water seepage is expected to move over the buried surface of the rock and

through the cracks. Due to the slope and elevation of the block, the water table is expected

to be many metres below the base of the proposed excavations.

7. Surface Water

No evidence of surface flows were observed on the property during the inspection. It is

expected that normal sheet wash will move onto the site from above the property during

heavy down pours.

8. Geotechnical Hazards and Risk Analysis

No geotechnical hazards were observed below or beside the property. The gently graded

slope that rises across the property and continues above at increasing angles is a potential

hazard (Hazard One). The treated timber retaining wall at the road frontage of the property

is a potential hazard (Hazard Two). The proposed excavations are a potential hazard until

retaining walls are in place (Hazard Three).

RISK ANALYSIS SUMMARY ON THE NEXT PAGE



J3342 16<sup>th</sup> April, 2021 Page 5.

## **Geotechnical Hazards and Risk Analysis - Risk Analysis Summary**

HAZARDS	Hazard One	Hazard Two	Hazard Three	
ТҮРЕ	The gentle slope that rises across the site and continues above at increasing angles failing and impacting on the proposed works.	Further movement of the sleeper tilting retaining wall at the road frontage of the property that causes failure (Photo 3).	The excavations (up to a depth of ~1.8m) collapsing onto the work site before retaining walls are in place.	
LIKELIHOOD	'Unlikely' (10 <sup>-4</sup> )	'Possible' (10 <sup>-3</sup> )	'Possible' (10 <sup>-3</sup> )	
CONSEQUENCES TO PROPERTY	'Medium' (12%)	'Medium' (15%)	'Medium' (15%)	
RISK TO PROPERTY	'Low' (2 x 10 <sup>-5</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )	'Moderate' (2 x 10 <sup>-4</sup> )	
RISK TO LIFE	5.5 x 10 <sup>-7</sup> /annum	8.3 x 10 <sup>-7</sup> /annum	9.2 x 10 <sup>-6</sup> /annum	
COMMENTS	This level of risk is 'ACCEPTABLE'.	This level of risk to life and property is 'TOLERABLE'. To move the risk to 'ACCEPTABLE' levels, the recommendations in <b>Section 16</b> are to be followed.	This level of risk to life and property is 'UNACCEPTABLE'. To move the risk to 'ACCEPTABLE' levels, the recommendations in <b>Section 13</b> are to be followed.	

(See Aust. Geomech. Jnl. Mar 2007 Vol. 42 No 1, for full explanation of terms)

## 9. Suitability of the Proposed Development for the Site

The proposed development is suitable for the site. No geotechnical hazards will be created by the completion of the proposed development provided it is carried out in accordance with the requirements of this report and good engineering and building practice.

#### 10. Stormwater

There is fall to Wandeen Road. Roof water from the proposed development is to be piped to the street drainage system through any tanks that may be required by the regulating authorities.



J3342 16<sup>th</sup> April, 2021

Page 6.

11. Excavations

An excavation to a maximum depth of  $^{\sim}1.8m$  is required to construct the ground floor of the house. Another excavation to a maximum depth of  $^{\sim}1.6m$  is required to construct the garage floor of the house. The excavations are expected to be through a thin silty soil over firm to hard clays with Extremely Low to Very Low Strength Shale expected to be encountered at an

average depth of ~0.9m below the current surface.

Excavations through soil, clay, and Extremely Low to Very Low Strength Shale can be carried

out with an excavator and bucket.

12. Vibrations

No excessive vibrations will be generated by excavation through soil, clay, and Extremely Low

to Very Low Strength Shale.

13. Excavation Support Requirements

No structures or boundaries will be within the zone of influence of either excavation. Any

large sandstone floaters within the footprint and zone of influence of either excavation are to

be cut/broken down without the use of pneumatic hammers and removed prior to the

commencement of the excavations (Photos 4 & 6).

The soil portions of the excavations are to be battered at 1.0 Vertical to 1.7 Horizontal (30°)

and cut batters through clay and Extremely Low to Very Low Strength Shale or better will

stand unsupported at near-vertical angles for short periods of time until retaining walls are

installed, provided they are kept from becoming saturated.

Upslope runoff is to be diverted from the cut faces by sandbag mounds or other diversion

works. Unsupported cut batters are to be covered to prevent access of water in wet weather

and loss of moisture in dry weather. The covers are to be tied down with metal pegs or other

suitable fixtures so they can't blow off in a storm. The materials and labour to construct the

retaining walls are to be organised so on completion of the excavations they can be



J3342 16<sup>th</sup> April, 2021 Page 7.

constructed as soon as possible. The excavations are to be carried out during a dry period. No excavations are to commence if heavy or prolonged rainfall is forecast.

During the excavation process, the geotechnical consultant is to inspect the cuts when they reach depths of not more than 1.5m, while the machine/excavation equipment is on site, to ensure the ground materials are as expected and no temporary support is required.

All excavation spoil is to be removed from site following the current Environmental Protection Agency (EPA) waste classification guidelines.

## 14. Retaining Walls

For cantilever or singly-propped retaining walls, it is suggested the design be based on a triangular pressure distribution of lateral pressures using the parameters shown in Table 1.

Table 1 – Likely Earth Pressures for Retaining Walls

	Earth Pressure Coefficients			
Unit	Unit weight (kN/m³)	'Active' Ka	'At Rest' K₀	
Soil and Residual Clays	20	0.40	0.55	
Extremely Low Strength Rock	22	0.25	0.35	
Rock Up to Low Strength Rock	24	0.25	0.35	

For rock classes refer to Pells et al "Design Loadings for Foundations on Shale and Sandstone in the Sydney Region". Australian Geomechanics Journal 1978.

It is to be noted that the earth pressures in Table 1 assume a level surface above the wall, do not account for any surcharge loads, and assume retaining walls are fully drained. Rock strength and relevant earth pressure coefficients are to be confirmed on site by the geotechnical consultant.



J3342 16<sup>th</sup> April, 2021

Page 8.

All retaining walls are to have sufficient back-wall drainage and be backfilled immediately behind the wall with free-draining material (such as gravel). This material is to be wrapped in a non-woven Geotextile fabric (i.e., Bidim A34 or similar), to prevent the drainage from

becoming clogged with silt and clay. If no back-wall drainage is installed in retaining walls, the

likely hydrostatic pressures are to be accounted for in the structural design.

15. Foundations

Spread footings and piers supported on the underlying Extremely Low to Very Low Strength

Shale are suitable footings for the proposed house. This ground material is expected to be

exposed across the majority of the bases of the proposed excavations. Where the slope falls

away on the downhill side and where the footprint of the house is not over the proposed

excavations, piers to Extremely Low to Very Low Strength Shale will be required to maintain

a uniform bearing material across the structure. This ground material is expected at an

average depth of ~0.9m below the current surface. A maximum allowable pressure of 600kPa

can be assumed for Extremely Low to Very Low Strength Rock. It should be noted that this

material is a soft rock and a rock auger will cut through it so the builders should not be looking

for refusal to end the footings.

As the bearing capacity of clay and shale reduces when it is wet, we recommend the footings

be dug, inspected, and poured in quick succession (ideally the same day if possible). If the

footings get wet, they will have to be drained and the soft layer of wet clay or shale on the

footing surface will have to be removed before concrete is poured.

If a rapid turnaround from footing excavation to the concrete pour is not possible, a sealing

layer of concrete may be added to the footing surface after it has been cleaned.

**NOTE**: If the contractor is unsure of the footing material required, it is more cost-effective to

get the geotechnical consultant on site at the start of the footing excavation to advise on

footing depth and material. This mostly prevents unnecessary over-excavation in clay-like

shaly-rock but can be valuable in all types of geology.



J3342 16<sup>th</sup> April, 2021

Page 9.

16. Maintenance

The treated timber retaining wall along the road frontage of the property was observed to be

tilting to a maximum of ~5° (Photo 3). To be prudent, we recommend the retaining wall be

inspected by the owners on an annual basis or after heavy prolonged rainfall, whichever

occurs first, keeping a photographic record of the inspections. We can carry out these

inspections upon request. Should any new movement be observed, the retaining wall is to be

remediated or rebuilt to current engineering standards.

17. Geotechnical Review

The structural plans are to be checked and certified by the geotechnical engineer as being in

accordance with the geotechnical recommendations. On completion, a Form 2 Part B will be

issued. This form is required for the Construction Certificate to proceed.

18. Inspections

The client and builder are to familiarise themselves with the following required inspections

as well as council geotechnical policy. We cannot provide certification for the regulating

authorities or the owner if the following inspections have not been carried out during the

construction process.

• The geotechnical consultant is to inspect the cuts as they are lowered to depths of not

more than 1.5m, while the machine/excavation equipment is on site, to ensure the

ground materials are as expected and no temporary support is required.

All footings are to be inspected and approved by the geotechnical consultant while

the excavation equipment is still onsite and before steel reinforcing is placed or

concrete is poured.



J3342 16<sup>th</sup> April, 2021 Page 10.

White Geotechnical Group Pty Ltd.

Ben White M.Sc. Geol., AusIMM., CP GEOL.

Bulut

No. 222757

**Engineering Geologist** 



J3342 16<sup>th</sup> April, 2021 Page 11.



Photo 1



Photo 2



J3342 16<sup>th</sup> April, 2021 Page 12.



Photo 3



Photo 4



J3342 16<sup>th</sup> April, 2021 Page 13.



Photo 5

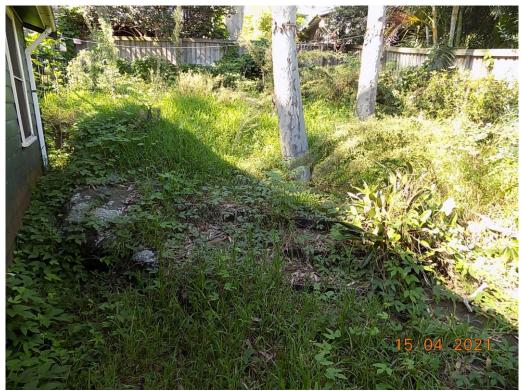


Photo 6



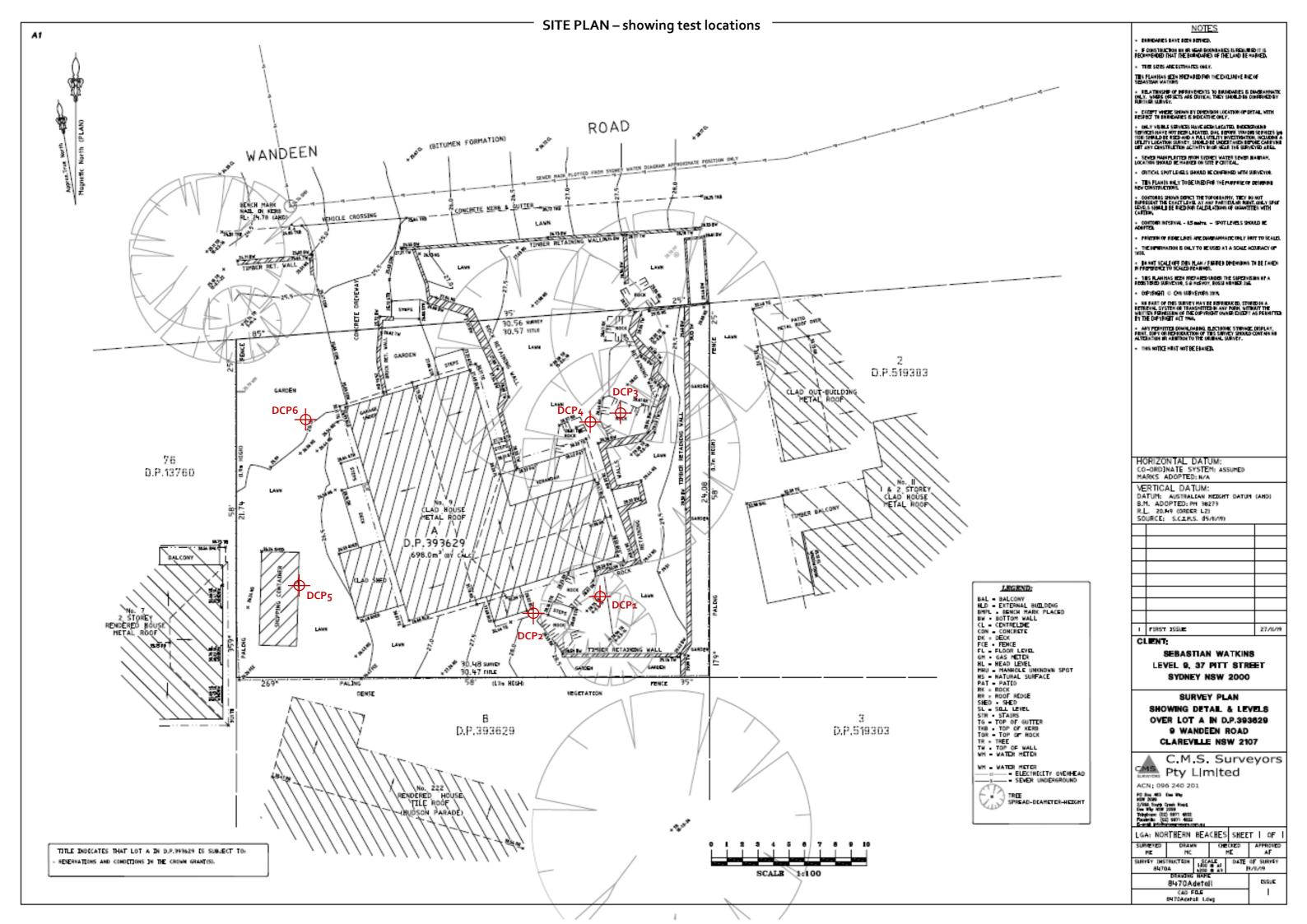
J3342 16<sup>th</sup> April, 2021 Page 14.

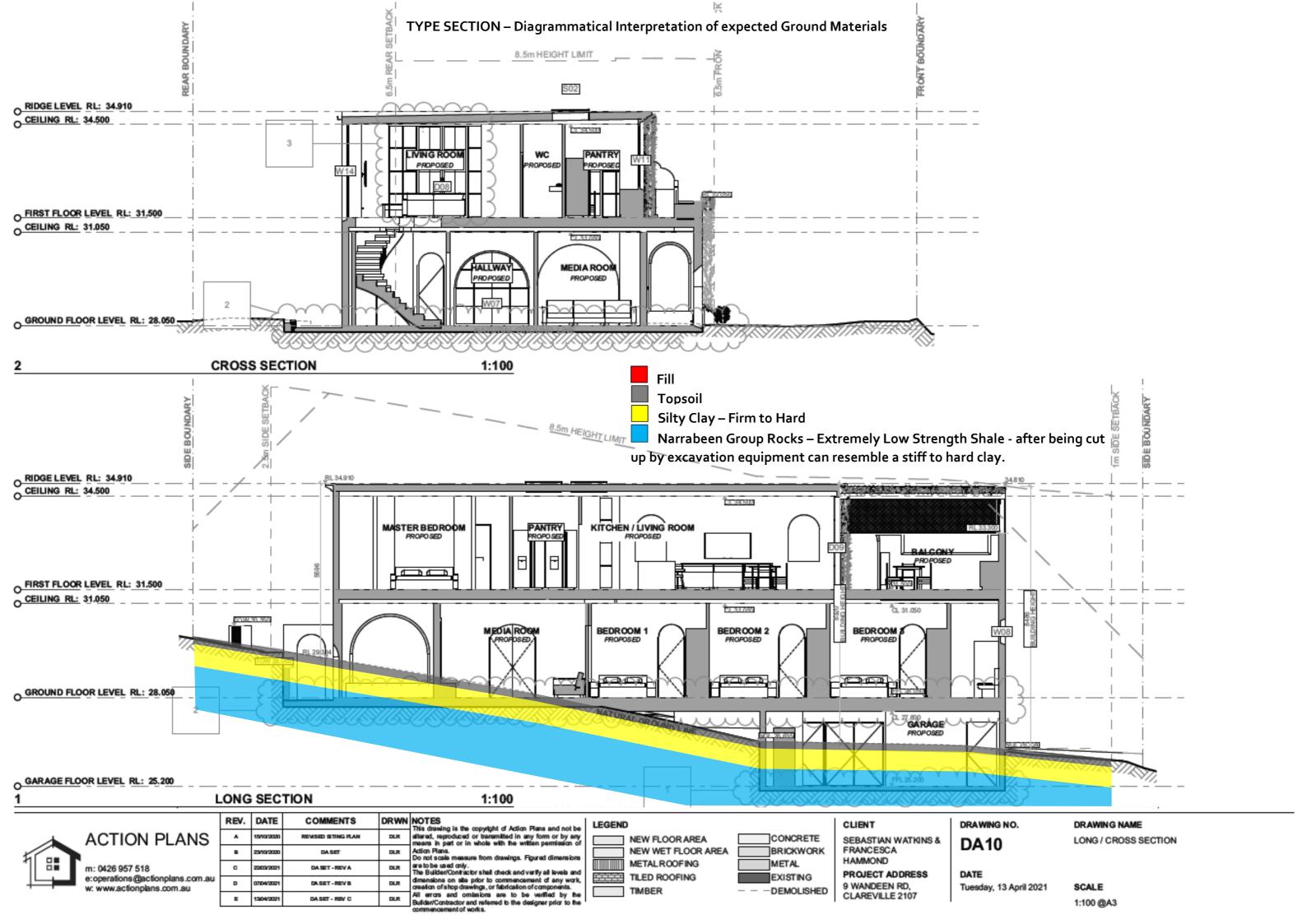
#### Important Information about Your Report

It should be noted that Geotechnical Reports are documents that build a picture of the subsurface conditions from the observation of surface features and testing carried out at specific points on the site. The spacing and location of the test points can be limited by the location of existing structures on the site or by budget and time constraints of the client. Additionally, the test themselves, although chosen for their suitability for the particular project, have their own limiting factors. The testing gives accurate information at the location of the test, within the confines of the test's capability. A geological interpretation or model is developed by joining these test points using all available data and drawing on previous experience of the geotechnical consultant. Even the most experienced practitioners cannot determine every possible feature or change that may lie below the earth. All of the subsurface features can only be known when they are revealed by excavation. As such, a Geotechnical report can be considered an interpretive document. It is based on factual data but also on opinion and judgement that comes with a level of uncertainty. This information is provided to help explain the nature and limitations of your report.

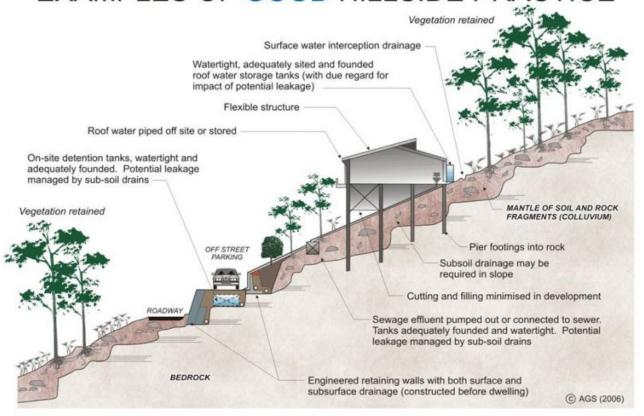
With this in mind, the following points are to be noted:

- If upon the commencement of the works the subsurface ground or ground water conditions prove different from those described in this report, it is advisable to contact White Geotechnical Group immediately, as problems relating to the ground works phase of construction are far easier and less costly to overcome if they are addressed early.
- If this report is used by other professionals during the design or construction process, any questions should be directed to White Geotechnical Group as only we understand the full methodology behind the report's conclusions.
- The report addresses issues relating to your specific design and site. If the proposed project design changes, aspects of the report may no longer apply. Contact White Geotechnical if this occurs.
- This report should not be applied to any other project other than that outlined in section 1.0.
- This report is to be read in full and should not have sections removed or included in other documents as this can result in misinterpretation of the data by others.
- It is common for the design and construction process to be adapted as it progresses (sometimes
  to suit the previous experience of the contractors involved). If alternative design and construction
  processes are required to those described in this report, contact White Geotechnical Group. We
  are familiar with a variety of techniques to reduce risk and can advise if your proposed methods
  are suitable for the site conditions.





# EXAMPLES OF GOOD HILLSIDE PRACTICE



## EXAMPLES OF POOR HILLSIDE PRACTICE

