

Preliminary Geotechnical Assessment

Project: Alterations & Additions 12A Rabaul Road, North Curl Curl NSW

Prepared for:

Sue Brauer

Ref: AG 24452 23 October 2024





WHAT TO DO WITH THIS REPORT

While your geotechnical assessment report may be a statutory requirement from council in support of your development application, it also contains information important to the structural design and construction methodology of your project. Therefore, it is critical that all relevant parties are provided with a copy of this report.

We suggest you give a copy of your geotechnical assessment report to: ☐ Your Structural/Stormwater/Civil Engineer ☐ Your Architect/Building Designer ☐ Your Certifier ☐ Your Project Manager ☐ Your Excavation Contractor ☐ Your Builder We would also suggest that if any of your project team have questions regarding the contents of this report, that we be contacted for clarification. **NEXT CRITICAL STAGES** Keep in mind that you will need AscentGeo again at different stages of your project. This may include: Review or endorsement of structural plans/architectural plans for a Construction Certificate Foundation/Footing inspection during construction Excavation hold point inspection, usually at hold points not exceeding 1.5m drops Final inspection and certification for an Occupation Certificate upon completion of works

GENERAL ADVICE

If after reading this report you have any questions, are unsure what to do next or when you need to get in touch, please reach out to us.

Given AscentGeo can't be on site the whole time, we recommend that you or/and your builder take a lot of progress photos, especially during excavation. Many of the potential problems that may pop up can be resolved if we have clear photos of the work that's been done.

A lot can change on site during a construction project: some of these changes are normal and innocuous, while others can be symptoms of larger or more serious issues. For this reason, it's important to contact us to discuss any changes you notice on site that you aren't sure about. This could include but not be limited to changes to ground or surface water, movement of structures, and settlement of paths or landscaping elements.

We're here to help.

The AscentGeo Team

admin@ascentgeo.com.au

9913 3179

ascentgeo.com.au



Preliminary Geotechnical Assessment

For Alterations & Additions at

12A Rabaul Road, North Curl Curl NSW

Document Status		Approved for Issue		
Version	Author		Reviewer	Date
1	Cameron Young BEnvSci Geol MAIG		Ben Morgan BScGeol MAIG RPGeo	23.10.2024
Document Distribution				
Version	Copies	Format	То	Date
1	1	PDF	Rapid Plans	23.10.2024

Limitations

This report has been prepared for Sue Brauer, c/- Rapid Plans, in accordance with AscentGeo's fee proposal dated 17 October 2024.

The report is provided for the exclusive use of the property owners and their nominated agents for the specific development and purpose as described in the report. This report must not be used for purposes other than those outlined in the report or applied to any other projects.

The information contained within this report is considered accurate at the time of issue with regard to the current conditions on site as identified by AscentGeo and the documentation provided by others.

The report should be read in its entirety and should not be separated from its attachments or supporting notes. It should not have sections removed or included in other documents without the express approval of AscentGeo.



Overview

Background

This report presents the findings of a preliminary geotechnical investigation carried out at 12A Rabaul Road, North Curl Curl (the 'Site'), undertaken by AscentGeo. This assessment has been prepared to accompany an application for DA with Northern Beaches Council.

Proposed Development

Details of the development are outlined in a series of architectural drawings prepared by Rapid Plans, project number RP0622BRA, drawing numbers DA 1003, 1011, 2002 – 2004, 4000, 4001, 5000, 5001 & 6000, dated 2/2/24.

The works comprise the following:

- Construction of first floor addition.
- Minor internal modifications to the existing dwelling to facilitate access to the proposed first floor.

Relevant Instruments

This geotechnical assessment has been prepared in accordance with the following relevant guidelines and standards:

- Northern Beaches Council Warringah Local Environment Plan (WLEP) 2011 and Warringah Development Control Plan (WDCP) 2011
- Australian Geomechanics Society's 'Landslide Risk Management Guidelines' (AGS 2007)
- Australian Standard 1726–2017 Geotechnical Site Investigations
- Australian Standard 2870–2011 Residential Slabs and Footings.

WDCP & WLEP Landslip Risk Class

The site is mapped as **Area A & B** subject to specific landslip risk/geotechnical hazard mapping with reference to the Warringah (WLEP) Landslip Risk Map, Northern Beaches Council (**Image 1**).



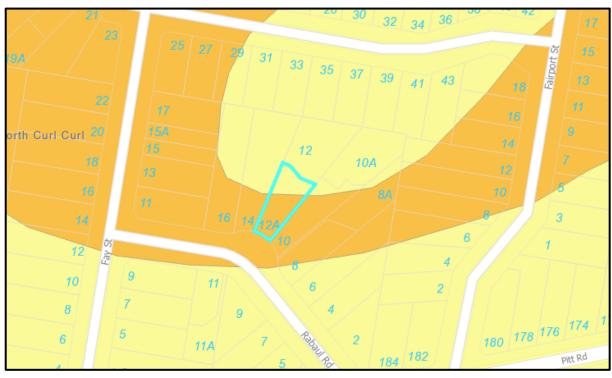


Figure 1. Warringah Landslip Risk Map: 12A Rabaul Road, North Curl. Curl NSW (© NBC Maps)



Site Description

Summary

A summary of site conditions identified at the time of our inspection is provided in Table 1.

Table 1. Summary of site conditions

Parameter Description		
Site Visit	Cameron Young, Engineering Geologist – 22 October 2024.	
Address	12A Rabaul Road, North Curl Curl – Lot 391 in DP 838916	
Site Area m² (approx.)	514.9m² (by calc.)	
Existing Development	Single storey rendered residence with garage under.	
Slope Aspect	South-west.	
Average Gradient	~20 degrees.	



Parameter	Description
Vegetation	Small shrubs and trees.
Retaining Structures	N/A
Neighbouring Environment	Residentially developed to the north, east and west. Rabaul Road to the south.
Geology	The Sydney 1:100,000 Geological Sheet 9130 (NSW Dept. Mineral Resources, 1983) indicates that the site is underlain by the Middle Triassic Hawkesbury Sandstone (Rh). The Hawkesbury rocks outcrops on the subject slope and in the surrounding properties.
Potential Geotechnical Hazards	No evidence of significant settlement, slope instability, undercutting, jointing or other geotechnical hazards were identified at the time of our assessment.
Groundwater	Due to the position of the site relative to the slope and the underlying geology, no significant standing water table is expected to influence the site.



Figure 2. Site location: 12 Rabaul Road, North Curl Curl NSW (© SIX Maps NSW Gov)

Preliminary Risk Assessment and Recommendations

With reference to the Australian Geomechanics Society's definitions, the existing conditions and proposed development are considered to constitute an 'ACCEPTABLE' risk to life and a 'LOW' risk to property provided that the recommendations outlined in Table 2 are adhered to.



Table 2. Geotechnical Recommendations

Recommendation	Description	
Soil & Rock Excavation	All proposed works will take place above the existing structure. No new footings are anticipated, and no significant soil or rock excavation is required.	
Footings	We recommend the existing footings be assessed by the structural engineer for their adequacy to support any additional loads imposed by the proposed works.	
	Whilst no new footings are anticipated, the allowable bearing pressure for footings taken to competent weathered bedrock is 600kPa . Higher allowable bearing capacities may be achievable subject to ground testing and/or inspection and certification of excavated footings.	
Stormwater Disposal The effective management of ground and surface water on site may most important factor in the long-term performance of built structure the stability of the block more generally.		
	It is essential that gutters, downpipes, drains, pipes, and connections are appropriately sized, functioning effectively, and discharging appropriately via non-erosive discharge.	
	All stormwater collected from hard surfaces is to be collected and piped directly to the council stormwater network through any storage tanks or onsite detention that may be required by the regulating authorities, and in accordance with all relevant Australian Standards and the detailed stormwater management plan by others.	
	Saturation of soils is one of the key triggers for many landslide events and a significant factor in destabilisation of structures over time. As such the review and design of stormwater systems must consider climate change and the increased potential for periods of concentrated heavy rainfall.	
Inspections	If required any new footings will require geotechnical inspection prior to introduction of steel of concrete.	
Conditions Relating to Design and Construction Monitoring	To comply with Northern Beaches Council conditions and/or Private Certifier requirements it may be necessary at the following stages for AscentGeo to: Review the geotechnical content of all structural designs prior to the issue of Construction Certificate Complete the abovementioned foundation material inspections during	
	construction to ensure compliance to design with respect to stability and geotechnical design parameters	
	By Occupation Certificate stage (project completion), AscentGeo must have inspected and certified excavations/foundation materials. A final	



Recommendation	Description
	site inspection may be required before the issue of the Occupation Certificate.
Further Geotechnical or Hydrological Investigation	No further geotechnical or hydrogeological investigations are required, provided that the above recommendations outlined in Table 2 are adhered to.

Should you have any queries regarding this report, please do not hesitate to contact the author of this report, undersigned.

For and on behalf of AscentGeo,

Cameron Young BEnvSci Geol MAIG Engineering Geologist

Ben Morgan BScGeol MAIG RPGeo Managing Director | Engineering Geologist



References

Australian Geomechanics Society Landslide Taskforce, Landslide Practice Note Working Group 2007 (Mar). 'Practice Note Guidelines for Landslide Risk Management 2007'. *Australian Geomechanics Journal*, vol. 42, no. 1, pp. 63–114.

Herbert C, 1983, Sydney 1:100 000 Geological Sheet 9130, 1st edition. Geological Survey of New South Wales, Sydney.

NSW Department of Finance, Services and Innovation, Spatial Information Viewer, maps.six.nsw.gov.au.

Northern Beaches Council, Online Mapping, Warringah Landslip Risk Map (WLEP 2011).

Safe Work Australia, 2018 (Oct), Code of Practice: Excavation Work. Safe Work Australia.

Standards Australia 1997, *Methods of Testing Soils for Engineering Purposes*, AS1289.6.3.2:1997, Standards Australia, NSW.

Standards Australia 2001, *Evaluation of human exposure to whole-body vibration. Part 1: General requirements*, AS2670.1:2001, Standards Australia, NSW.

Standards Australia 2006, Explosives – storage and use, AS2187.2:2006, Standards Australia, NSW.

Standards Australia 2007, *Guidelines for Earthworks for Commercial and Residential Developments*. AS3798:2007, Standards Australia, NSW.

Standards Australia 2011, Residential Slabs and Footings, AS2870:2011, Standards Australia, NSW.

Standards Australia 2017, Geotechnical Site Investigations, AS1726:2017, Standards Australia, NSW.



Appendix A

Information Sheets

General Notes About This Report



INTRODUCTION

These notes have been prepared by Ascent Geotechnical Consulting Pty Ltd (Ascent) to help our Clients interpret and understand the limitations of this report. Not all sections below are necessarily relevant to all reports.

SCOPE OF SERVICES

This report has been prepared in accordance with the scope of services set out in Ascent's proposal under Ascent's Terms and Conditions, or as otherwise agreed with the Client. The scope of work may have been limited by a range of factors including time, budget, access and/or site constraints.

RELIANCE ON INFORMATION PROVIDED

In preparing the report, Ascent has necessarily relied upon information provided by the Client and/or their Agents. Such data may include surveys, analyses, designs, maps and design plans. Ascent has not verified the accuracy or completeness of the data except as stated in this report.

GEOTECHNICAL AND ENVIRONMENTAL REPORTING

Geotechnical and environmental reporting relies on the interpretation of factual information, based on judgment and opinion, and is far less exact than other engineering or design disciplines.

Geotechnical and environmental reports are prepared for a specific purpose, development, and site, as described in the report, and may not contain sufficient information for other purposes, developments, or sites (including adjacent sites), other than that described in the report.

SUBSURFACE CONDITIONS

Subsurface conditions can change with time and can vary between test locations. For example, the actual interface between the materials may be far more gradual or abrupt than indicated.

Therefore, actual conditions in areas not sampled may differ from those predicted, since no subsurface investigation, no matter how comprehensive, can reveal all subsurface details and anomalies.

Construction operations at or adjacent to the site and natural events such as floods, earthquakes or groundwater fluctuations can also affect subsurface conditions, and thus the continuing adequacy of a geotechnical report. Ascent should be kept informed of any such events, and should be retained to identify variances, conduct additional tests if required, and recommend solutions to problems encountered on site.

GROUNDWATER

Groundwater levels indicated on borehole and test pit logs are recorded at specific times. Depending on ground permeability, measured levels may or may not reflect actual levels if measured over a longer time period. Also, groundwater levels and seepage inflows may fluctuate with seasonal and environmental variations and construction activities.

INTERPRETATION OF DATA

Data obtained from nominated discrete locations, subsequent laboratory testing and empirical or external sources are interpreted by trained professionals in order to provide an opinion about overall site conditions, their likely impact with respect to the report purpose and recommended actions in accordance with any relevant industry standards, guidelines or procedures.

SOIL AND ROCK DESCRIPTIONS

Soil and rock descriptions are based on AS 1726 – 1993, using visual and tactile assessment, except at discrete locations where field and / or laboratory tests have been carried out. Refer to the accompanying soil and rock terms sheet for further information.

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This report shall not be reproduced either totally or in part without the permission of Ascent. Where information from this report is to be included in contract documents or engineering specification for the project, the entire report should be included in order to minimise the likelihood of misinterpretation.

FURTHER ADVICE

Ascent would be pleased to further discuss how any of the above issues could affect a specific project. We would also be pleased to provide further advice or assistance including:

Assessment of suitability of designs and construction techniques;
Contract documentation and specification;
Construction advice (foundation assessments,

excavation support).

Abbreviations, Notes & Symbols

SUBSURFACE INVESTIGATION

ИE	THOD

METHOD				
Borehole Logs		Excavation Logs		
AS#	Auger screwing (#-bit)	ВН	Backhoe/excavator bucket	
AD#	Auger drilling (#-bit)	NE	Natural exposure	
В	Blank bit	HE	Hand excavation	
V	V-bit	Χ	Existing excavation	
T	TC-bit			
HA	Hand auger	Hand auger Cored Borehole Logs		
R	Roller/tricone	NMLC	NMLC core drilling	
W	Washbore	NQ/HQ	Wireline core drilling	
AH	Air hammer			
AT	Air track			
LB	Light bore push tube			
MC	Macro core push tube			
DT	Dual core push tube			
	Borehole AS# AD# B V T HA R W AH AT LB MC	Borehole Logs AS# Auger screwing (#-bit) AD# Auger drilling (#-bit) B Blank bit V V-bit T TC-bit HA Hand auger R Roller/tricone W Washbore AH Air hammer AT Air track LB Light bore push tube MC Macro core push tube	Borehole Logs Excavation AS# Auger screwing (#-bit) BH AD# Auger drilling (#-bit) NE B Blank bit HE V V-bit X T TC-bit HA Hand auger Cored Boren R Roller/tricone NMLC W Washbore NQ/HQ AH Air hammer AT Air track LB Light bore push tube MC Macro core push tube	

SUPPORT

Borehole Logs		Excavation Logs	
С	Casing	S	Shoring
M	Mud	В	Benched

SAMPLING

U#

В	Bulk sample
D	Disturbed sample

Thin-walled tube sample (#mmdiameter)

ES

EW Environmental water sample

FIELD TESTING

PP	Pocket penetrometer (kPa)
DCP	Dynamic cone penetromete
PSP	Perth sand penetrometer
SPT	Standard penetration test
PBT	Plate bearing test

Vane shear strength peak/residual (kPa) and vane size (mm)

N* SPT (blows per 300mm) Nc SPT with solid cone Refusal

*denotes sample taken

BOUNDARIES

 Known
 Probable
 Possible

SOIL

MOISTURE CONDITION

D	Dry
M	Moist
W	Wet
Wp	Plastic Limit
WI	Liquid Limit
MC	Moisture Content

CONSI	STENCY	DENSI	TY INDEX
VS	Very Soft	VL	Very Loose
S	Soft	L	Loose
F	Firm	MD	Medium Dense
St	Stiff	D	Dense
VSt	Very Stiff	VD	Very Dense

Hard Friable

USCS SYMBOLS

GW	Well graded gravels and gravel-sand mixtures, little or no fines
GP	Poorly graded gravels and gravel-sand mixtures, little or no

Silty gravels, gravel-sand-silt mixtures GM GC Clayey gravels, gravel-sand-clay mixtures

SD Poorly graded sands and gravelly sands little or no fine	SW	Well graded sands and gravelly sands, little or no fines
or Footily graded sailes and gravelly sailes, little of no line	SP	Poorly graded sands and gravelly sands, little or no fines

Silty sand, sand-silt mixtures SC Clayey sand, sand-clay mixtures

ML Inorganic silts of low plasticity, very fine sands, rock flour, silty

or clayey fine sands

CL Inorganic clays of low to medium plasticity, gravelly clays,

OL

Organic clays of now of mental plasticity, gravely, sandy clays, silty clays
Organic silts and organic silty clays of low plasticity
Inorganic clays of high plasticity
Organic clays of medium to high plasticity
Deat much and other highly organic soils МН СН

ОН Peat muck and other highly organicsoils

ROCK

WEATH	ERING	STRE	NGTH
RS	Residual Soil	EL	Extremely Low
XW	Extremely Weathered	VL	Very Low
HW	Highly Weathered	L	Low
MW	Moderately Weathered	M	Medium
DW*	Distinctly Weathered	Н	High
SW	Slightly Weathered	VH	Very High
FR	Fresh	EH	Extremely High

*covers both HW & MW

ROCK QUALITY DESIGNATION (%)

= sum of intact core pieces > 100mm x 100 total length of section being evaluated

CORE RECOVERY (%)

= core recovered x 100

core IIft

NATURAL FRACTURES

T	ν	b	е	

JŤ. **Joint** BP Bedding plane SM Seam FΖ Fractured zone S7 Shear zone

Infill or Coating

Cn	Clean
St	Stained
Vn	Veneer
Co	Coating
CI	Clay
Ca	Calcite
Fe	Iron oxide
Mi	Micaceous
Qz	Quartz

Shape

pl	Planar
cu	Curved
un	Undulose
st	Stepped
ir	Irregular

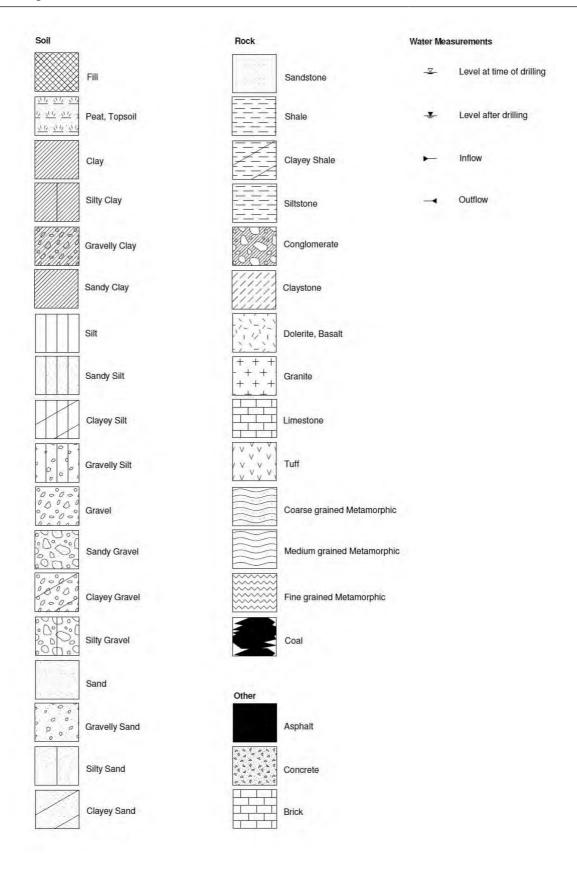
Roughness

pol	Polished
slk	Slickensided
smo	Smooth
rou	Rough

Soil & Rock Terms

SOIL				STRENGTH			
MOISTURE CON				Term	Is50 (MPa)	Term	Is50 (MPa)
Term	Description			Extremely Low	< 0.03	High	1 – 3
Dry		dry. Cohesive and		Very Low	0.03 – 0.1	Very High	3 – 10
hard, friable or powdery. Uncemented granular soils run freely through the hand.			Low Medium	0.1 – 0.3 0.3 – 1	Extremely High	> 10	
Moist Feels cool and darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.			WEATHERING				
Wet As for moist, but with free water forming on hands when handled.			Term Residual Soil	Description Soil developed	on extremely weathe	red rock; the mass	
	s, moisture content		bed in relation to an, > greater than, <		structure and s	ubstance fabric are n	o longer evident
less than, << muc	ch less than].			Extremely Weathered		red to such an extent t either disintegrates	
CONSISTENCY Term	c (kPa)	Term	c (kPa)		remoulded, in v visible	vater. Fabric of origin	al rock is still
Very Soft	u < 12	Very Stiff	ս 100 200	Highly	Rock strenath	usually highly change	d by weathering:
Soft	12 - 25	Hard	> 200	Weathered		ghly discoloured	,
Firm	25 - 50	Friable	-	Moderately	Rock strength	usually moderately ch	anged by
Stiff	50 - 100			Weathered	weathering; roo	k may be moderately	discoloured
DENSITY INDEX	I _D (%)	Term	I _D (%)	Distinctly Weathered	See 'Highly We	athered' or 'Moderate	ely Weathered'
Very Loose Loose	< 15 15 – 35	Dense Very Dense	65 – 8 > 85	Slightly Weathered		discoloured but show gth from fresh rock	vs little or no
Medium Dense	35 – 65			Fresh	Rock shows no	signs of decomposit	ion or staining
PARTICLE SIZE				NATURAL FRAC	CTURES		
Name Subdivision Size (mm)			Type	Description			
Boulders Cobbles		> 200 63 - 200		Joint	A discontinuity	or crack across whic ength. May be open	
Gravel	coarse	20 - 63		Redding plane		layers of mineral gra	
	medium	6 - 20		Bedding plane	or composition	layers of fillileral gra	iiiis oi siiiiidi sizes
0 1	fine	2.36 - 6		Seam	•	osited soil (infill), extr	emely weathered
Sand	coarse medium	0.6 -2.36 0.2 - 06		Coam	insitu rock (XW), or disoriented usua e host rock (crushed)	illy angular
Silt & Clay	fine	0.075 0.2 < 0.075		Shear zone	material interse	nly parallel planar bou	ed (generally <
MINOR COMPO	NENTS				50mm) joints a	nd /or microscopic fra	cture (cleavage)
Term	Proportion by	fine grained			planes		
	Mass coarse grained			Vein	Intrusion of any mass. Usually i	shape dissimilar to t gneous	he adjoining rock
Trace	≤ 5%	≤ 15%					
Some	5 - 2%	15 - 30%		Shape	Description		
				Planar	Consistent orie	ntation	
SOIL ZONING				Curved	Gradual chang	e in orientation	
Layers	Continuous expo			Undulose	Wavy surface		
Lenses		yers of lenticular sh		Stepped	One or more w	ell defined steps	
Pockets	Irregular inclusio	ons of different mate	rial	Irregular	Many sharp ch	anges in orientation	
SOIL CEMENTIN Weakly	IG Easily broken up	b by hand		Infill or	Description		
Moderately Effort is required to break up the soil by hand		Coating Clean	No visible cost	ng or discolouring			
•	·			Stained		ng or discolouring ng but surfaces are d	iscoloured
SOIL STRUCTUR				Veneer		•	
Massive Coherent, with any partings both vertically and horizontally spaced at greater than 100mm			A visible coating of soil or mineral, too thin to measure; may be patchy Visible coating < 1 mm thick. Ticker soil material.				
Weak Peds indistinct and barely observable on pit face. When disturbed approx. 30% consist of peds smaller than 100mm			Coating	Visible coating ≤ 1mm thick. Ticker soil material described as seam			
Weak	7()()mm	intinat in condint on	dsoil When	Roughness	Description		
			a son. Wileli	Polished	Shiny smooth s		
Weak	Peds are quite d		naller than 100mm		Grooved or stri	atad aurfaga wayally	
	Peds are quite d	consists of peds sn	naller than 100mm	Slickensided			•
	Peds are quite d		naller than 100mm	Smooth	Smooth to touc	h. Few or no surface	irregularities
Strong ROCK SEDIMENTARY	Peds are quite d disturbed >60%	consists of peds sn			Smooth to touc Many small sur		irregularities plitude generally <
Strong ROCK SEDIMENTARY Rock Type	Peds are quite d disturbed >60% ROCK TYPE DEFII Definition (more	consists of peds sn NITIONS e than 50% of rock of		Smooth Rough	Smooth to touc Many small sur 1mm). Feels lik	h. Few or no surface face irregularities (am e fine to coarse sand	irregularities politude generally < paper
Strong ROCK SEDIMENTARY I Rock Type Conglomerate	Peds are quite d disturbed >60% ROCK TYPE DEFII Definition (more gravel sized (consists of peds sn NITIONS e than 50% of rock or the same some same some some some some some some some so		Smooth Rough Note: soil and roo	Smooth to touc Many small sur 1mm). Feels lik	h. Few or no surface face irregularities (am e fine to coarse sand generally in accorda	irregularities politude generally < paper
Strong ROCK SEDIMENTARY Rock Type	Peds are quite d disturbed >60% ROCK TYPE DEFII Definition (more gravel sized (sand sized (0	consists of peds sn NITIONS e than 50% of rock of	consists of)	Smooth Rough Note: soil and roo	Smooth to touc Many small sur 1mm). Feels lik	h. Few or no surface face irregularities (am e fine to coarse sand generally in accorda	irregularities politude generally < paper
Strong ROCK SEDIMENTARY I Rock Type Conglomerate Sandstone	Peds are quite d disturbed >60% ROCK TYPE DEFII Definition (more gravel sized (sand sized (<0.1 silt sized (<0.1 clay, rock is n	NITIONS e than 50% of rock or 2mm) fragments .06 to 2mm) grains 06mm) particles, ro	consists of) ck is not laminated	Smooth Rough Note: soil and roo	Smooth to touc Many small sur 1mm). Feels lik	h. Few or no surface face irregularities (am e fine to coarse sand generally in accorda	irregularities politude generally < paper

Graphic Symbols Index



Foundation Maintenance and Footing Performance: A Homeowner's Guide



BTF 18 replaces Information Sheet 10/91

Buildings can and often do move. This movement can be up, down, lateral or rotational. The fundamental cause of movement in buildings can usually be related to one or more problems in the foundation soil. It is important for the homeowner to identify the soil type in order to ascertain the measures that should be put in place in order to ensure that problems in the foundation soil can be prevented, thus protecting against building movement.

This Building Technology File is designed to identify causes of soil-related building movement, and to suggest methods of prevention of resultant cracking in buildings.

Soil Types

The types of soils usually present under the topsoil in land zoned for residential buildings can be split into two approximate groups – granular and clay. Quite often, foundation soil is a mixture of both types. The general problems associated with soils having granular content are usually caused by erosion. Clay soils are subject to saturation and swell/shrink problems.

Classifications for a given area can generally be obtained by application to the local authority, but these are sometimes unreliable and if there is doubt, a geotechnical report should be commissioned. As most buildings suffering movement problems are founded on clay soils, there is an emphasis on classification of soils according to the amount of swell and shrinkage they experience with variations of water content. The table below is Table 2.1 from AS 2870, the Residential Slab and Footing Code.

Causes of Movement

Settlement due to construction

There are two types of settlement that occur as a result of construction:

- Immediate settlement occurs when a building is first placed on its foundation soil, as a result of compaction of the soil under the weight of the structure. The cohesive quality of clay soil mitigates against this, but granular (particularly sandy) soil is susceptible.
- Consolidation settlement is a feature of clay soil and may take place because of the expulsion of moisture from the soil or because of the soil's lack of resistance to local compressive or shear stresses. This will usually take place during the first few months after construction, but has been known to take many years in exceptional cases.

These problems are the province of the builder and should be taken into consideration as part of the preparation of the site for construction. Building Technology File 19 (BTF 19) deals with these problems.

Erosion

All soils are prone to erosion, but sandy soil is particularly susceptible to being washed away. Even clay with a sand component of say 10% or more can suffer from erosion.

Saturation

This is particularly a problem in clay soils. Saturation creates a boglike suspension of the soil that causes it to lose virtually all of its bearing capacity. To a lesser degree, sand is affected by saturation because saturated sand may undergo a reduction in volume – particularly imported sand fill for bedding and blinding layers. However, this usually occurs as immediate settlement and should normally be the province of the builder.

Seasonal swelling and shrinkage of soil

All clays react to the presence of water by slowly absorbing it, making the soil increase in volume (see table below). The degree of increase varies considerably between different clays, as does the degree of decrease during the subsequent drying out caused by fair weather periods. Because of the low absorption and expulsion rate, this phenomenon will not usually be noticeable unless there are prolonged rainy or dry periods, usually of weeks or months, depending on the land and soil characteristics.

The swelling of soil creates an upward force on the footings of the building, and shrinkage creates subsidence that takes away the support needed by the footing to retain equilibrium.

Shear failure

This phenomenon occurs when the foundation soil does not have sufficient strength to support the weight of the footing. There are two major post-construction causes:

- Significant load increase.
- Reduction of lateral support of the soil under the footing due to erosion or excavation.
- In clay soil, shear failure can be caused by saturation of the soil adjacent to or under the footing.

	GENERAL DEFINITIONS OF SITE CLASSES
Class	Foundation
Α	Most sand and rock sites with little or no ground movement from moisture changes
S	Slightly reactive clay sites with only slight ground movement from moisture changes
M	Moderately reactive clay or silt sites, which can experience moderate ground movement from moisture changes
H	Highly reactive clay sites, which can experience high ground movement from moisture changes
E	Extremely reactive sites, which can experience extreme ground movement from moisture changes
A to P	Filled sites
P	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise

Tree root growth

Trees and shrubs that are allowed to grow in the vicinity of footings can cause foundation soil movement in two ways:

- Roots that grow under footings may increase in cross-sectional size, exerting upward pressure on footings.
- Roots in the vicinity of footings will absorb much of the moisture in the foundation soil, causing shrinkage or subsidence.

Unevenness of Movement

The types of ground movement described above usually occur unevenly throughout the building's foundation soil. Settlement due to construction tends to be uneven because of:

- · Differing compaction of foundation soil prior to construction.
- · Differing moisture content of foundation soil prior to construction.

Movement due to non-construction causes is usually more uneven still. Erosion can undermine a footing that traverses the flow or can create the conditions for shear failure by eroding soil adjacent to a footing that runs in the same direction as the flow.

Saturation of clay foundation soil may occur where subfloor walls create a dam that makes water pond. It can also occur wherever there is a source of water near footings in clay soil. This leads to a severe reduction in the strength of the soil which may create local shear

Seasonal swelling and shrinkage of clay soil affects the perimeter of the building first, then gradually spreads to the interior. The swelling process will usually begin at the uphill extreme of the building, or on the weather side where the land is flat. Swelling gradually reaches the interior soil as absorption continues. Shrinkage usually begins where the sunk heat is greatest.

Effects of Uneven Soil Movement on Structures

Erosion and saturation

Erosion removes the support from under footings, tending to create subsidence of the part of the structure under which it occurs. Brickwork walls will resist the stress created by this removal of support by bridging the gap or cantilevering until the bricks or the mortar bedding fail. Older masonry has little resistance. Evidence of failure varies according to circumstances and symptoms may include:

- Step cracking in the mortar beds in the body of the wall or above/below openings such as doors or windows.
- Vertical cracking in the bricks (usually but not necessarily in line with the vertical beds or perpends).

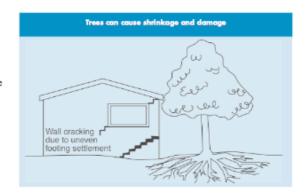
Isolated piers affected by erosion or saturation of foundations will eventually lose contact with the bearers they support and may tilt or fall over. The floors that have lost this support will become bouncy, sometimes rattling ornaments etc.

Seasonal swelling/shrinkage in clay

Swelling foundation soil due to rainy periods first lifts the most exposed extremities of the footing system, then the remainder of the perimeter footings while gradually permeating inside the building footprint to lift internal footings. This swelling first tends to create a dish effect, because the external footings are pushed higher than the internal ones.

The first noticeable symptom may be that the floor appears slightly dished. This is often accompanied by some doors binding on the floor or the door head, together with some cracking of comice mitres. In buildings with timber flooring supported by bearers and joists, the floor can be bouncy. Externally there may be visible dishing of the hip or ridge lines.

As the moisture absorption process completes its journey to the innermost areas of the building, the internal footings will rise. If the spread of moisture is roughly even, it may be that the symptoms will temporarily disappear, but it is more likely that swelling will be uneven, creating a difference rather than a disappearance in symptoms. In buildings with timber flooring supported by bearers and joists, the isolated piers will rise more easily than the strip footings or piers under walls, creating noticeable doming of flooring.



As the weather pattern changes and the soil begins to dry out, the external footings will be first affected, beginning with the locations where the sun's effect is strongest. This has the effect of lowering the external footings. The doming is accentuated and cracking reduces or disappears where it occurred because of dishing, but other cracks open up. The roof lines may become convex.

Doming and dishing are also affected by weather in other ways. In areas where warm, wet summers and cooler dry winters prevail, water migration tends to be toward the interior and doming will be accentuated, whereas where summers are dry and winters are cold and wet, migration tends to be toward the exterior and the underlying propensity is toward dishing.

Movement caused by tree roots

In general, growing roots will exert an upward pressure on footings, whereas soil subject to drying because of tree or shrub roots will tend to remove support from under footings by inducing shrinkage.

Complications caused by the structure itself

Most forces that the soil causes to be exerted on structures are vertical – i.e. either up or down. However, because these forces are seldom spread evenly around the footings, and because the building resists uneven movement because of its rigidity, forces are exerted from one part of the building to another. The net result of all these forces is usually rotational. This resultant force often complicates the diagnosis because the visible symptoms do not simply reflect the original cause. A common symptom is binding of doors on the vertical member of the frame.

Effects on full masonry structures

Brickwork will resist cracking where it can. It will attempt to span areas that lose support because of subsided foundations or raised points. It is therefore usual to see cracking at weak points, such as openings for windows or doors.

In the event of construction settlement, cracking will usually remain unchanged after the process of settlement has ceased.

With local shear or erosion, cracking will usually continue to develop until the original cause has been remedied, or until the subsidence has completely neutralised the affected portion of footing and the structure has stabilised on other footings that remain effective.

In the case of swell/shrink effects, the brickwork will in some cases return to its original position after completion of a cycle, however it is more likely that the rotational effect will not be exactly reversed, and it is also usual that brickwork will settle in its new position and will resist the forces trying to return it to its original position. This means that in a case where swelling takes place after construction and cracking occurs, the cracking is likely to at least partly remain after the shrink segment of the cycle is complete. Thus, each time the cycle is repeated, the likelihood is that the cracking will become wider until the sections of brickwork become virtually independent.

With repeated cycles, once the cracking is established, if there is no other complication, it is normal for the incidence of cracking to stabilise, as the building has the articulation it needs to cope with the problem. This is by no means always the case, however, and monitoring of cracks in walls and floors should always be treated exclusive.

Upheaval caused by growth of tree roots under footings is not a simple vertical shear stress. There is a tendency for the root to also exert lateral forces that attempt to separate sections of brickwork after initial cracking has occurred. The normal structural arrangement is that the inner leaf of brickwork in the external walls and at least some of the internal walls (depending on the roof type) comprise the load-bearing structure on which any upper floors, ceilings and the roof are supported. In these cases, it is internally visible cracking that should be the main focus of attention, however there are a few examples of dwellings whose external leaf of masonry plays some supporting role, so this should be checked if there is any doubt. In any case, externally visible cracking is important as a guide to stresses on the structure generally, and it should also be remembered that the external walls must be capable of supporting themselves.

Effects on framed structures

Timber or steel framed buildings are less likely to exhibit cracking due to swell/shrink than masonry buildings because of their flexibility. Also, the doming/dishing effects tend to be lower because of the lighter weight of walls. The main risks to framed buildings are encountered because of the isolated pier footings used under walls. Where erosion or saturation cause a footing to fall away, this can double the span which a wall must bridge. This additional stress can create cracking in wall linings, particularly where there is a weak point in the structure caused by a door or window opening. It is, however, unlikely that framed structures will be so stressed as to suffer serious damage without first exhibiting some or all of the above symptoms for a considerable period. The same warning period should apply in the case of upheaval. It should be noted, however, that where framed buildings are supported by strip footings there is only one leaf of brickwork and therefore the externally visible walls are the supporting structure for the building. In this case, the subfloor masonry walls can be expected to behave as full brickwork walls.

Effects on brick veneer structures

Because the load-bearing structure of a brick veneer building is the frame that makes up the interior leaf of the external walls plus perhaps the internal walls, depending on the type of roof, the building can be expected to behave as a framed structure, except that the external masonry will behave in a similar way to the external leaf of a full masonry structure.

Water Service and Drainage

Where a water service pipe, a sewer or stormwater drainage pipe is in the vicinity of a building, a water leak can cause erosion, swelling or saturation of susceptible soil. Even a minuscule leak can be enough to saturate a clay foundation. A leaking tap near a building can have the same effect. In addition, trenches containing pipes can become watercourses even though backfilled, particularly where broken nubble is used as fill. Water that runs along these trenches can be responsible for scrious crosion, interstrata scepage into subfloor areas and saturation.

Pipe leakage and trench water flows also encourage tree and shrub roots to the source of water, complicating and exacerbating the problem.

Poor roof plumbing can result in large volumes of rainwater being concentrated in a small area of soil:

 Incorrect falls in roof guttering may result in overflows, as may gutters blocked with leaves etc.

- Corroded guttering or downpipes can spill water to ground.
- Downpipes not positively connected to a proper stormwater collection system will direct a concentration of water to soil that is directly adjacent to footings, sometimes causing large-scale problems such as erosion, saturation and migration of water under the building.

Seriousness of Cracking

In general, most cracking found in masonry walls is a cosmetic nuisance only and can be kept in repair or even ignored. The table below is a reproduction of Table C1 of AS 2870.

AS 2870 also publishes figures relating to cracking in concrete floors, however because wall cracking will usually reach the critical point significantly earlier than cracking in slabs, this table is not reproduced here.

Prevention/Cure

Plumbing

Where building movement is caused by water service, roof plumbing, sewer or stormwater failure, the remedy is to repair the problem. It is prudent, however, to consider also rerouting pipes away from the building where possible, and relocating taps to positions where any leakage will not direct water to the building vicinity. Even where gully traps are present, there is sometimes sufficient spill to create erosion or saturation, particularly in modern installations using smaller diameter PVC fixtures. Indeed, some gully traps are not situated directly under the taps that are installed to charge them, with the result that water from the tap may enter the backfilled trench that houses the sewer piping. If the trench has been poorly backfilled, the water will either pond or flow along the bottom of the trench. As these trenches usually run alongside the footings and can be at a similar depth, it is not hard to see how any water that is thus directed into a trench can easily affect the foundation's ability to support footings or even gain entry to the subfloor area.

Ground drainage

In all soils there is the capacity for water to travel on the surface and below it. Surface water flows can be established by inspection during and after heavy or prolonged rain. If necessary, a grated drain system connected to the stormwater collection system is usually an easy solution.

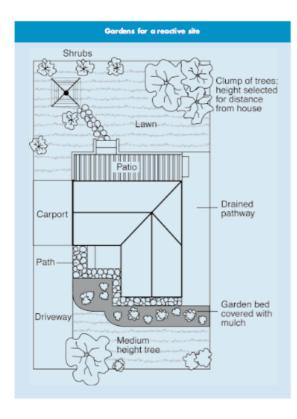
It is, however, sometimes necessary when attempting to prevent water migration that testing be carried out to establish watertable height and subsoil water flows. This subject is referred to in BTF 19 and may properly be regarded as an area for an expert consultant.

Protection of the building perimeter

It is essential to remember that the soil that affects footings extends well beyond the actual building line. Watering of garden plants, shrubs and trees causes some of the most serious water problems.

For this reason, particularly where problems exist or are likely to occur, it is recommended that an apron of paving be installed around as much of the building perimeter as necessary. This paving

Description of typical damage and required repair	Approximate crack width limit (see Note 3)	Damage category
Hairline cracks	<0.1 mm	0
Fine cracks which do not need repair	<1 mm	1
Cracks noticeable but easily filled. Doors and windows stick slightly	⊲ mm	2
Cracks can be repaired and possibly a small amount of wall will need to be replaced. Doors and windows stick. Service pipes can fracture. Weathertightness often impaired	5-15 mm (or a number of cracks 3 mm or more in one group)	3
Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Window and door frames distort. Walls lean or bulge noticeably, some loss of bearing in beams. Service pipes disrupted	15–25 mm but also depend on number of cracks	4



should extend outwards a minimum of 900 mm (more in highly reactive soil) and should have a minimum fall away from the building of 1:60. The finished paving should be no less than 100 mm below brick vent bases.

It is prudent to relocate drainage pipes away from this paving, if possible, to avoid complications from future leakage. If this is not practical, earthenware pipes should be replaced by PVC and backfilling should be of the same soil type as the surrounding soil and compacted to the same density.

Except in areas where freezing of water is an issue, it is wise to remove taps in the building area and relocate them well away from the building – preferably not uphill from it (see BTF 19).

It may be desirable to install a grated drain at the outside edge of the paving on the uphill side of the building. If subsoil drainage is needed this can be installed under the surface drain.

Condensation

In buildings with a subfloor void such as where bearers and joists support flooring, insufficient ventilation creates ideal conditions for condensation, particularly where there is little clearance between the floor and the ground. Condensation adds to the moisture already present in the subfloor and significantly slows the process of drying out. Installation of an adequate subfloor ventilation system, either natural or mechanical, is desirable.

Warning: Although this Building Technology File deals with cracking in buildings, it should be said that subfloor moisture can result in the development of other problems, notably:

- Water that is transmitted into masonry, metal or timber building elements causes damage and/or decay to those elements.
- High subfloor humidity and moisture content create an ideal environment for various pests, including termites and spiders.
- Where high moisture levels are transmitted to the flooring and walls, an increase in the dust mite count can ensue within the living areas. Dust mites, as well as dampness in general, can be a health hazard to inhabitants, particularly those who are abnormally susceptible to respiratory ailments.

The garden

The ideal vegetation layout is to have lawn or plants that require only light watering immediately adjacent to the drainage or paving edge, then more demanding plants, shrubs and trees spread out in that order.

Overwatering due to misuse of automatic watering systems is a common cause of saturation and water migration under footings. If it is necessary to use these systems, it is important to remove garden beds to a completely safe distance from buildings.

Existing trees

Where a tree is causing a problem of soil drying or there is the existence or threat of upheaval of footings, if the offending roots are subsidiary and their removal will not significantly damage the tree, they should be severed and a concrete or metal barrier placed vertically in the soil to prevent future root growth in the direction of the building. If it is not possible to remove the relevant roots without damage to the tree, an application to remove the tree should be made to the local authority. A prudent plan is to transplant likely offenders before they become a problem.

Information on trees, plants and shrubs

State departments overseeing agriculture can give information regarding root patterns, volume of water needed and safe distance from buildings of most species. Botanic gardens are also sources of information. For information on plant roots and drains, see Building Technology File 17.

Excavation

Excavation around footings must be properly engineered. Soil supporting footings can only be safely excavated at an angle that allows the soil under the footing to remain stable. This angle is called the angle of repose (or friction) and varies significantly between soil types and conditions. Removal of soil within the angle of repose will cause subsidence.

Remediation

Where erosion has occurred that has washed away soil adjacent to footings, soil of the same classification should be introduced and compacted to the same density. Where footings have been undermined, augmentation or other specialist work may be required. Remediation of footings and foundations is generally the realm of a specialist consultant.

Where isolated footings rise and fall because of swell/shrink effect, the homeowner may be tempted to alleviate floor bounce by filling the gap that has appeared between the bearer and the pier with blocking. The danger here is that when the next swell segment of the cycle occurs, the extra blocking will push the floor up into an accentuated dome and may also cause local shear failure in the soil. If it is necessary to use blocking, it should be by a pair of fine wedges and monitoring should be carried out fortnightly.

This BTF was prepared by John Lewer FAIB, MIAMA, Partner, Construction Diagnosis.

The information in this and other issues in the series was derived from various sources and was believed to be correct when published.

The information is advisory. It is provided in good faith and not claimed to be an exhaustive treatment of the relevant subject.

Further professional advice needs to be obtained before taking any action based on the information provided.

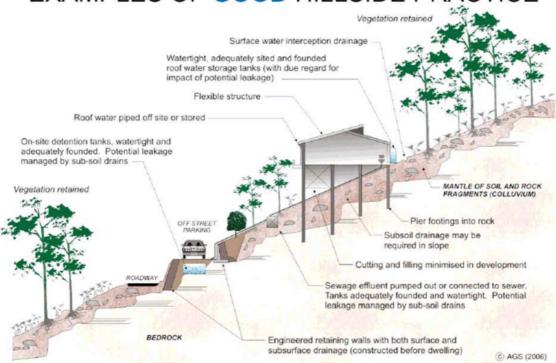
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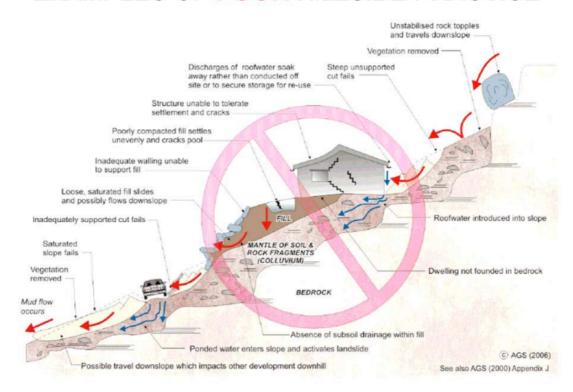
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EXAMPLES OF GOOD HILLSIDE PRACTICE



EXAMPLES OF POOR HILLSIDE PRACTICE



PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

APPENDIX C: LANDSLIDE RISK ASSESSMENT

QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY

QUALITATIVE MEASURES OF LIKELIHOOD

Approximate	Approximate Annual Probability	Implied Indicative Landslide	e Landslide			-
Indicative Value	Notional Boundary	Recurrence Interval	Interval	Description	Descriptor	Геле
10.1	5×10-2	10 years		The event is expected to occur over the design life.	ALMOST CERTAIN	A
10-2	0.00 0.00	100 years	20 years	The event will probably occur under adverse conditions over the design life.	LIKELY	В
10^{-3}	0XIO	1000 years	2000 years	The event could occur under adverse conditions over the design life.	POSSIBLE	C
10-4	5x10".	10,000 years	Superior OOU OC	The event might occur under very adverse circumstances over the design life.	UNLIKELY	D
10-5	5x10°	100,000 years	zo,ooo years	The event is conceivable but only under exceptional circumstances over the design life.	RARE	E
10^{-6}	OIXC	1,000,000 years	200,000 years	The event is inconceivable or fanciful over the design life.	BARELY CREDIBLE	F
No. of the Control of				m 111 1 111		

The table should be used from left to right; use Approximate Annual Probability or Description to assign Descriptor, not vice versa. Ξ Note:

QUALITATIVE MEASURES OF CONSEQUENCES TO PROPERTY

Approximate	Approximate Cost of Damage			
Indicative Value	Notional Boundary	Description	Descriptor	revel
200%	,0001	Structure(s) completely destroyed and/or large scale damage requiring major engineering works for stabilisation. Could cause at least one adjacent property major consequence damage.	CATASTROPHIC	1
%09	100%	Extensive damage to most of structure, and/or extending beyond site boundaries requiring significant stabilisation works. Could cause at least one adjacent property medium consequence damage.	MAJOR	2
20%	40%	Moderate damage to some of structure, and/or significant part of site requiring large stabilisation works. Could cause at least one adjacent property minor consequence damage.	MEDIUM	3
5%	10%	Limited damage to part of structure, and/or part of site requiring some reinstatement stabilisation works.	MINOR	4
0.5%		Little damage. (Note for high probability event (Almost Certain), this category may be subdivided at a notional boundary of 0.1%. See Risk Matrix.)	INSIGNIFICANT	5

The Approximate Cost of Damage is expressed as a percentage of market value, being the cost of the improved value of the unaffected property which includes the land plus the 6 Notes:

The Approximate Cost is to be an estimate of the direct cost of the damage, such as the cost of reinstatement of the damaged portion of the property (land plus structures), stabilisation works required to render the site to tolerable risk level for the landslide which has occurred and professional design fees, and consequential costs such as legal fees, temporary accommodation. It does not include additional stabilisation works to address other landslides which may affect the property. 3

(4) The table should be used from left to right; use Approximate Cost of Damage or Description to assign Descriptor, not vice versa

PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

APPENDIX C: - QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY (CONTINUED)

QUALITATIVE RISK ANALYSIS MATRIX – LEVEL OF RISK TO PROPERTY

LIKELIHOOD	000	CONSEQUI	CONSEQUENCES TO PROPERTY (With Indicative Approximate Cost of Damage)	RTY (With Indicati	ve Approximate Cost	of Damage)
	Indicative Value of Approximate Annual Probability	1: CATASTROPHIC 200%	2: MAJOR 60%	3: MEDIUM 20%	4: MINOR 5%	5: INSIGNIFICANT 0.5%
A - ALMOST CERTAIN	10-1	НА	VH	VH	Н	M or L (5)
B - LIKELY	10^{-2}	НΛ	ΗΛ	Н	M	${f T}$
C - POSSIBLE	10 ⁻³	HΛ	Н	M	M	ΛΓ
D - UNLIKELY	10-4	н	M	Т	Г	ΛΓ
E - RARE	10-5	M	L	Г	VL	VL
F - BARELY CREDIBLE	10-6	Т	ΛΓ	ΛΓ	VL	VL

ଡିଡ Notes:

For Cell A5, may be subdivided such that a consequence of less than 0.1% is Low Risk.

When considering a risk assessment it must be clearly stated whether it is for existing conditions or with risk control measures which may not be implemented at the current time.

RISK LEVEL IMPLICATIONS

	Risk Level	Example Implications (7)
		Unacceptable without treatment. Extensive detailed investigation and research, planning and implementation of treatment
VH	VERY HIGH RISK	options essential to reduce risk to Low; may be too expensive and not practical. Work likely to cost more than value of the
		property.
		Theoremetable without treatment. Detailed investigation relaming and implementation of treatment antions required to reduce
Н	HIGH RISK	chacepagns without treatment. Detailed hivestigation, planning and implementation of treatment opinions required to reduce risk to Low. Work would cost a substantial sum in relation to the value of the property.
		May be tolerated in certain circumstances (subject to regulator's approval) but requires investigation, planning and
M	MODERATE RISK	implementation of treatment options to reduce the risk to Low. Treatment options to reduce to Low risk should be
		implemented as soon as practicable.
•	ASIG MOT	Usually acceptable to regulators. Where treatment has been required to reduce the risk to this level, ongoing maintenance is
7	LOW KISA	required.
VI.	VERY I OW RISK	Acceptable. Manage by normal slope maintenance procedures.
	NOW HOT INT	

The implications for a particular situation are to be determined by all parties to the risk assessment and may depend on the nature of the property at risk; these are only given as a general guide. Note: (7)