

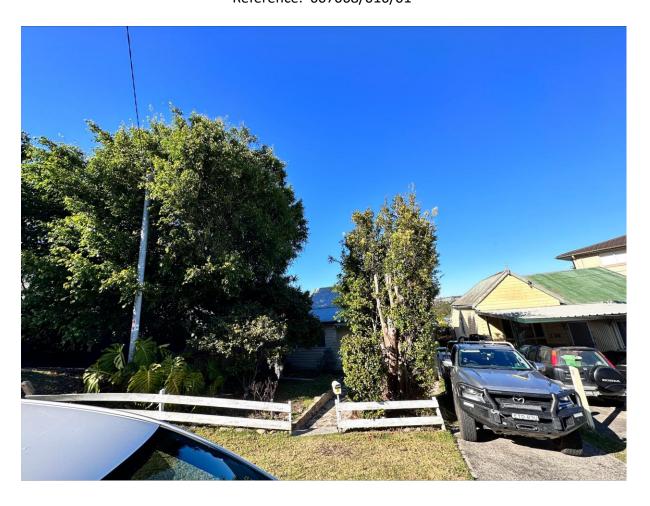
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> October 23, 2023 Project No. 30055/9201 Report No. 23/3478 MT/fr

# **SUMMARY SHEET**

Client: McDonald Jones Homes Address: Lot 1, 36 Dalley Street, Queenscliff Reference: 607068/016/01



SITE CLASSIFICATION	Р	AS2870-2011
WIND CLASSIFICATION	N2	AS4055-2021
EXPOSURE CLASSIFICATION	A1	AS2870-2011

This summary sheet must be read in conjunction with the full report.



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# SITE INVESTIGATION REPORT

Client: McDonald Jones Homes

Address: Lot 1, 36 Dalley Street, Bilgola Plateau Proposed Development: Residential dwelling

# **Site Description**

Approx. area (m<sup>2</sup>): 295

Approx. fall: 1.5 metres to the southwest, reasonable site drainage

Vegetation: Grass, shrubs and trees Improvements: Existing dwelling

# Geology, Fieldwork Details and Subsurface Conditions

The Sydney geological series sheet, at a scale of 1:100,000 shows that the site is underlain by Hawkesbury Sandstone. Rocks within this formation comprise medium to coarse grained quartz sandstone, minor shale and laminite lenses.

Two boreholes were drilled and two Dynamic Cone penetrometer (DCP) tests were carried out on October 13, 2023 at the locations shown on Drawing No. 23/3478. Restricted site access dictated the borehole locations. *Because there was no access for the drilling rig, BH2 was drilled using a hand auger.* The subsurface conditions encountered are shown on the attached borehole logs. Explanation sheets and notes relating to geotechnical reports are also attached.

When assessing the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour regarding the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies.

The subsurface conditions consist of topsoil/fill overlying natural silty sands and weathered sandstone. Topsoil/fill is present to a depth of 0.6 metres in BH1 and to the depth of hand auger refusal on weathered sandstone, 0.8 metres in BH2. Medium dense silty sands underlie the topsoil/fill to the depth of auger refusal, 0.8 metres in BH1.



No groundwater was observed in the boreholes during the fieldwork.

#### Wind Classification

The classification given below has been prepared to assist the designer in accordance with the guidelines set out in AS4055-2021 "Wind loads for housing" and expected future development conditions at the site and surrounding areas. Final designs should be verified by an experienced qualified building engineer to accurately determine the appropriate Wind Classifications in accordance with the Building Code of Australia.

Region	А
Terrain Category	TC3
Topographic Classification	T2
Shielding	FS
Rating	N2

#### Site Classification

The classification has been prepared in accordance with the guidelines set out in the "Residential Slabs and Footings" Code, AS2870 - 2011.

Because there are trees and an existing dwelling present, abnormal moisture conditions (AMC) prevail at the site. (Refer to Section 1.3.3 of AS2870).

Because of the AMC and over 400mm of fill, the site is classified a *Problem Site (P)*. Because the fill is undocumented and does not appear to be placed as controlled engineered fill it is not appropriate to reclassify this site.

Foundation design and construction consistent with this classification shall be adopted as specified in the above referenced standard and in accordance with the following design details.

# Foundation Design and Construction

The topsoil/fill are unsuitable for providing foundation support.

Pad and/or strip footings founded in medium dense silty sands below any topsoil/fill, may be proportioned using an allowable bearing pressure of 100kPa. The minimum depth of founding must comply with the requirements of AS2870.

Footings and piers founded in the weathered sandstone may be proportioned using an allowable end bearing pressure of 800 kPa. An allowable adhesion of 80 kPa may be adopted for the portion of the shaft within the weathered sandstone. When piers are founded in sandstone the adhesion within the overlying soils must be ignored. An experienced geotechnical engineer should confirm appropriate founding levels and allowable bearing



pressures during construction, based on assessment made during footing excavation or pier hole drilling.

During footing excavation or site preparation, weathered sandstone may be encountered at some locations. If this occurs, bucket piers or the like should be used to ensure all footings bear on materials of similar stiffness.

In order to ensure the bearing values given can be achieved, care should be taken to ensure the base of the excavations is free of all loose material prior to concreting. To this end, it is recommended that all excavations be concreted as soon as possible, preferably immediately after excavating, cleaning, inspecting and approval. Pier excavations should not be left open overnight. The possibility of groundwater inflow needs to be considered when drilling the piers and pouring concrete.

The site is considered suitable for slab on ground construction provided due regard is given to the ground surface slope and the fill is certified as being placed in a controlled manner. Otherwise, piers will be required to suspend the slab. Footings and slabs may be proportioned for soil movements consistent with a *Slightly Reactive (S)* classification.

During foundation construction, should the subsurface conditions vary to those inferred in this report, a suitably experienced geotechnical engineer should review the design and recommendations given above to determine if any alterations are required.

## Soil Aggressiveness

The exposure classification for the concrete has been determined for the onsite soils. The exposure classification is obtained from Tables 5.1 and 5.2 of AS2870-2011. In regards to the electrical conductivity, the laboratory test results have been multiplied by the appropriate factor to convert the results to EC<sub>e</sub>.

Detailed test reports are attached and summarised below, together with the exposure classification.

Sample No.	Electrical Conductivity (dS/m)		рН	Sulfate (ppm)	Exposure Classification
	EC <sub>1:5</sub>	EC <sub>e</sub>			
S1/9201	0.033	0.3	7.0	<10	A1

The minimum concrete strength and reinforcement cover required for the various exposure classifications are given in Tables 5.3 and 5.4 of AS2870-2011 (see attached).



#### **Additional Comments**

Attention is drawn to Appendix B of AS2870 - 2011 regarding the need to properly maintain the foundations. Surface drainage should be provided to avoid the possibility of water ponding near the building and the finished ground surface should fall at least 50 mm over one metre away from the building.

The above classification has been made assuming that all footings will bear in either natural ground or in controlled filling. Prior to the placement of any filling the existing surface should be stripped of all vegetation and topsoil.

If excavations for rainwater or detention tanks are to be made within 6 metres of the building foundations, advice should be sought regarding their effect on the foundations.

Placing absorption trenches on the high side of the property may create abnormal moisture conditions for the foundations (Refer to Section 1.3.3 of AS2870). This could have a negative effect on the foundation performance and more than likely alter the site classification provided above.

This report has been prepared assuming that no trees other than those noted will be present on the site. If future tree planting is planned, eg. there is a landscaping plan, their effect on the foundation performance must be considered.

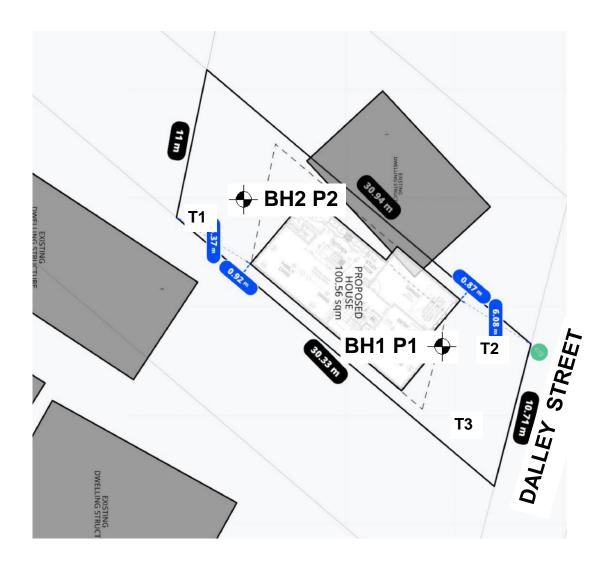
This report has been prepared assuming the site development will be limited to one or two storey residential buildings. The information and interpretation may not be relevant if the design proposal changes (e.g. to a five-storey building involving major cuts during the site preparation). If changes occur, we would be pleased to review the report and advise on the adequacy of the investigation.

Yours faithfully,

Mrigesh Tamang

Senior Geotechnical Engineer

STS Geotechnics Pty Limited





STS Geotechnics Pty. Ltd.

Client: McDONALD JONES HOMES

SITE INVESTIGATION
LOT 1, 36 DALLEY STREET, QUEENSCLIFF
BOREHOLE AND PENETROMETER LOCATIONS

Scale: Unknown
Date: October 2023

Project No.
30055/9201

Drawing No: 23/3478

# **Important Information**



## INTRODUCTION

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report. When copies of reports are made, they should be reproduced in full.

## **GEOTECHNICAL REPORTS**

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by STS Geotechnics Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions. The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, STS Geotechnics Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

# **UNFORSEEN CONDITIONS**

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, STS Geotechnics Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows reinterpretation and assessment of the implications for future work.

## SUBSURFACE CONDITIONS

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on the drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

# SUPPLY OF GETEOECHNICAL INFORMATION OR TENDERING PURPOSES

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.

# **Exposure Classification** and Concrete Requirements



# TABLE 5.1 FROM AS2870-2011

## **EXPOSURE CLASSIFICATION FOR CONCRETE IN SALINE SOILS**

Saturated Extract Electrical Conductivity (EC <sub>c</sub> ), dS/m	Exposure Classification
<4	A1
4-8	A2
8-16	B1
>16	B2

#### NOTES:

- 1. Guidance on concrete in saline environments can be found in CCAA T56.
- 2. Exposure classifications are from AS3600.
- 3. The currently accepted method of determining the salinity level of the soil is by measuring the extract electrical conductivity (EC) of a soil and water mixture in deciSiemens per metre (dS/m) and using conversion factors that allow for the soil texture to determine the saturated extract electrical conductivity (EC<sub>e</sub>).
- 4. The division between a non-saline and saline soil is generally regarded as an EC<sub>e</sub> value of 4 dS/m, therefore no increase in the minimum concrete strength is required below this value.

# **TABLE 5.2 FROM AS2870-2011**

## **EXPOSURE CLASSIFICATION FOR CONCRETE IN SULFATE SOILS**

Exp	oosure Conditions	Exposure Classification		
Sulfates (expr	essed as SO <sub>4</sub> )*			
In Soil	In Groundwater	рН	Soil Conditions	Soil Conditions
ppm	ppm		A†	B‡
<5000	<1000	>5.5	A2	A1
5000-10 000	1000-3000	4.5-5.5	B1	A2
10 000-20 000	3000-10 000	4-4.5	B2	B1
>20 000	>10 000	<4	C2	B2

- Approximately 100 ppm SO<sub>4</sub> = 80 ppm SO<sub>3</sub>.
- † Soil conditions A high permeability soils (eg. Sands and gravels) that are in groundwater.
- ‡ Soil conditions B low permeability soils (eg. Silts and clays) or all soils have groundwater.

# **Exposure Classification** and Concrete Requirements



# **TABLE 5.3 FROM AS2870-2011**

# MINIMUM DESIGN CHARACTERISTIC STRENGTH (f'c) AND CURING REQUIREMENTS FOR CONCRETE

Exposure Classification	Minimum f'c MPa	Minimum Initial Curing Requirement
A1	20	Cure continuously for at
A2	25	least 3 days
B1	32	
B2	40	Cure continuously for at
C1	≥50	least 7 days
C2	≥50	

# **TABLE 5.4 – FROM AS2870-2011**

# MINIMUM REINFORCEMENT COVER FOR CONCRETE

Exposure Classification	Minimum Cover in Saline Soils* (mm)	Minimum Cover in Sulfate Soils† (mm)
A1	See Clause 5.3.2	40
A2	45	50
B1	50	60
B2	55	65
C1	‡	70
C2	‡	85

- \* Where a damp-proofing membrane is installed, the minimum reinforcement cover in saline soils may be reduced to 30 mm.
- † Where a damp-proofing membrane is installed, the minimum reinforcement cover in sulfate soils may be reduced by 10 mm.
- ‡ Saline soils have a maximum exposure classification of B2 as per Table 5.1.

# STS Geotechnics Pty Ltd

# **GEOTECHNICAL LOG - NON CORE BOREHOLE**

			Project: 30055/9201	BOREHOLE NO.: BH 1			
		6 Dalley Street, Queenscliff Date: October 13, 2023 o Drawing No. 23/3478 Logged: PS Checked By: MT		Sheet 1 of 1			
W AT TA EB RL	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  Soil Name, grain size /plasticity, colour; secondary constituents (Inc. Description), minor constituents including other remarks	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E	
			TOPSOIL/FILL: CLAYEY SAND: fine to medium to coarse grained, dark grey, rootlets	SC	_	М	
	S1 @ 0.3 m	0.5					
			SILTY SAND: fine to medium to coarse grained, brown	SM	MEDIUM DENSE	М	
		1.0	AUGER REFUSAL AT 0.8 M ON WEATHERED SANDSTONE				
	D - disturbe	Contractor: STS Equipment: Christie					
	S - jar samp				eter (mm): 100		
NOTES:	·		See explanation sheets for meaning of all descriptive terms and symbols  An		Vertical (°): 0		
L							

# STS Geotechnics Pty Ltd

# **GEOTECHNICAL LOG - NON CORE BOREHOLE**

Client: McDonald Jones Homes Project: Lot 1, 36 Dalley Street, Queenso			Project: 30055/9201	BOREHOLE NO.: BH 2			
		ley Street, Quee wing No. 23/34		Sheet 1 of 1			
W AT TA EB RL	S A M P L E	<b>DEPTH</b> (m)	DESCRIPTION OF DRILLED PRODUCT  Soil Name, grain size /plasticity, colour; secondary constituents (Inc. Description), minor constituents including other remarks	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E	
			TOPSOIL/FILL: CLAYEY SAND: fine to medium to coarse grained, dark grey, rootlets	SC	_	M	
		0.5	HAND AUGER REFUSAL AT 0.6 M ON WEATHERED SANDSTONE				
		1.0					
		2.0					
		2.5					
	D - disturbe			ntractor			
		f water table or			:: Hand Auger		
	S - jar samp	ie			eter (mm): 100  Vertical (°): 0		
NOTES:				rill Bit: S			



# **STS Geotechnics Pty Ltd**

14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



# Dynamic Cone Penetrometer Test Report

Project: LOT 1, 36 DALLEY STRRET, QUEENSCLIFF Project No.: 30055/9201

Client: MCDONALD JONES HOMES Report No.: 23/3477

Address: 62 Norwest Boulevarde, Baulkham Hills Report Date: 16/10/2023

Test Method: AS 1289.6.3.2 Page: 1 of 1

	,		_			,
Site No.	P1	P2				
Location	Refer to Drawing No. 23/3478	Refer to Drawing No. 23/3478				
Date Tested	13/10/2023	13/10/2023				
Starting Level	Surface Level	Surface Level				
Depth (m)		Pe	netration Resistar	nce (blows / 150m	ım)	
0.00 - 0.15	2	2				
0.15 - 0.30	2	2				
0.30 - 0.45	4	3				
0.45 - 0.60	4	2				
0.60 - 0.75	Refusal	Refusal				
0.75 - 0.90						
0.90 - 1.05						
1.05 - 1.20						
1.20 - 1.35						
1.35 - 1.50						
1.50 - 1.65						
1.65 - 1.80						
1.80 - 1.95						
1.95 - 2.10						
2.10 - 2.25						
2.25 - 2.40						
2.40 - 2.55						
2.55 - 2.70						
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: \* Pre drilled prior to testing

PS

Technician:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Form: RPS26 Date of Issue: 31/05/21 Revision: 2



Client

# **CERTIFICATE OF ANALYSIS**

**Work Order** : ES2335698

: STS Geotechnics Contact **ENQUIRES STS** 

Address : Unit 14/1 Cowpasture Place

Wetherill Park 2164

Telephone

Project : 30055/30060/32453/32454

Order number : 2023-365

C-O-C number : ----

Sampler : IS. MB. PS

Site

Quote number : EN/222 No. of samples received : 13 No. of samples analysed : 13

Page : 1 of 5

Laboratory : Environmental Division Sydney

Contact : Customer Services ES

Address : 277-289 Woodpark Road Smithfield NSW Australia 2164

Telephone : +61-2-8784 8555

**Date Samples Received** : 17-Oct-2023 11:30

Date Analysis Commenced : 18-Oct-2023

Issue Date : 20-Oct-2023 12:16



This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with **Quality Review and Sample Receipt Notification.** 

#### **Signatories**

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories Position Accreditation Category

Ankit Joshi Senior Chemist - Inorganics Sydney Inorganics, Smithfield, NSW Page : 2 of 5 Work Order : ES2335698

Client : STS Geotechnics
Project : 30055/30060/32453/32454



#### **General Comments**

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contract for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

- ^ = This result is computed from individual analyte detections at or above the level of reporting
- ø = ALS is not NATA accredited for these tests.
- ~ = Indicates an estimated value.
- ED045G: The presence of Thiocyanate, Thiosulfate and Sulfite can positively contribute to the chloride result, thereby may bias results higher than expected. Results should be scrutinised accordingly.

Page : 3 of 5
Work Order : ES2335698

 Client
 : STS Geotechnics

 Project
 : 30055/30060/32453/32454



# Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	30055/9201	30055/9212	30055/9224	30055/9228	30055/9229
		Samplii	ng date / time	16-Oct-2023 00:00				
Compound	CAS Number	LOR	Unit	ES2335698-001	ES2335698-002	ES2335698-003	ES2335698-004	ES2335698-005
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	7.0	5.4	5.3	7.2	7.1
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	33	26	55	44	186
EA055: Moisture Content (Dried @ 105-	-110°C)							
Moisture Content		0.1	%	8.4	12.8	10.2	7.3	11.6
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	<10	20	40	20	140

Page : 4 of 5
Work Order : ES2335698

 Client
 : STS Geotechnics

 Project
 : 30055/30060/32453/32454



# Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	30055/9230	30055/9231	30055/9232	30055/9233	30055/9234
		Samplii	ng date / time	17-Oct-2023 00:00	17-Oct-2023 00:00	17-Oct-2023 00:00	17-Oct-2023 00:00	16-Oct-2023 00:00
Compound	CAS Number	LOR	Unit	ES2335698-006	ES2335698-007	ES2335698-008	ES2335698-009	ES2335698-010
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	8.4	7.2	7.6	7.2	7.4
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	614	223	292	273	418
EA055: Moisture Content (Dried @ 105-	110°C)							
Moisture Content		0.1	%	6.6	11.2	11.4	8.7	16.1
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	350	80	120	120	300

Page : 5 of 5
Work Order : ES2335698

 Client
 : STS Geotechnics

 Project
 : 30055/30060/32453/32454



# Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	30060/1862	32453/S1	32454/S1	 
		Sampli	ng date / time	17-Oct-2023 00:00	16-Oct-2023 00:00	16-Oct-2023 00:00	 
Compound	CAS Number	LOR	Unit	ES2335698-011	ES2335698-012	ES2335698-013	 
				Result	Result	Result	 
EA002: pH 1:5 (Soils)							
pH Value		0.1	pH Unit	8.8	6.7	6.0	 
EA010: Conductivity (1:5)	EA010: Conductivity (1:5)						
Electrical Conductivity @ 25°C		1	μS/cm	501	19	27	 
EA055: Moisture Content (Dried @ 105-11	10°C)						
Moisture Content		0.1	%	7.3	11.1	7.8	 
ED040S : Soluble Sulfate by ICPAES							
Sulfate as SO4 2-	14808-79-8	10	mg/kg	240	10	10	 
ED045G: Chloride by Discrete Analyser							
Chloride	16887-00-6	10	mg/kg		100	20	 



# **EXPLANATION OF NOTES, ABBREVIATIONS & TERMS USED ON BOREHOLE AND TEST PIT LOGS**

	^ ^ \	N METHOD

НА	Hand Auger	ADH	Hollow Auger	NQ	Diamond Core - 47 mm
DT	Diatube Coring	RT	Rotary Tricone bit	NMLC	Diamond Core - 52 mm
NDD	Non-destructive digging	RAB	Rotary Air Blast	HQ	Diamond Core - 63 mm
AD*	Auger Drilling	RC	Reverse Circulation	HMLC	Diamond Core - 63 mm
*V	V-Bit	PT	Push Tube	EX	Tracked Hydraulic Excavator
*T	TC-Bit, e.g. AD/T	WB	Washbore	HAND	Excavated by Hand Methods

#### PENETRATION RESISTANCE

ı Low Resistance Rapid penetration/ excavation possible with little effort from equipment used.

Penetration/ excavation possible at an acceptable rate with moderate effort from equipment used. M **Medium Resistance** 

Penetration/ excavation is possible but at a slow rate and requires significant effort from **High Resistance** Н

equipment used.

Refusal/Practical Refusal No further progress possible without risk of damage or unacceptable wear to equipment used. R

These assessments are subjective and are dependent on many factors, including equipment power and weight, condition of excavation or drilling tools and experience of the operator.

#### **WATER**

**GWNO** 

**¥** Standing Water Level

Partial water loss

**>** Water Seepage

**Complete Water Loss** GROUNDWATER NOT OBSERVED - Observation of groundwater, whether present or not, was not possible

due to drilling water, surface seepage or cave-in of the borehole/ test pit.

GROUNDWATER NOT ENCOUNTERED - Borehole/ test pit was dry soon after excavation. However, **GWNE** 

groundwater could be present in less permeable strata. Inflow may have been observed had the borehole/ test pit

been left open for a longer period.

#### **SAMPLING AND TESTING**

Standard Penetration Testing to AS1289.6.3.3 2004 SPT

4,7,11 = Blows per 150mm. N = Blows per 300mm penetration following a 150mm seating drive 4.7.11 N=18 Where practical refusal occurs, the blows and penetration for that interval are reported, N is not reported 30/80mm

Penetration occurred under the rod weight only, N<1 RW

НW Penetration occurred under the hammer and rod weight only, N<1

Hammer double bouncing on anvil, N is not reported HB

Sampling

S1 Jar sample – number indicates sample number

Disturbed Sample **Bulk disturbed Sample** 

В Thin walled tube sample - number indicates nominal sample diameter in millimetres U50

Testing

D

Pocket Penetrometer test expressed as instrument reading in kPa PΡ

Dynamic Cone Penetrometer (AS1289.6.3.1 1997) DCP Perth Sand Penetrometer (AS1289.6.3.2 1997) PSP

### **GEOLOGICAL BOUNDARIES**

- -?- -?- -?- - = Boundary = Observed Boundary = Observed Boundary (Interpreted or inferred) (Position known) (Position approximate)

# **ROCK CORE RECOVERY**

TCR =Total Core Recovery (%) RQD = Rock Quality Designation (%)

 $\frac{\textit{Length of core recovered}}{\times 100} \times 100$  $= \frac{\sum Axial \ lengths \ of \ core > 100mm}{\times 100} \times 100$ Length of core run Length of core run



# METHOD OF SOIL DESCRIPTION USED ON **BOREHOLE AND TEST PIT LOGS**



FILL

COUBLES or **BOULDERS** 

SILT (ML or MH)

ORGANIC SOILS (OL, OH or Pt)

CLAY (CL, CI or CH)

SAND (SP or SW)

GRAVEL (GP or GW)

Combinations of these basic symbols may be used to indicate mixed materials such as sandy clay

## **CLASSIFICATION AND INFERRED STRATIGRAPHY**

Soil is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS 1726:2017, Section 6.1 -Soil description and classification.

PARTICI	LE SIZE CHAR	CS	GROUP SY	MBOLS			
Fraction	Components	Sub			visions	Symbol	Description
Oversize	BOULDERS	Division	mm >200		6 of n is	GW	Well graded gravel and gravel-sand mixtures, little or no fines, no dry strength.
Oversize	COBBLES		63 to 200	SILS luding r thar	GRAVEL More than 50% of coarse fraction is >2.36mm	GP	Poorly graded gravel and gravel-sand mixtures, little or no fines, no dry
		Coarse	19 to 63	exc exc eate	Se fi		strength. Silty gravel, gravel-sand-silt mixtures,
	GRAVEL	Medium	6.7 to 19	NEC Soil S gre	dore	GM	zero to medium dry strength.
Coarse	-	Fine	2.36 to 6.7	GRAINED SOILS 5% of soil excludir ction is greater tha 0.075mm	20	GC	Clayey gravel, gravel-sand-clay mixtures, medium to high dry strength.
grained soil	SAND	Coarse	0.6 to 2.36	SE G an 65 fract 0.0	% of n is	SW	Well graded sand and gravelly sand, little or no fines, no dry strength.
		Medium	0.21 to 0.6	COARSE GRAINED SOILS More than 65% of soil excluding oversize fraction is greater than 0.075mm	SAND More than 50% coarse fraction <2.36 mm	SP	Poorly graded sand and gravelly sand, little or no fines, no dry strength.
		Fine	0.075 to 0.21			SM	Silty sand, sand-silt mixtures, zero to medium dry strength.
Fine	SILT		0.002 to 0.075		Mor	SC	Clayey sand, sandy-clay mixtures, medium to high dry strength.
grained soil	CLAY	NTV DD ODE	<0.002	ding lan	.SS <	ML	Inorganic silts of low plasticity, very fine sands, rock flour, silty or clayey fine sands, zero to medium dry strength.
60	PLASTICITY PROPERTIES				Liquid Limit less 50%	CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, medium to high dry strength.
50 - 50 -	, un 20				Liquic	OL	Organic silts and organic silty clays of low plasticity, low to medium dry strength.
10 EX /		CH or O	1,013	FINE GRAINED SOILS More than 35% of soil excluding oversized fraction is less than 0.075mm	T ^%	МН	Inorganic silts of high plasticity, high to very high dry strength.
¥ 101 20 €	MH or OH			FIIA ore th	Liquid Limit > than 50%	СН	Inorganic clays of high plasticity, high to very high dry strength.
PLAS				_		ОН	Organic clays of medium to high plasticity, medium to high dry strength.
0 10 20 30 40 50 60 70 80 90 100				High Orga soi	nic	PT	Peat muck and other highly organic soils.

## **MOISTURE CONDITION**

Symbol	Term	Description
D	Dry	Non- cohesive and free running.
М	Moist	Soils feel cool, darkened in colour. Soil tends to stick together.
W	Wet	Soils feel cool, darkened in colour. Soil tends to stick together, free water forms when handling.

Moisture content of cohesive soils shall be described in relation to plastic limit (PL) or liquid limit (LL) for soils with higher moisture content as follows: Moist, dry of plastic limit (w < PL); Moist, near plastic limit (w ≈ PL); Moist, wet of plastic limit (w < PL); Wet, near liquid limit ( $w \approx LL$ ), Wet, wet of liquid limit (w > LL),

CONSISTENCY						
Symbol	Term	Undrained Shear Strength (kPa)	SPT "N" #			
VS	Very Soft	≤ 12	≤ 2			
S	Soft	>12 to ≤ 25	>2 to ≤ 4			
F	Firm	>25 to ≤ 50	>4 to 8			
St	Stiff	>50 to ≤ 100	>8 to 15			
VSt	Very Stiff	>100 to ≤ 200	>15 to 30			
Н	Hard	>200	>30			
Fr	Friable	=	•			

CONCICTENCY

DENSITY					
Symbol	Term	Density Index %	SPT "N" #		
VL	Very Loose	≤ 15	0 to 4		
L	Loose	>15 to ≤ 35	4 to 10		
MD	Medium Dense	>35 to ≤ 65	10 to 30		
D	Dense	>65 to ≤ 85	30 to 50		
VD	Very Dense	>85	Above 50		
	•				

In the absence of test results, consistency and density may be assessed from correlations with the observed behaviour of the material. # SPT correlations are not stated in AS1726:2017, and may be subject to corrections for overburden pressure, moisture content of the soil, and equipment type

MINOR COMPONENTS					
Term	Assessment Guide Proportion by Mass				
Add 'Trace'	Presence just detectable by feel or eye but soil properties little or no different to general properties of primary component	Coarse grained soils: ≤ 5% Fine grained soil: ≤ 15%			
Add 'With'	Presence easily detectable by feel or eye but soil properties little or no different to general properties of primary component	Coarse grained soils: 5 - 12% Fine grained soil: 15 - 30%			
Prefix soil name	Presence easily detectable by feel or eye in conjunction with the general properties of primary component	Coarse grained soils: >12% Fine grained soil: >30%			



# TERMS FOR ROCK MATERIAL STRENGTH AND WEATHERING

#### **CLASSIFICATION AND INFERRED STRATIGRAPHY**

Rock is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS1726 – 2017, Section 6.2 – Rock identification, description and classification.

## **ROCK MATERIAL STRENGTH CLASSIFICATION**

Symbol	Term	Point Load Index, Is <sub>(50)</sub> (MPa) #	Field Guide
VL	Very Low	0.03 to 0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxial sample by hand. Pieces up to 30 mm can be broken by finger pressure.
L	Low	0.1 to 0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
М	Medium	0.3 to 1	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
Н	High	1 to 3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken with pick with a single firm blow; rock rings under hammer.
VH	Very High	3 to 10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
EH	Extremely High	>10	Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

\* Rock Strength Test Results

Point Load Strength Index, Is<sub>(50)</sub>, Axial test (MPa)

Point Load Strength Index, Is<sub>(50)</sub>, Diametral test (MPa)

Relationship between rock strength test result ( $Is_{(50)}$ ) and unconfined compressive strength (UCS) will vary with rock type and strength, and should be determined on a site-specific basis. However UCS is typically 20 x  $Is_{(50)}$ .

# **ROCK MATERIAL WEATHERING CLASSIFICATION**

Sym	bol	Term	Field Guide	
RS		Residual Soil	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported.	
XW		Extremely Weathered	Rock is weathered to such an extent that it has soil properties - i.e. it either disintegrates or can be remoulded, in water.	
	HW		Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores. In some environments it is convenient to subdivide into Highly Weathered and Moderately Weathered, with the degree of alteration typically less for MW.	
DW	MW	Distinctly Weathered		
SW		Slightly Weathered	Rock slightly discoloured but shows little or no change of strength relative to fresh rock.	
FR		Fresh	Rock shows no sign of decomposition or staining.	



# ABBREVIATIONS AND DESCRIPTIONS FOR ROCK MATERIAL AND DEFECTS

## **CLASSIFICATION AND INFERRED STRATIGRAPHY**

Rock is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS1726 – 2017, Section 6.2 – Rock identification, description and classification.

#### **DETAILED ROCK DEFECT SPACING**

Defect Spacing			Bedding Thickness (Stratification)	
Spacing/width (mm)	Descriptor	Symbol	Symbol	
opacing/width (illin)	Descriptor	Cymbol	Thinly laminated	<6
<20	Extremely Close	EC	Laminated	6 – 20
20-60	Very Close	VC	Very thinly bedded	20 – 60
60-200	Close	С	Thinly bedded	60 – 200
200-600	Medium	М	Medium bedded	200 – 600
600-2000	Wide	W	Thickly bedded	600 – 2,000
2000-6000	Very Wide	VW	Very thickly bedded	> 2,000

#### ABBREVIATIONS AND DESCRIPTIONS FOR DEFECT TYPES

Defect Type	Abbr.	Description
Joint	JT	Surface of a fracture or parting, formed without displacement, across which the rock has little or no tensile strength. May be closed or filled by air, water or soil or rock substance, which acts as cement.
Bedding Parting	BP	Surface of fracture or parting, across which the rock has little or no tensile strength, parallel or sub-parallel to layering/ bedding. Bedding refers to the layering or stratification of a rock, indicating orientation during deposition, resulting in planar anisotropy in the rock material.
Contact	CO	The surface between two types or ages of rock.
Sheared Surface	SSU	A near planar, curved or undulating surface which is usually smooth, polished or slickensided.
Sheared Seam/ Zone (Fault)	SS/SZ	Seam or zone with roughly parallel almost planar boundaries of rock substance cut by closely spaced (often <50 mm) parallel and usually smooth or slickensided joints or cleavage planes.
Crushed Seam/ Zone (Fault)	CS/CZ	Seam or zone composed of disoriented usually angular fragments of the host rock substance, with roughly parallel near-planar boundaries. The brecciated fragments may be of clay, silt, sand or gravel sizes or mixtures of these.
Extremely Weathered Seam/ Zone	XWS/XWZ	Seam of soil substance, often with gradational boundaries, formed by weathering of the rock material in places.
Infilled Seam	IS	Seam of soil substance, usually clay or clayey, with very distinct roughly parallel boundaries, formed by soil migrating into joint or open cavity.
Vein	VN	Distinct sheet-like body of minerals crystallised within rock through typically open-space filling or crack-seal growth.

NOTE: Defects size of <100mm SS, CS and XWS. Defects size of >100mm SZ, CZ and XWZ.

## ABBREVIATIONS AND DESCRIPTIONS FOR DEFECT SHAPE AND ROUGHNESS

Shape	Abbr.	Description	Roughness	Abbr.	Description		
Planar	PR	Consistent orientation	Polished	POL	Shiny smooth surface		
Curved	CU	Gradual change in orientation	Slickensided	SL	Grooved or striated surface, usually polished		
Undulating	UN	Wavy surface	Smooth	SM	Smooth to touch. Few or no surface irregularities		
Stepped	ST	One or more well defined steps	Rough	RO	Many small surface irregularities (amplitude generally <1mm).  Feels like fine to coarse sandpaper		
Irregular	IR	Many sharp changes in orientation	Very Rough	VR	Many large surface irregularities, amplitude generally >1mm. Feels like very coarse sandpaper		

Orientation: Vertical Boreholes – The dip (inclination from horizontal) of the defect.

**Inclined Boreholes –** The inclination is measured as the acute angle to the core axis.

ABBREVIATIONS AND	DESCR	IPTIONS FOR DEFECT COATING	DEFECT APERTURE			
Coating	Abbr.	Description	Aperture	Abbr.	Description	
Clean	CN	No visible coating or infilling	Closed	CL	Closed.	
Stain		No visible coating but surfaces are discoloured by staining, often limonite (orange-brown)	Open	OP	Without any infill material.	
Veneer	VNR	A visible coating of soil or mineral substance, usually too thin to measure (< 1 mm); may be patchy	Infilled	-	Soil or rock i.e. clay, silt, talc, pyrite, quartz, etc.	